

ELECTRON TUBES

PART 5 MAY 1967

Cathode-Ray Tubes Camera Tubes

Photo Tubes Photoconductive Devices

Photomultiplier Tubes Scintillators



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Scintillators



INTRODUCTION

The Data Handbook ELECTRON TUBES contains data on current types of tubes. It comprises a number of bound parts and a loose-leaf binder: the blue binder.

The bound parts contain both the final and the tentative publishing data which are available at a certain closing date. These parts will be re-issued at regular intervals in order to provide continuously for sufficient information to all those who are professionally engaged in the field of electronics, but for whom it is of secondary importance to have the disposal of the very latest additions.

For those who do need the latest information the loose-leaf binder will 'be useful, as it contains all data which have become available after the latest issues of the bound part. The binder is kept up-to-date by the regular appearance of supplements.

When a bound part is re-issued, the pertinent contents of the binder are transferred to this part, thus preventing the binder from becoming overcrowded.

The present part 5 of the Handbook ELECTRON TUBES contains the data on Cathode-ray tubes, Camera tubes, Phototubes, Photoconductive devices, Photomultiplier tubes and Scintillators.

For owners of the loose-leaf binder on tubes it may be advisable to make sure that the data on a particular type in the bound part have not been rendered out of date by a later issue in the binder. This applies especially to tentative data.





Cathode-ray tubes



GENERAL OPERATIONAL RECOMMENDATIONS CATHODE-RAY TUBES

GENERAL

Unless otherwise stated the data are given for a nominal tube.

LIMITING VALUES

Unless otherwise stated the tubes are rated according to the absolute maximum rating system.

HEATER

Parallel operation

The heater voltage must be within $\pm 7 \%$ of the nominal value when the supply voltage is at its nominal value, and when a tube having the published heater characteristics is employed.

This figure is permissible only if the voltage variation is dependent upon more than one factor. In these circumstances the total tolerance may be taken as the square root of the sum of the squares of the individual deviations arising from the effect of the tolerances of the separate factors, providing no one of these deviations exceeds ± 5 %. Should the voltage variation depend on one factor only, the voltage variation must not exceed ± 5 %.

Series operation

The heater current must be within $\pm 5 \%$ of the nominal value when the supply voltage is at its nominal value and a tube having the published heater characteristics is employed. This figure is permissible only if the current variation is dependent upon more than one factor. In these circumstances the total tolerance may be taken as the square root of the sum of the squares of the individual deviations arising from the effects of the tolerances of the separate factors, providing no one of these deviations exceeds $\pm 3.5 \%$. Should the total current variation depend upon one factor only, the current variation must not exceed $\pm 3.5 \%$.

When calculating the tolerances of associated components, the ratio of the change of heater voltage to the change of heater current in a typical series chain including a cathode ray tube is taken as 1.8, both deviations being expressed as percentages.

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HEATER (continued)

With certain combinations of valves and tube, differences in the thermal inertia may result in particular heaters being run at exceedingly high temperature during the warming up period. During this period unless otherwise stated in the published data, it is permissible for the heater voltage of the tube to rise to a maximum value of 50~% in excess of the nominal rated value when using a tube with the published heater characteristics. A surge limiting device may be necessary in order to meet this requirement. When measuring the surge value of heater voltage, it is important to employ a peak reading device, such as an oscilloscope.

In addition to the quoted above, fluctuations in the mains supply voltage not exceeding $\pm 10\%$ are permissible. These conditions are, however, the worst which are acceptable and it is better practise to maintain the heater as close to its published ratings as possible. Furthermore in all types of equipment closer adjustment of heater voltage or current will react favourably upon tube life and performance.

CATHODE

The potential difference between cathode and heater should be as low as possible and in any case must not exceed the limiting value given on the data sheets for individual tubes. Operation with the heater positive with respect to cathode is not recommended. In order to avoid excessive hum the A.C. component of the heater-to-cathode voltage should be as low as possible e.g. less than 20 V_{rms}. When the heater is in a series chain or earthed, the 50 c/s impedance between heater and cathode should not exceed 100 k Ω . If the heater is supplied from separate transformer windings the resistance between heater and cathode must not exceed 1 M Ω .

ELECTRODES

In no circumstances should the tube be operated without a D.C. connection between each electrode and the cathode. The total effective impedance between any electrode and the cathode should be as low as possible and must never be allowed to exceed the published maximum value.

ELECTRODE VOLTAGES

Reference point for electrode voltages is the cathode. For cathode drive service the reference point is grid No.1.

Grid cut-off voltages

Values are given for the limits of grid cut-off voltage per unit of the first accelerator voltage. The brightness control voltage should be arranged so that it can handle any tube within the limits shown, at the appropriate first accelerator voltage. 7Z2 5880

First accelerator voltage

The first accelerator electrode of a so called unipotential lens provides by applying a fixed voltage independent focus and brightness controls. Care should be taken not to exceed the maximum and minimum limits for reasons of reliability and performance.

Deflection blanking electrode voltage

The mean potential of the deflection blanking electrode should be equal to that of the first accelerator.

If applicable the voltage difference (ΔV_{g_3}) given in the data should be applied to the beam blanking electrode to obtain beam blanking of a stated beam current for all tubes of the relevant type.

Focusing voltage

The focusing electrode voltage limits are given in the data. The focus voltage supply should be arranged such that it can handle these limits, so that in any tube the cross-sectional area of the electron-beam on the screen can be optimally displayed. As the focus current is very limited a high resistance series chain may be used.

Astigmatism control electrode voltage

To achieve optimum performance under all conditions it is desirable to apply a voltage for control of astigmatism (a difference in potential of this electrode and the y plates). The required range to cover any tube is given in the relevant data.

Beam centring electrode voltage

The beam centring electrode facilitates the possibility to centre the scan in xdirection with respect to the geometric centre of the faceplate by applying a voltage, the limits of which are given in the relevant data, to this electrode. Optimum condition is obtained when the brightness at both left and right edges of the scan are equal.

Deflection plate shield voltage

It is essential that the deflection plate shield voltage equals the mean y plates voltage.

Geometry control electrode voltage

By varying the potential of this electrode the necessary range of which is given in the relevant data the possible occurrence of pin-cushion and barrel-pattern distortion can be controlled.

Deflection voltages

For optimum performance it is essential that true symmetrical voltages are applied. It should further be noted that the mean x and y plate potentials must be equal. Moreover the deflection plate shield voltage, the mean astigmatism control voltage, if applicable the mean beam centring electrode voltage and the geometry electrode voltage should also be equal to the mean x and y plate potentials. If use is made of the full deflection capabilities of the tube, the deflection plates will intercept part of the electron beam near the edge of the scan. Therefore a low impedance deflection plate drive is necessary.

Raster distortion and its determination

Limits of raster distortion are given for most tubes.

A graticule, consisting of concentric rectangles is aligned with the electrical x axis of the tube. The edges of a raster will fall between these rectangles with optimum correction potentials applied.

Measuring procedure:

a) Shift the x-trace to the centre of the graticule.

- b) Align horizontal centre line of graticule with the centre line of the x-trace.
- c) Shift x-trace vertically between resp. upper and lower two horizontal lines of graticule. The eastern of the network per will not fall outside the area bounded by the

The centre of the x-trace now will not fall outside the area bounded by the horizontal graticule lines.

- d) Without moving the graticule, switch to a vertical trace and shift this trace horizontally (resp. left and right) between the pairs of vertical lines of the graticule, and also now the centre of the y-trace will not fall outside the area bounded by the vertical graticule lines.
- e) Focus and astigmatism will be adjusted for optimum performance.
- f) Pattern geometry correction will be adjusted for optimum performance in the sense of minimizing simultaneously the deviation of the centre of x - respectively y-trace.

Linearity

The linearity is defined as the sensitivity at a deflection of 75 % of the useful scan with respect to differ from the sensitivity at a deflection of 25 % of the useful scan. These sensitivities will not differ by more than the indicated value.

Post deflection shield voltage

In order to optimize contrast in mesh tubes a fixed negative voltage with respect to the geometry control electrode voltage should be applied. The range is given in the data. 7Z2 5882

Helix resistance

In order to calculate the high tension supply a minimum resistance is given in the data.

Final accelerator voltage

Tubes with PDA are designed for a given final accelerator voltage to astigmatism control electrode voltage ratio. Operation at higher ratio may result in changes in deflection uniformity and pattern distortion.

High tension supply

In order to avoid damage of the screen it is important that prior to the high tension a deflection voltage e.g. the time base voltage is applied.

LINE WIDTH

Shrinking raster method. Conditions as given in the relevant data.

Focus and astigmatism potentials should be adjusted for optimum performance. Optimum performance is that adjustment which will simultaneously minimize the horizontal and vertical trace widths at the centre of the useful scan.

The raster shall be compressed until the line structure first disappears or begins to overlap or show reverse line structure.

The line width is equal to the quotient of the width of the compressed pattern transverse to the line structure divided by the number of lines which are being scanned.

In older types the line width is measured on a circle with the aid of a microscope.

CAPACITANCES

Unless otherwise stated the values given are nominal values measured on a cold tube on the tube contacts. The contacts and measuring leads or sockets being screened.

MOUNTING

Unless otherwise stated the mounting position is any. However, the tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

To avoid dangerous glass strain care should be taken when installing the tube.

Shielding

The tubes must be shielded against electrical and magnetic fields. Special attention should be paid to the mounting of transformers, coils etc.

SCREEN

To prevent screen burn stationary or slow moving spots together with high screen currents should be avoided.

If measurements are to be made under high ambient light conditions it is advisable to use a contrast improving filter and or a light hood.

TRACKING ERROR

Tracking is the ability of a multigun tube to superimpose simultaneously information from each gun.

Tracking error is the maximum allowable distance between the displays of any two guns.

RATING SYSTEMS (in accordance with I.E.C. publication 134)

Absolute maximum rating system

Absolute maximum ratings are limiting values of operating and environmental conditions applicable to any electronic device of a specified type as defined by its published data, which should not be exceeded under the worst probable conditions.

These values are chosen by the device manufacturer to provide acceptable serviceability of the device, taking no responsibility for equipment variations, environmental variations, and the effects of changes in operating conditions due to variations in the characteristics of the device under consideration and of all other electronic devices in the equipment.

The equipment manufacturer should design so that, initially and throughout life, no absolute-maximum value for the intended service is exceeded with any device under the worst probable operating conditions with respect to supply voltage variation, equipment component variation, equipment control adjustment, load variations, signal variation, environmental conditions, and variations in characteristics of the device under consideration and of all other electronic devices in the equipment.

Design-maximum rating system

Design-maximum ratings are limiting values of operating and environmental conditions applicable to a bogey electronic device of a specified type as defined by its published data, and should not be exceeded under the worst probable conditions.

These values are chosen by the device manufacturer to provide acceptable serviceability of the device, taking responsibility for the effects of changes in operating conditions due to variations in the characteristics of the electronic device under consideration.

The equipment manufacturer should design so that, initially and throughout life, no design-maximum value for the intended service is exceeded with a bogey device under the worst probable operating conditions with respect to supply-voltage variation, equipment component variation, variation in characteristics of all other devices in the equipment, equipment control adjustment, load variation, signal variation and environmental conditions.

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Design-centre rating system

Design-centre ratings are limiting values of operating and environmental conditions applicable to a bogey electronic device of a specified type as defined by its published data, and should not be exceeded under normal conditions.

These values are chosen by the device manufacturer to provide acceptable serviceability of the device in average applications, taking responsibility for normal changes in operating conditions due to rated supply-voltage variation, equipment component variation, equipment control adjustment, load variation, signal variation, environmental conditions, and variations in the characteristics of all electronic devices.

The equipment manufacturer should design so that, initially, no design-centre value for the intended service is exceeded with a bogey electronic device in equipment operating at the stated normal supply-voltage.

NOMENCLATURE

Two type nomenclature systems are currently in existance for our C.R. tubes. All future tubes will have numbers in the "new system", earlier tubes will retain numbers in the "old system".

NEW CODE SYSTEM

The type number consists of a single letter followed by two sets of figures ending with one or two letters.

The first letter indicates the prime appplication of the tube.

- A Television display tube for domestic application
- D Oscilloscope tube single trace
- E Oscilloscope tube multiple trace
- F Radar display tube direct view
- L Display storage tube
- M T.V. display tube for professional application direct view
- P Display tube for professional application projection
- Q Flying spot scanner

The first group of figures indicates the diameter or diagonal of the luminescent screen in cm.

The second group of figures is a two-figure serial number indicating a particular design or development.

The second group of letters indicates the properties if the phosphor screen. The first letter denotes the colour of the fluorescence or phosphorescence in the case of long or very long afterglow screens.

The second letter of this group is a serial letter to denote other specific differences in screen properties.

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- A Purple reddish purple bluish purple
- B Blue purplish blue greenish blue
- D Blue green
- G Green bluish green yellowish green
- K Yellow green
- L Orange Orange pink
- R Red reddish orange red purple purplish red pink purplish pink
- Y Yellow greenish yellow yellowish orange
- W White screen for T.V. display tubes
- X Three-colour screen for T.V. display tubes

OLD SYSTEM

The type number consists of two letters followed by two sets of figures. The first letter indicates the method of focusing and deflection:

- A Electrostatic focusing and electromagnetic deflection
- B Electrostatic focusing and electrostatic deflection
- M Electromagnetic focusing and electromagnetic deflection.

The second letter indicates the properties of the phosphor screen.

See also section "Screen Phosphors"

The first group of figures:

for round tubes: screen diameter in cm

for rectangular tubes: screen diagonal in cm

The second group of figures denotes the serial number

LIST OF SYMBOLS

| Symbols denoting electrodes and electrode connections | |
|---|--------------------------------|
| Heater or filament | f , |
| Cathode | k |
| Grid Grids are distinguished by means of an additional numeral; the electrode nearest to the cathode having the lowest number. | g |
| Deflection plates intended for deflection in horizon- tal direction. | x ₁ ,x ₂ |
| Deflection plates intended for deflection in vertical direction. Sectioned deflection plates are indicated by an additional decimal e.g. y _{1.1} y _{1.2} and y _{2.1} y _{2.2} | у1, у2 |
| External conductive coating | m |
| Fluorescent screen | l |
| Tube pin which must not be connected externally | i.c. |
| Tube pin which may be connected externally | n.c. |
| Symbols denoting voltages | |
| Symbol for voltage, followed by an index denoting the relevant electrode. | V |
| Heater or filament voltage | Vf |
| Peak value of a voltage | V _p |
| Peak to peak value of a voltage | V _{pp} |

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Symbols denoting currents

- Remark I The positive electrical current is directed opposite to the direction of the electron current.
- Remark II The symbols quoted represent the average values of the concerning currents unless otherwise stated.

Symbol for current followed by an index denoting the relevant electrode.

Heater or filament current

Symbols denoting powers

Dissipation of the fluorescent screen

Grid dissipation

Symbols denoting capacitances

See I.E.C. Publication 100.

Symbols denoting resistances

Symbol for resistance followed by an index for the relevant electrode pair. When only one index is given the second electrode is the cathode.

When R is replaced by Z the "resistance should read "impedance"

Symbols denoting various quantities

| Brightness | | В |
|-------------------------|--|---|
| Frequency | | f |
| Magnetic field strength | | Н |
| Deflection factor | | М |

Ι

 I_{f}

Wo

Wg

R

SCREEN PHOSPHORS AND

INDUSTRIAL CATHODE-RAY TUBES

CHOICE OF SCREEN

When a cathode ray tube is chosen for a particular application, the designer of the apparatus bases his choice on a number of factors; for example, screen shape and size, the operating potentials that will be available, and the screen characteristics. He may find that the required physical and electrical configuration is provided by a number of tube types which employ different screen phosphors, so that he will have to choose between one phosphor and another. In any event, the performance obtainable from the screen is of major importance, since the purpose of any cathode ray tube application is the provision of a suitable display.

Here the relationship between screen characteristics and the requirements of the main groups of applications will be discussed. The suitability of particular screen types is considered in terms of operating conditions that will be met and the performance that must be achieved.

The ultimate choice is determined by the detailed requirements of each specific application; therefore, in addition to general guidance, the methods of calculating the performance that will be obtained under given conditions are included. The calculations take into account the characteristics of the screen, the operational requirements, the nature of the viewing device, and the effect (where the screen is viewed by the eye) of the external viewing conditions.

GENERAL REQUIREMENTS

The three major screen properties - energy conversion efficiency, persistence, and spectral distribution - should be those most suitable for the application. Where there is any degree of conflict between one requirement and another, the best compromise must be achieved. The performance of the screen should be reasonably constant throughout the range of beam currents that is likely to be met.

These general requirements will be discussed in relation to the main groups of cathode ray tube applications. These are:

- 1. Raster type applications, in which the writing speed is generally constant but the beam current is modulated to produce variation of light and shade.
- Oscilloscope applications, in which the beam current is usually constant during a trace but the writing speed may vary.
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- 3. Radar applications
- 4. Flying-spot scanners
- 5. Storage applications

SCREENS FOR RASTER TYPE APPLICATIONS

A number of different screens are available for raster type displays. Those which are most suitable for the main sub-groups of this group of applications are indicated in the following notes.

Monitors and Viewfinders

Monitoring and viewfinding systems in television studios operate at the same field repetition frequency and timebase speed as the broadcast channel, and their screen requirements are substantially the same as those of domestic television tubes. The repetition frequencies are such that persistence of vision and the persistence of the screen obviate flicker. The persistence must not be sufficiently great to smear the images of moving objects.

In monochrome television systems, white fluorescence is used, for aesthetic reasons. The W type screen is widely established for domestic viewing tubes and studio monitors and viewfinders.

Closed Circuit Systems

Where closed circuit monochrome television systems make use of normal television field and line speeds, screens with W phosphor are suitable.

In some systems, however, other speeds are used. If the scanning speed is low, the screen must have a persistence which is long enough to minimise flicker, and a long-persistence screen such as type LA, LD or LC must be used in order to maintain a complete picture.

Data Transmission

Since the images to be transmitted are, in general, stationary, the information does not need to be modified at the same rate as television picture information. The field repetition frequency and the bandwidth can be reduced, and transmission over lines is relatively simple. At repetition frequencies down to five fields per second a tolerable freedom from flicker is achieved with the cadmium chloro-phosphate phosphors that are used, for example, in the LA screen. For even lower frequencies, the LD screen is recommended. This screen, it should be noted, has a relatively low power-loading limit, and care must be taken to avoid burning.

Telerecording

A major limitation to the quality of telerecording is the difficulty of both pulling the film through the camera gate and operating the shutter in the field flyback time. In early systems, the first field of the interlaced picture was used for these operations; therefore only half the information was recorded.

To overcome this limitation, the information from the first field is stored in the screen of the cathode ray tube during the time that the shutter is closed. The film is pulled through the gate and the shutter is opened. The second field is then imposed on the stored field on the screen. The stored information of the first field will, of course, have lost some of its initial luminance; therefore the second field is written on the screen at a correspondingly reduced luminance level. The full interlaced information is then photographed.

The application is obviously a critical one, and the screen must meet a number of special requirements. The persistence must be defined within narrow limits, and it must be substantially constant throughout the life of the tube, otherwise the timing of the system will be inaccurate. There must not be a sharp peak of light output ("flash") at the moment of excitation, otherwise the second field will appear brighter than the first. And the light output from the first field must not have decayed to an unusably low level by the time that the second field has to be written.

These special requirements are met by screen type LA.

SCREENS FOR RASTER TYPE APPLICATIONS

The range of frequencies for which oscilloscopes are designed is extremely wide, and even in a single instrument a wide range may have to be covered. The requirements of light output and persistence at high speeds conflict with the requirements at low speeds, therefore a compromise is usually necessary. If the screen that is used has a good luminous efficiency, a satisfactory compromise can be attained.

General Purpose Applications

The screens in the G group are widely used in general purpose oscilloscopy. They have a high efficiency and a reasonably fast build-up, so that they are suitable for use at fairly high writing speeds. The GH screen has two spectral distribution peaks, one in the green and one in the blue region. The blue peak provides a high actinic efficiency for use with panchromatic film or, in some instances, with orthochromatic film. However, the effective visual persistence is rather short, so that at slow scan speeds very little information is obtained from the trace.

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The lack of visual persistence in the GH screen has led to the introduction of the GL and GP types. The high efficiency of the GH screen is largely retained, but the persistence is of the order of one to five seconds, depending on the operating conditions. Slow scan speeds can therefore be used.

The GM screen has a purplish-blue flash and a yellowish-green persistence. For normal oscilloscopic work, and especially at voltages between 1 kV and 10 kV, this is the recommended screen if a long persistence is the main requirement. The luminous efficiency is about one-fourth of that of the GH type, so that for this reason, as well as the long persistence, the GM screen is not suitable for high-speed applications.

Non-recurrent High-speed Applications

When a rapid non-recurrent phenomenon is to be observed, a long-persistence screen with a slow build-up is not suitable. The usual technique is to use a fast screen and photographic recording. A timebase, triggered by the incoming signal, is applied to the X deflectors, and the signal itself to the Y deflectors.

The choice of screen for the single-shot type of application is dictated by the recording material that is to be used. For panchromatic and some orthochromatic film, the GH screen provides the fastest writing speed. If the trace is visible on this screen, then, in general, it can also be photographed if good photographic materials and techniques are used. For blue-sensitive film or recording paper the BE screen is preferable. Its luminous efficiency is low, but its spectral characteristic matches that of the emulsion.

Moving Film Applications

When a moving film technique is employed for the recording of recurrent phenomena, the persistence of the screen must be short if smearing of the image is to be avoided. With orthochromatic film, the BE screen is recommended. Smearing is negligible in the majority of applications, and appears only under certain unusual and extreme conditions. Equally good results may be obtained with panchromatic film and the GH screen.

Slow-scan Applications

Visual observations of slowly-varying functions is often unsatisfactory with general purpose screens. The eye does not easily appreciate the path of a moving spot, since the spot tends to attract most of the observer's attention. This difficulty is overcome, to some extent, by the use of a long-persistence screen. The spot leaves a trace which persists long enough for the waveform to be examined.

The useful persistence of any screen is dependent on the ambient illumination. If the screen is provided with a hood, a dark-adapted eye can see the trace down to quite low levels of light output. Writing speed also affects the persistence, to a certain limit which depends on the screen type which is used. In single-shot 7Z2 5901

applications an increase in spot velocity will reduce the persistence, and vice versa. The observation of information which recurs only a few times per second can be improved by the use of a long-persistence screen; but, in general, the length of the persistence obtained will not be great.

For most long-persistence applications the GM screen is recommended. The GL and GP screens are also useful.

For very long persistence the LC or LD screens are used. They have orange luminescence. Care should be taken to avoid overloading these screens, since they are prone to burning.

SCREENS FOR RADAR APPLICATIONS

A long persistence is usually of primary importance in radar applications, because the aerial sweep is slow and the picture must be retained for relatively long periods. The choice of a screen is complicated if the display is to be viewed where there is much ambient light. A long-persistence screen with a relatively low light output may be less suitable than a screen with shorter persistence but greater light output.

The build-up characteristic is of particular interest in radar applications. It can be exploited, under conditions of repeated excitation, to differentiate between the desired "permanent" echoes and noise such as sea clutter. The echo from a target is repeatedly displayed on successive scans, and full brightness is built up; whereas transitory echoes are not additive, and produce less than peak brightness. The published build-up curves for radar-type screens are presented in a way that simulates p.p.i. conditions. Points on the curve, as shown in "Screen data", represent the light output from the screen immediately before each excitation pulse.

Radar requirements, when examined in detail, are found to be exacting. For instance, in general purpose marine navigational systems the performance must be satisfactory throughout a wide variety of aerial sweep speeds, pulse repetition frequencies, and target ranges (say from 0.5 to 50 miles). In a single installation, a diversity of operating conditions must be catered for, therefore the choice of screen for the display tube is necessarily a compromise. A number of screen types are available.

The LD screen has found extensive use in medium-range marine navigational systems. It has a very long persistence which provides a good display over a large variety of aerial rotation speeds and pulse repetition frequencies.

In river radar systems with short ranges and fast-moving targets, a rather shorter persistence is required, since it is only necessary to maintain good brightness between sweeps. Also, if the range has to be changed when navigating at close quarters, the trace from the earlier scan must clear quickly if it is not to clutter the first traces of the later scan. The LB screen meets these requirements. 7Z2 5902 In long-range navigational radar, and particularly in marine true-motion installations, the LC very long-persistence screen is widely used. It is also suitable where successive traces of a moving target are required for comparison, so that paths and speeds can be seen directly. The LC screen is also used in meteorological work, in airfield control, and in military radar systems. In many instances it is used in conjunction with interscan and data-handling techniques.

The GM long-persistence screen is sometimes used in marine radar. Its persistence is considerably shorter than that of the LC and LD screens. It has a disadvantage in that it does not provide the resolution capabilities possessed by tubes which use LC or LD screens. The reason for the lower resolution is that the screen is of the double-layer type; and, in order to obtain the desired decay characteristic, it is thicker than the LC and LD screens. The first layer is excited by electrons. This layer re-emits energy in the ultraviolet region, which then excites the second layer from which the luminous output is obtained. Resolution is lost during this process because of the scattering of the ultraviolet through the thickness of the second layer.

The GB screen is, like the GM screen, of the double-layer variety. It is used successfully in weather warning systems in aircraft cockpits. The main requirement is the ability to withstand the high accelerating voltages used in tubes for this type of application. Its long persistence is similar to that of the GM screen. With the aerial scanning speeds that occur in this type of equipment it displays complete cloud formations during the aerial sweep.

One of the main uses of the GJ medium-persistence screen is in airborne radar systems, where the scan rate is high enough to overcome the limited persistence of the screen. Its spectral emission makes it suitable for visual observation at the high ambient light levels normally encountered in this type of application.

For large radar displays a projection system may be used. For this purpose the BC screen, which has a killed persistence, provides a purplish-blue and ultraviolet output which is projected, by optical means, on to a large secondary screen which has suitable long-persistence characteristics.

SCREENS FOR FLYING-SPOT SCANNERS

In flying-spot scanners the energy conversion efficiency of the screen, throughout the spectral range that corresponds to the colour response of the detecting device, must be as high as possible.

Very short persistence is essential where high-definition scans are used, but the requirement is less stringent for slow-speed facsimile reproduction. For example, if a 625-line raster of 5 Mc/s definition is required, then there must be no effective light output after 0.3 μ s; but for a slow-speed system of comparable definition and a line speed of one second, the persistence can be as long as 2 ms. 7Z2 5903 The BA very short-persistence screen is widely used for monochrome rastertype applications. Its peak output is at 400 to 420 m μ m, in the ultraviolet region. It is therefore particularly suitable for use with photomultipliers having conventional caesium-antimony photocathodes. The persistence enables a good overall signal-to-noise ratio to be achieved.

The GE short-persistence screen has been developed for flying-spot applications in colour television systems. Its persistence is sufficiently short. It has an adequate light output in the red region of the visible spectrum, with a peak at 510 m μ m in the green region.

SCREENS FOR STORAGE APPLICATIONS

In some applications it is an advantage if a trace can be stored for future examination or for direct comparison with later traces. The GN screen provides storage for periods up to several hours.

A back layer emits energy in the blue and ultraviolet region when it is bombarded with electrons. The front layer, excited by the ultraviolet radiation, has blue fluorescence and green phosphorescence, with a persistence of the same order as that of the GM screen.

If the screen is subsequently exposed to infrared radiation, a second light output is obtained, with an intensity and a persistence which are functions of the original writing conditions and of the intensity of the infrared irradiation. The stored trace, or a succession of superimposed traces, can thus be made available. The stored traces, when they are made visible by irradiation, have a brightness related to that at which they were written, and they all decay at the same rate as one another. Erasure is effected by prolonged infrared irradiation.

Ambient ultraviolet radiation should be excluded, since it will activate the front layer and produce background light which reduces contrast. Stray infrared should also, of course, be excluded, since it will dissipate the stored trace. The GN screen has a rather low maximum writing speed.

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SCREEN CHARACTERISTICS

INTERPRETATION OF PUBLISHED SCREEN CHARACTERISTICS

The field of c.r.t. applications is very extensive. For this reason it is impossible to provide published data covering all conceivable requirements. The measurements for published data are taken under conditions as close as possible to those at which the given screen is expected to operate. In some applications, the nature of the display does not readily lend itself to measurement purposes, and a resort has to be made to a more suitable type of display.

Where a given application departs from the conditions specified in published data, some valuable information can be extracted by means of simple calculations. Inevitably, some errors will be introduced; but in view of the approximately logarithmic response of the eye, the answers obtained are reasonably valid.

Much of the information presented in published data is based on a raster type of display, using - for measurement purposes - a non-interlaced raster of 200 lines and 50 fields per second. Whenever possible, the raster is defocused so that the lines just begin to merge together. This produces reasonably uniform screen loading. The quoted values of screen loading apply to the loading while the screen is under electron bombardment, and the effect of flyback is taken into account. The values of screen luminance given in published data are in terms of photometric units. This implies that the results are intended to represent the appearance of the display as seen by the eye.

In the following discussions, small letters are used for general considerations and for quantities in published data, while capital letters represent quantities involved in a particular case under consideration.

SCREEN LUMINANCE

The user can control four factors which affect screen luminance as seen by the eye. They are the area of excitation, the beam current, the applied potential, and the duration of excitation. A brief review of the effect of these factors on luminance will be made. In the first instance it will be assumed that only one of the factors is varied at a time.

The relationship between the luminance b and the current i reaching the screen can be written as

$$b = k_1 i \gamma$$

where k_1 is a constant and the index γ at small values of current is, for most screens, slightly less than unity. It decreases in value with increase in beam current.

The relationship between the potential v applied to the screen and the luminance is more complex, and is often written in the form

$$b = k_2 (v - v_0)^n$$

where

 $k_2 = a \text{ constant} \\ v_0 = a \text{ threshold potential} \\ n = an \text{ index, greater than unity.}$

Both v_0 and n are functions of the phosphor and of the manner in which it is deposited on the tube face. For this reason the relationship may vary from one tube type to another, although the same screen type may be used.

When a screen is operated at a current density well below the saturation level, it may be assumed that the luminance increases with increase of the duration of excitation. Thus,

 $b = k_3 t \tag{3}$

This holds only within the maximum limit for t, which is set by the time resolution of the eye and is about 0.1 s.

Over reasonably small variations in size of the excited area, the luminance can be considered as inversely proportional to the area, or

 $b = k_4/a$

Experimental results seem to indicate that the luminance of the screen produced by all the factors can be represented as:

$$b = \frac{k}{a} i \gamma (v - v_0)^n t$$
(5)

Thus, to a first approximation, the luminance is a function of the energy applied to the screen. The range over which the beam current and the duration of excitation may vary is considerable. However, the amount of energy the screen can handle is limited; therefore the screen can deal with an increase in one of these quantities at the expense of the other. A large increase in both the beam current and the excitation time will lead to saturation and eventually to permanent screen damage in the form of burn.

(1)

(2)

(4)

The published data are normally given in the form of average luminance b as a function of average screen loading u, or

 $\mathbf{b} = \mathbf{f}(\mathbf{u}) \tag{6}$

for several values of potential applied to the screen.

The raster itself is formed by scanning a spot progressively over a specified area. Thus an elementary screen area can be considered as that covered by the area of the electron beam. For the purpose of calculation let us assume this elementary area to be w cm wide and w cm long. If the current in the beam is i μ A, then as the beam is passing the elementary area, the real screen loading is given by

$$u(pk) = \frac{1}{w^2}$$
(7)

The duration of the loading is t_W , that is the transit time of the spot over the elementary area.

The amplitude of the waveform of peak luminance is a function of the build-up and decay characteristics of the particular screen under consideration. For screens with extremely short characteristics, the luminance is in the form of a pulse of light of amplitude b(pk) and duration t_W . On the other hand, a screen having long characteristics will produce luminance which follows the build-up characteristic during the excitation time t_W , and afterwards the decay characteristic. Two screens operating under identical conditions and having the same conversion efficiency, but differing in build-up and decay characteristics, should have the same b(pk) t_W product. However, their instantaneous luminance will follow their build-up characteristics, and therefore may differ considerably.

Thus the b(pk) used in these calculations is largely a fictitious quantity. It is equal to the area embraced by the build-up and persistence characteristic of a given screen, divided by the time of excitation. As an absolute quantity it is of little value. However, since it is derived from the screen characteristics, it is useful in comparing screen operating conditions.

Let the raster repetition frequency be $f_r = \frac{1}{t_r}$. Then: the average screen loading is

$$u = \frac{i}{w^2} \frac{t_w}{t_r}$$

and the average screen luminance

$$b = b(pk) \frac{t_W}{t_r}$$

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(9)

(8)

Both equations contain the term t_W/t_r . Since the raster is scanned linearly,

$$t_{\rm W} = t_{\rm I} \frac{{\rm w}}{{\rm I}} \tag{10}$$

where l is the length of scanned line and t_1 is the time required to scan the line, therefore

$$\frac{t_{\rm W}}{t_{\rm r}} = \frac{t_{\rm l}}{t_{\rm r}} \frac{w}{l} \tag{11}$$

Let us assume that the raster produced for preparation of published data is so defocused that the lines are touching each other. If the raster height is h, its width is l, and the number of lines is n, then

$$w = \frac{h}{n}$$

therefore

$$\frac{t_{W}}{t_{r}} = \frac{t_{l}}{t_{r}} \frac{h}{nl}$$

Furthermore,

$$t_1 = \frac{t_1}{n}$$

therefore

$$\frac{t_W}{t_r} = \frac{h}{n^{2}l} = \frac{w^2}{hl}$$

Substituting in Eqs (8) and (9) we obtain

$$u = \frac{i}{hl}$$

and

$$b = b(pk) \frac{w^2}{hl}$$

or

$$b = b(pk) \frac{h}{n^2 l}$$

when the lines just touch.

The published data provide the values of average screen luminance b as a function of average screen loading u. Thus, if one of the quantities is known, it is possible to determine the other. In many cases allowances have been made for flyback times, so i is the actual current and b the actual luminance during excitation.

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(15a)

(15b)

(14)

(13)

(12)

In all cases the published data provide information at several values of potential applied to the screen. In this way all the factors in Eq(5) are taken into account.

The derived formulas enable investigation of the effect of various screen operating conditions on the screen luminance to be made. For instance, it has been shown in Eq (15) that the peak luminance is inversely proportional to the square of spot size. Thus, with the raster size and the number of lines maintained constant, halving of the spot diameter increases the screen loading by a factor of 4. If the efficiency characteristics were linear, no change in light output would be obtained. Any possible reduction in average light output can be found approximately from published data as a ratio of

> screen luminance at 4 x operating current 4 x screen luminance at the operating current

But there would be an increase in peak luminance in accordance with Eq (15a). It should be noted that Eq(15b) will not apply in this case, as the lines would not be touching (that is, nw \neq h); this equation is relevant only for luminance changes of a raster in which the lines are just touching

In oscilloscope work, especially at high writing speeds, it is of importance to obtain as high a spot luminance as possible. Consequently, the value of beam current is pushed to the limit. Unfortunately, as the beam current is increased there is some increase in beam diameter. Since the spot luminance is proportional to i/w^2 , the optimum conditions are occurring when the quotient is at a maximum.

In slow-scan applications, let us assume that the tube operating conditions and the number of lines used are the same as for the published data. For the same length of scanned line, let the scanning time be T_1 (where $T_1 > t_1$). The increase in screen loading is in the ratio T_1/t_1 .

In consequence, one would expect only a slight drop in light output for a small value of the quotient; but for large values there would be not only a drop in average screen luminance but also some distortion of spot shape caused by screen saturation.

Let us now assume that the raster repetition frequency is constant and the number of lines is varied. On the whole, not much change will be expected when the lines are overlapping. When the lines are well separated, a reduction in the number of lines will produce higher screen loading and a reduction in light output. The converse will happen when the number of lines is increased.

In the following sections an attempt will be made to evaluate various applications in terms of published data information.

DATA INTERPRETATION FOR RASTER TYPE APPLICATIONS

From the preceding argument, the average screen loading in a practical case is

$$U = \frac{I}{W^2} \cdot \frac{T_W}{T_r}$$
(16)

where \mathbf{T}_w is the time taken to traverse one spot width, and \mathbf{T}_r is the time taken to scan one raster.

The average screen luminance is

$$B = B_{(pk)} \frac{T_W}{T_r}$$
(17)

Let us assume that the height of the scanned raster is H, the width is L, the active line scanning time is T_l , the raster repetition period is T_r , the number of lines is N, and the number of active lines is N_a . Then

$$T_w = Tl \frac{W}{L}$$

and

$$\frac{T_{W}}{T_{r}} = \frac{T_{l}}{T_{r}} \cdot \frac{W}{L} \cdot$$

For any scan, if

 τ_s = duration of scan τ_f = duration of flyback $\overline{\tau}$ = duration of whole cycle

then

$$\tau = \tau_{\rm S} + \tau_{\rm f} \, .$$

If we write

$$\frac{\tau_{\rm f}}{\tau_{\rm s} + \tau_{\rm f}}$$
 = p (the flyback fraction)

then

$$\tau_{\rm S} = \tau \left(1 - p\right)$$

In the case under consideration, T_l is the active scanning time, and T_m is the interval between lines, therefore

 $T_1 = T_m (1 - P_1)$

where P₁ is the flyback fraction in the line direction. Similarly

 $N_{a} = N(1 - P_{v})$

where Pv is the vertical flyback factor.

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(19)

(18)

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13

Substitution for T₁ in Eq (18) gives

$$\frac{T_{W}}{T_{r}} = \frac{1 - P_{l}}{T_{r}} \cdot T_{m} \cdot \frac{W}{L}$$
(20)

But $T_r = NT_m$ and $N = N_a/(1 - P_v)$ therefore

$$T_{\rm m} = \frac{T_{\rm r}}{N_{\rm a}} (1 - P_{\rm v}) \tag{21}$$

If we assume that the lines are touching, then $N_a = H/W$, therefore

$$\frac{T_{\rm W}}{T_{\rm r}} = (1 - P_{\rm l}) (1 - P_{\rm v}) \frac{W^2}{HL}$$
(22)

Finally, substituting in Eqs (16) and (17) we have

$$U = \frac{1}{HL} (1 - P_1) (1 - P_v)$$
(23)

and

$$B = B(pk) \frac{W^2}{HL} (1 - P_l) (1 - P_v)$$
(24)

Since W = H/N_a and $N_a = N(1 - P_v)$, then

$$B = B(pk) \frac{H(1 - P_1)}{N^2 L(1 - P_V)}.$$
 (25)

Now

$$I(1 - P_l)(1 - P_v) = I_{av}$$
 (26)

where I_{av} represents an average current flowing through the cathode ray tube in presence of line and field blanking. For the 405-line and 625-line television systems, $P_I = 0.185$ and $P_v = 0.07$. Thus in these systems the current I present in the raster exceeds the average current by a factor of 1.31.

In the above calculations it has been assumed that the lines of the raster are touching each other. This is rather an exception than a rule. When considering this problem it is necessary to define more accurately the screen luminance. In most cases it is a mean value for the whole raster. For these considerations the calculations are acceptable in their present form.

Frequently, the published data for television tubes are given in terms of beam current for a quoted raster size. From these values the average screen loading u = i/hl may be readily obtained. Alternatively, we have from Eqs (23) and (26)

$$\frac{i}{hl} = \frac{I}{HL}$$

or

$$i = I \frac{hl}{HL}$$

(27) 7Z2 5911
Example

It is intended to operate a tube with a W screen as a television monitor at a screen potential of 14 kV and with a raster 20 cm by 15 cm. What luminance can be expected if the average beam current is $50 \ \mu$ A.

As the tube is intended for operation in a television system,

$$I_{av} = I (1 - P_l) (1 - P_v) = I \ge 0.76$$
$$I = \frac{50}{0.76} = 66 \ \mu A.$$

The current density is therefore

$$\frac{i}{hl} = \frac{66}{300} = 0.22 \ \mu A/cm^2.$$

At this current density and at a screen potential of 14 kV, the luminance, as can be seen from the relevant curve, is 280 nt.

DATA INTERPRETATION FOR OSCILLOSCOPE APPLICATIONS

The requirements of repetitive and single-pulse applications must be considered.

Repetitive Excitation

An oscilloscope display is essentially a single trace display. In any particular situation, let us assume that the length of trace is L, the duration T_1 , and the repetition frequency $F_r = 1/T_r$. For a line width W, let the transit time be T_W , then from Eq (8) the screen loading is

$$U = \frac{I}{W^2} \frac{T_W}{T_r} .$$

Since

$$T_w = T_1 \frac{W}{L}$$

then

$$U = \frac{I}{WL} \frac{T_1}{T_r} .$$

The average screen loading obtained from the above formula may be used to find the corresponding average trace luminance from the published data.

Single-Pulse Excitation

It is possible to estimate, from the published data, the trace luminance under single-pulse excitation. Since the trace is not repetitive, let us take a repetition frequency at which the eye resolves light modulation, say about 10 c/s. 7Z2 5912

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(28)

Let this repetitive time be T_r , then the average screen loading is

$$U = \frac{I}{W^2} \frac{T_W}{T_r}$$
(29)

and the corresponding average screen luminance B can be found from the published data.

From Eq (9) the peak luminance is

$$B(\mathbf{pk}) = B \frac{T_{\mathbf{r}}}{T_{\mathbf{w}}}$$
(30)

and its duration is T_w .

The $B(pk)T_W$ product is equal to the area under the build-up and decay characteristic of a given screen. For fast- and medium-persistence screens, most of this area will be within time T_r (< 0.1 s). Hence the luminance perceived by the eye will be

$$\frac{B(pk)T_W}{T_r} = B$$

Example

In a particular application a scan of 4 cm and a duration of 10 μ s are produced at a repetition frequency of 400 c/s. The tube has a GH type screen. It is operated at 10 kV, and the current reaching the screen during the trace is 10 μ A. What trace luminance can be expected at a line width of 0.2 mm.

| I | = | 10 µA | T1 = | $\frac{10}{106}$ s |
|---|---|--------------------|------|--------------------|
| w | = | $\frac{2}{100}$ cm | т = | 100 |
| L | = | 4 cm | 'r | 400 5 |

Substitution in Eq (28) gives

$$U = 10 \frac{100}{2 \times 4} \frac{10}{106} \frac{400}{1} = 0.5 \ \mu \text{A/cm}^2$$

From the published data for the GH screen the trace luminance at 10 kV and this screen current density is seen to be 300 nt.

DATA INTERPRETATION FOR RADAR APPLICATIONS

For radar type applications, persistence is of primary importance. For this reason the published information on persistence characteristics of radar screens is more extensive than that provided for other types. The data are prepared from measurements made with a non-interlaced raster. Care is taken to defocus the raster uniformly, so that the individual lines of the raster touch each other. The whole raster is considered as a single pulse, since any given area is excited only once during any one field. 7Z2 5913

To cover a variety of situations, several sets of data are published. Single raster excitations simulate the case of moving targets, when the screen area is excited only once. For permanent echoes and marker pips, there are curves showing persistence with repeated raster excitation. The persistence is measured from the end of excitation. From this information can be derived the variation in trace luminance during normal operation and the screen persistence when changing from one range to another.

The build-up characteristic is important during range-changing. The required information is given by a separate build-up characteristic which shows the luminance of the trace just before the next pulse arrives.

Screen Loading

Consider a small portion of screen under published data conditions. As in previous considerations, the raster area is hl, but only one field of n lines is applied. The current reaching the screen is i, with suitable corrections for flyback times. The spot is defocused so that the lines are touching each other. The charge per unit area reaching the screen is

$$q = \frac{i}{w^2} t_w$$
(32)

and this is proportional to screen luminance Eq (5).

Since

$$t_{w} = t_{1} \frac{w}{1}$$
$$q = \frac{i}{w_{1}} t_{1}$$

also

w =
$$\frac{h}{n}$$
 and $nt_1 = t_r$

therefore

$$q = \frac{i}{hl} t_r$$
(34)

Under p.p.i. conditions Eq (33) is also applicable. In order to express it in terms of p.p.i. constants, let

D = diameter of p.p.i. display

R = range corresponding to the radius of display.

Consider a portion of the display at a distance $\frac{1}{2}D'$ from the centre, so that

$$\frac{D'}{D}$$
 = x and x < 1.

7Z2 5914

(33)

Then the length of considered scan is

$$L = \frac{1}{2}D'.$$

With a signal velocity of 12.3 μ s per loop nautical mile,

$$T_x = 12.3 \text{ x RK10}^{-0} \text{ s.}$$

It was necessary to include a constant K in the equation for T_x in order to take into account overlap of scanning lines of the p.p.i. display. The overlap can be calculated as the ratio of the number of scans per aerial rotation to the number of lines that can be placed on the circumference of the considered portion of display. In terms of p.p.i. data, at a point distant $\frac{1}{2}$ D' from the centre.

$$K_{x} = \frac{F_{p}T_{a}}{\pi x D} W$$

where

 F_p = pulse repetition frequency T_a = time of one aerial revolution.

Substitution of the above data in Eq (33) gives

$$Q_x = \frac{2 I}{\pi x D^2} 12.3 R F_p T_a 10^{-6}.$$

The screen luminance of the p.p.i. display is the same as that in published data if the above equation is equal to Eq (34). Equating and rearranging gives a screen loading of

$$u_x = \frac{i}{hl} = \frac{2I}{\pi x D^2} = 12.3 \text{ R Fp} \frac{T_a}{t_r} 10^{-6}.$$

For published data, $t_r = \frac{1}{50}$ s, therefore

$$u_{\rm X} = \frac{i}{hl} = \frac{3.91}{x D^2} \, IRF_{\rm p}T_{\rm a} \, 10^{-4} \, \mu A/cm^2 \tag{35}$$

Now i/hl is the screen loading used in the presentation of published data, therefore the value of screen persistence can be determined.

It should be noted that u_x varies over the screen. If a constant value of u is required, then a bright-up circuit must be incorporated, so that I/x will be constant.

Single-pulse Excitation: Moving Target Conditions

For fast-moving objects a situation can exist where within one aerial rotation the echo moves on the display a distance greater than the spot diameter of the tube. The persistence curve resulting from such an excitation is given in published data by graphs for single-pulse excitation. The screen loading can be calculated from Eq (35). 7Z2 5915

Repeated-pulse Excitation: Permanent Echoes

The luminance produced by a permanent echo is a result of excitation received from a succession of aerial sweeps. The persistence is given in the published data by graphs for repeated-pulse excitation. The repetition interval t_a of pulses in the published data is 1 s. In practical applications, the aerial rotation frequency may be different, and for that reason the equation for screen loading needs adjustment. Experimental evidence indicates that under the conditions shown in the published data, the screen luminance is a function u of the product of the current and the number of pulses. Thus the necessary adjustment can be effected by multiplying Eq (35) by t_a/T_a . With $t_a = 1$ s, the modified equation becomes

$$U_x = \frac{3.91}{x D^2} IRF_p 10^{-4} \mu A/cm^2$$

Build-up

The rate at which persistence luminance builds up for a permanent echo is shown in published data by means of build-up characteristics. Since these characteristics are given as a function of the number of pulses, the screen loading can be calculated from Eq (36).

Example

A tube with an LD screen is employed in a p.p.i. display. It is operated at 10 kV, and the peak current at the end of the trace is $150 \ \mu$ A. If the pulse repetition frequency is 3 kc/s and the aerial rotational frequency is 20 r.p.m., determine the luminance of the persistence trace at the edge of the display when the display is set to operate at a range of one nautical mile for the full useful screen radius of 10 cm.

(a) Moving targets

2 01

Screen loading is calculated from Eq (35):

$$U_{x} = \frac{3.97}{x D^{2}} IRF_{p}T_{a} 10^{-4} \mu A/cm^{2}$$

$$D = 20 cm \qquad F_{p} = 3 kc/s$$

$$I = 150 \mu A \qquad T_{a} = 3 s$$

$$R = 1 nautical mile \qquad x = 1$$

so that

 $U_x = 1.32 \,\mu A/cm^2$.

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(36)

The persistence characteristics of the LD screen (pages 68 and 69) gives persistence luminance for single-pulse excitation at an e.h.t. of 10 kV. The required persistence can be read off the graph for a screen loading of $1.32 \mu A/cm^2$. This screen loading is higher than any shown on the graph, but the results can be deduced by extrapolation.

(b) Permanent echoes

Screen loading is calculated from Eq (36):

$$U_x = \frac{3.91}{x D^2} IRF_p 10^{-4} \mu A/cm^2.$$

Substitution gives

$$U_{x} = 0.44 \,\mu A/cm^{2}$$
.

This lower value has no actual meaning in terms of current; but it indicates which curve in the graphs on pages 68 or 69 is to be used. The result will apply for a fully built-up condition - say after 60 or more pulses.

(c) Build-up

For any intermediate number of pulses down to about ten, the small variation in the starting point of the decay curves can be obtained from the build-up curve on page 70. The value of $U_x = 0.44 \ \mu A/cm^2$, and the persistence curves for multiple pulse excitation on pages 68 and 69 can then be used.

AMBIENT ILLUMINATION

In the discussion of the requirements of different applications it has been assumed that the only light to be considered is that produced by the display. Background illumination has been altogether neglected. Under practical conditions the background illumination is of the greatest importance. In fact, it determines the luminance that the tube must produce if the display is to be usable.

There are three sources of stray illumination:

Light from the back of the screen is reflected by the tube walls. It returns to the screen in a diffuse form and reduces the contrast between the trace and the unexcited parts of the screen.

Light from the front of the screen is reflected back to the screen from surrounding surfaces. Again the effect is to illuminate the unexcited areas.

Ambient illumination, especially in lighted rooms and in daylight situations, is obviously a major factor in the reduction of contrast.

The minimum contrast perceptible by the eye is about 2 per cent. If the luminance of the trace in the absence of background illumination is B, and the luminance of the rest of the tube face is b, then the luminance of the trace in the presence of the background illumination is B + b. The change in luminance from trace to background is B. For limit perception,

$$\frac{B}{B+b}100 = 2$$

so that

$$B=\frac{b}{49}$$

This is practically the absolute minimum that can be tolerated. For comfortable viewing the contrast should be about 80 per cent; that is, B = 4b. For an oscilloscope display a lower contrast is acceptable than for a raster display.

A laboratory during hours of daylight may have an illumination of about 250 kx. In this illumination a perfectly diffusing surface will have a luminance of $250/\pi$ $\simeq 80$ nt. With transmission and reflection losses of 30 per cent, the tube surface will have a luminance of 56 nt.

For the examples calculated in this chapter we have

| Television monitor tube | 280 nt | | |
|--|--------|--|--|
| Oscilloscope display | 300 nt | | |
| P.P.I. display (permanent echo at 1 s) | 1.3 nt | | |

The contrast for the last case in the presence of a 250 lx background illumination is

 $\frac{1.3}{56}$ 100 = 2.3 %,

which is just about perceptible.

At night an average laboratory will have a lower illumination. If this is, say, 50 lx, the luminance of the radar display quoted will improve, for the contrast will be

$$\frac{1.3}{11.2}100 = 11.6\%.$$

When the decay characteristic is taken into consideration, the effect of ambient illumination is even more serious. If the persistence of the p.p.i. display which has been discussed is plotted in the presence of laboratory illumination as above, the resulting curve will be entirely different from that given on pages 68 and 69 for a current density of $0.2 \,\mu\text{A/cm}^2$. After about seven seconds the display will be lost in the background.

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USE OF FILTERS

Contrast can be improved by placing a filter in front of the tube. Light from outside has to pass through the filter twice before reaching the eye, whereas the light from the trace passes through only once.

For maximum contrast the filter should be as dense as possible; but if the luminance of the trace is already low, it will be attenuated to an unusable level if the filter is too dense. However, a filter whose transmission characteristic is matched to the spectral distribution of the screen will provide differential filtering. The light output from the screen will be transmitted with minimum loss, while external light from other parts of the spectrum will be suppressed.

The GM double-layer screen has a purplish-blue fluorescence and a yellowishgreen phosphorescence. As the blue component is subjectively brighter than the yellow, it is advantageous in some applications to filter it out with a suitable filter if maximum use is to be made of the yellow persistence period. The Chance C2 glass filter is suitable; or, for combination with a graticule, a sheet of amber Perspex may be used.

Exclusion of ambient ultraviolet radiation from the GN storage screen is provided by filters such as the llford 108. The infrared radiation for reading can be obtained from low-power tungsten lamps. They should be provided with filters to suppress the visible light which would reduce contrast. A combination of the llford filters 207 and 813 is suitable. A composite viewing hood can be used, containing the lamps, filters, and ultraviolet stop filter.

GENERAL DATA

The information given in this reference section is obtained from measurements of phosphors settled in typical cathode ray tubes. The tube used is, of course, of a type appropriate for the screen in question.

For each screen type there is a spectral response curve. The relative response is plotted against the wavelength of the light output, the peak light output being shown as 100 per cent. No absolute values of light output can be read off; and no comparisons of the luminance of different screen types can be made from these curves.

On each response curve is quoted the subjective colour sensation in terms of the x-y co-ordinates of the C.I.E. system. These points are also indicated on the diagram.

For two or three screen types, the diagram shows two points: one refers to the initial "flash" or fluorescence, while the other point refers to the persistence (phosphorescence) colour. Thus, the GM screen has a purplish-blue flash and a yellowish-green persistence, and it is classified as a screen of the G group. The two linked points shown for the GH screen are those pertaining to high-brilliance and low-brilliance operation.

For comparison of the spectral response of the screens available for each of the main groups of application, collective response curves, are given. Here again, the response curves are normalised, and they provide no information about the comparative light outputs of different screens.

The Kelly charts are marked - in accordance with general colorimetric practice - with the wavelengths in milli-micrometres ($m\mu m$) that correspond to the saturated spectral colours lying on the perimeter.

The persistence and efficiency curves, and the special curves relating to radar screens, should be read in conjunction with the relevant parts of the text.

PERSISTENCE NOMOGRAPHS FOR OSCILLOSCOPE SCREENS

Although the persistence curves give a good indication of the differences between screens under typical conditions, it is found in practice that the operation of the screen is often far removed from the published conditions. This is especially so for oscilloscope applications. With this as a prime consideration, the screens most used for oscilloscope work have been investigated in rather more detail than, say, the screens used in television monitors.

7Z2 5920

Radar screens, although subjected to some changes in operation conditions, are limited in their applicational range, and in most cases the published curves give adequate information. The flying spot screen BA has only a small dynamic characteristic change, and once again requires no elaboration.

Most oscilloscope screens have a persistence dependent on current density, electron energy, excitation time, and repetition frequency. The exception to this is the GJ screen which has a decay law of the form exp (-80 t) which is independent of the above characteristics and is therefore specified by the published decay curve. The dynamic range of the other oscilloscope screens has been evaluated empirically.

The BE and GH screens have a common decay law:

 $L_t \propto t_p^{-1}$

where Lt is the light output at a time tp during the decay.

Experiment has shown that modification to the form

$$\frac{L_{t}}{L_{0}} = \frac{k}{t_{p} + k}$$

where

 L_0 = initial light output at $t_p = 0$ k = a constant

produces a good approximation to the practical persistence curve.

Incorporation of some of the relevant screen characteristics gives

$$t_{p} = \left[\gamma(I_{b}/a)\beta t_{e}^{\alpha(k - \tan^{-1} s \log \frac{I_{b}/a}{q})}\right](\frac{L_{o}}{L_{t}} - 1)$$

where

t_e = excitation time Ib/a = beam current density

and the constants α , β , γ , k, s, and q have been evaluated for each screen type.

Voltage and repetition frequency are not included in this formula. The voltage has little effect on persistence if it exceeds 3 kV. Below 3 kV the persistence increases. The repetition frequency has a pronounced effect; but, because of the complexity of interrelating occupance and build-up time limits, the formula in its present form applies only for single or low-occupance occurrences.

To simplify the use of the equation, nomographs have been constructed in which the variables are light output (as a percentage of flash), excitation time, and persistence. Current density is introduced as a parameter. Nomographs for the BE and GH screens are given. Each nomograph consists of three main scales: t_e (excitation time), t_p (decay time), and L_t/L_0 per cent (decay percentage). The t_e and t_p scales are split into three, for various current densities. As the current density has a second-order effect, the range over which the scales may be used is denoted at the foot of the scale.

To use the nomograph, a straight edge is placed across the sheet against the two known variables, and the third variable is read off. For example:

What is the persistence of the GH screen at 0.5 per cent of flash under the following conditions.

Excitation time = $10 \ \mu s$ Current density = $0.8 \ \mu A/mm^2$

A straight-edge placed against $L_t/L_o = 0.5$ per cent and $t_e = 10 \ \mu s$ on the > 0.8 $\mu A/mm^2$ scale will intersect the > 0.8 $\mu A/mm^2 t_p$ scale at 0.9 ms. Thus the persistence is 0.9 ms to 0.5 per cent under this condition.

Excitation time is determined, in practice, by dividing the spot diameter by the spot velocity. That is,

$$t_e = \frac{d}{v}$$

where

d = spot diameter (mm)
v = spot velocity (mm/s)

A maximum limit for t_e occurs when build-up is accomplished by steady excitation, or when the time occupance approaches unity. This maximum limit is indicated by the discontinuation of the t_e scale at its top end. Thus for excitation times greater than the limit value, the limit value should be used.

The reading accuracy of the nomographs has been reduced by including only the scale intervals of 5 and 10 on the logarithmic t_p and t_e scales. The reasons for this are that the nomograph includes several approximations, and, secondly, unavoidable spreads in screen production may cause significant deviations. This spread has less significance when the wide dynamic range covered by the logarithmic characteristics is being considered.

No nomograph is given for the GM screen, since the interdependent characteristics of the two phosphor layers are too complex for this kind of presentation.

7Z2 5922

-

designation equivalent Jedec P32 P24 P33 P22 P11 P31 P4 Pl 1 P2P7 P2 1 medium short medium short medium short (fluorescence) medium short medium short medium short persistence very short very short very long very long medium medium medium medium killed short long long long yellowish-orange phosphorescent yellowish-green yellowish-green yellowish-green yellowish-green yellowish-green green (infrared colour excited) orange orange orange or ange green green green blue tri-colour screen yellowish-orange yellowish-green yellowish-green yellowish-green fluorescent purplish-blue purplish-blue purplish-blue purplish-blue purplish-blue bluish-green colour or ange or ange orange or ange green green white blue blue blue system old G1) Σ D H 0 Z L M U 2 X E EL. B × system new GE GH GL GM GN LA LB LC TD YA BC GB GK GP BA BD BE BF 5 M ×

7Z2 5923

1) used in projection tubes

SCREEN TYPES



Kelly Chart











BC SCREEN 7Z04510 T CIE co-ordinates x=0.170 y=0.024 (%) 100 Relative response 80 60 40 20 -0 Q35 0.5 λ (µm) 0.4 0.45 0.55

BC SCREEN



BD SCREEN



BE SCREEN





BF SCREEN





12.12.1965





GE SCREEN





GH SCREEN









GL SCREEN





GM SCREEN










GM SCREEN





GM











LB SCREEN













LB SCREEN



LC SCREEN











IC







7Z04620 excitation (sec) : Pulse of 1 field duration repeated scanned at every second for 60 seconds. 20 190 lines, defocused, 50 fields per second. Vscreen : 10 kV Temperature: 20 °C Raster : 200 mm x 100 mm, cessation of 8 2 Excitation Time after 5 WARD in sur -Querens SUA 5 101 0.5 0.05 0.03 0.01 5 3 0.2 0.1 (Siin) asnonice (nits) 200 Time after cessation of excitation (sec) 7Z04621 -50 fields per second. : Pulse of 1 field duration repeated scanned at every second for 60 seconds. 50 190 lines, defocused, : 200 mm x 100 mm, 20 Vscreen : 15 kV Temperature: 20 oC 2 Excitation Raster 5 WALCH Street of the state -03414 Cm3+ COJUM KEN 2-02 5 (uits) 0.5 0.3 0.1 0.05 0.02 aor

12.12.1965

69

LD SCREEN



SCREEN

ID









SCREEN









INSTRUMENT CATHODE-RAY TUBE

Oscilloscope tube with 10 cm diameter flat face-plate and post deflection acceleration by means of a helical electrode. The low heater consumption together with the high sensitivity and short overall length render this tube suitable for transistorised equipment.

| | QUICK | REFERENCE DAT. | A | | | · // |
|--------------------|------------|----------------|----------------|----|---------|------|
| Final accelerator | voltage | | $V_{g_6(l)}$ | = | 4 | kV |
| Display area | horizontal | | | fu | ll scan | |
| | vertical | 44.1 - 4 14 | | = | 6 | cm |
| Deflection factor, | horizontal | | M _x | = | 27.5 | V/cm |
| | vertical | | My | = | 9.8 | V/cm |

SCREEN

| | Colour | Persistence |
|----------|-----------------|--------------|
| D10-11BE | blue | medium short |
| D10-11GH | green | medium short |
| D10-11GM | yellowish green | long |
| D10-11GP | bluish green | medium short |

Useful screen diameter

min. 85 mm

Useful scan at $V_{g6(l)}/V_{g4} = 4$

horizontal

full scan

vertical

min. 60 mm

The useful scan may be shifted vertically to a max. of 4 mm with respect to the geometric centre of the faceplate.

HEATING

Indirect by A.C. or D.C.; parallel supply

Heater voltage Heater current $\frac{V_{f}}{I_{f}} = \frac{6.3}{95} \frac{V}{mA}$ 7Z2 7719



Mounting position: any

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

Base 14 pin all glass

Dimensions and connections

| Overall length (also inclusive socket type 555 | 66) | max. | 320 | mm |
|--|-----|---------|------|----|
| Face diameter | | max. | 102 | mm |
| Net weight | | approx. | 480 | g |
| Accessories | | | | |
| Socket (supplied with the tube) | | type 53 | 5566 | |
| Final accelerator contact connector | | type 55 | 5560 | |
| Mu-metal shield | | type 55 | 5541 | |
| | | | | |

| CAPACITANCES | | | | | |
|--|--------------------|---|-----|----|--|
| \mathbf{x}_1 to all other elements except \mathbf{x}_2 | $C_{x_1(x_2)}$ | = | 3.5 | pF | |
| \mathbf{x}_2 to all other elements except \mathbf{x}_1 | $C_{x_2(x_1)}$ | = | 3.5 | pF | |
| y_1 to all other elements except y_2 | $C_{y_1(y_2)}$ | = | 2.5 | pF | |
| y_2 to all other elements except y_1 | $C_{y_2(y_1)}$ | = | 3.0 | pF | |
| \mathbf{x}_1 to \mathbf{x}_2 | $\dot{c}_{x_1x_2}$ | = | 2.0 | pF | |
| y_1 to y_2 | $C_{y_1y_2}$ | = | 1.7 | pF | |
| Control grid to all other elements | C _{g1} | = | 4.5 | pF | |
| Cathode to all other elements | Ck | = | 3.0 | pF | |
| | | | | | |

FOCUSING

electrostatic

double electrostatic

| DEFLECTION | |
|------------|--|
|------------|--|

x plates symmetrical

y plates symmetrical

If use is made of the full deflection capabilities of the tube the deflection plates will intercept part of the electron beam; hence a low impedance deflection plate drive is desirable.

Angle between x and y traces

 $90^{\circ} \pm 1^{\circ}$

LINE WIDTH

Measured with the shrinking raster method in the centre of the screen

| Final accelerator voltage | $V_{g_6(l)}$ | = | 4000 | V |
|---------------------------------------|--------------|---|------|------|
| Astigmatism control electrode voltage | Vg4 | = | 1000 | V 2) |
| First accelerator voltage | Vg2 | = | 1000 | V |
| Beam current | I(() | = | 10 | μA |
| Line width | 1.w. | = | 0.35 | mm |

HELIX

Post deflection accelerator helix resistance = min. 50 M Ω

2) See page 5

| TYPICAL OPERATING CONDITIONS | | | | | |
|--|------------------|-----|------------|-----|------------------|
| Final accelerator voltage | Vg6(l) | = | 4 | 000 | V |
| Geometry control electrode voltage | Vg5 | . = | $1000 \pm$ | 100 | V ¹) |
| Astigmatism control electrode voltage | Vg4 | = | $1000 \pm$ | 50 | v ²) |
| Focusing electrode voltage | V _{g3} | = | 50 to | 200 | V |
| First accelerator voltage | v _{g2} | = | 1 | 000 | V |
| Control grid voltage for visual extinction of focused spot | -V _{g1} | = | 25 to | 67 | v |
| Deflection factor | | | | | |
| horizontal | $M_{\mathbf{x}}$ | = | 24 to | 31 | V/cm |
| vertical | My | = | 8.6 to | 11 | V/cm |
| Deviation of linearity of deflection | | = | max. | 2 | % ³) |
| Geometry distortion | | Se | ee note 4 | | |
| Useful scan | | | | | |
| horizontal | | fu | ll scan | | |
| vertical | | = | min. | 60 | mm |

CIRCUIT DESIGN VALUES

| Focusing voltage | v _{g3} | = | 50 | to | 200 | V per kV of V _{g4} |
|--|-----------------|---|-----|----|-----|-----------------------------|
| Control grid voltage for visual extinction of focused spot | -Vg1 | = | 25 | to | 67 | V per kV of V_{g_2} |
| Deflection factor at | | | | | | |
| $V_{g_{6}(l)}/V_{g_{4}} = 4$ | | | | | | |
| horizontal | M _x | = | 24 | to | 31 | V/cm per kV of V_{g_4} |
| vertical | My | = | 8.6 | to | 11 | V/cm per kV of V_{g_4} |
| Control grid circuit resistance | Rg1 | = | max | | 1.5 | ΜΩ |
| Focusing electrode current | Ig3 | = | -30 | to | +30 | μΑ 5) |

 $(1)^{2})^{3})^{4})^{5}$) See page 5

| Final accelerator voltage $V_{g_6(l)} = mi$ | .x. 5000 n. 1500 | V V |
|--|---------------------|--------------------|
| Geometry control electrode voltage V_{g_5} = ma | x. 2200 | v |
| Astigmatism control electrode voltage $V_{g_4} = ma$ | n. 2200 | V V |
| Focusing electrode voltage V_{g_3} = ma | x. 1500 | v |
| First accelerator voltage V_{g_2} = ma | x. 2200 | V |
| Control grid voltage negative $-V_{g_1} = ma$ | . 200 | v |
| positive V _{g1} = ma | 1x. 0 | v · |
| Cathode to heater voltage cathode positive V+k/f- = ma | 100 x. | v |
| cathode negative $V-k/f+$ = ma | ix. 15 | V |
| Voltage between astigmatism control electrode and any deflection plate $V_{g_4/x} = ma$ | ix. 500 | v |
| V _{g4/y} = ma | 1x. 500 | V |
| Cathode current, average I_k = ma | 1x. 300 | μA |
| Screen dissipation W_{ℓ} = ma | ıx. 3 | mW/cm ² |
| Ratio $V_{g_6(\ell)}/V_{g_4}$ $V_{g_6(\ell)}/V_{g_4} = ma$ | ux. 4 | |
| Ratio V_{g_2}/V_{g_4} $V_{g_2}/V_{g_4} = ma$ | n. 1 | |

- 1) This tube is designed for optimum performance when operating at the ratio $V_{g6(\ell)}/V_{g4} = 4$. Operation at other ratio may result in changes in deflection uniformity and geometry distortion. The geometry control electrode voltage should be adjusted for optimum performance. For any necessary adjustment its potential will be within the stated range.
- 2) The astigmatism control electrode voltage should be adjusted for optimum spot shape. For any necessary adjustment its potential will be within the stated range.
- 3) The sensitivity at a deflection of less than 75% of the useful scan will not differ from the sensitivity at a deflection of 25% of the useful scan by more than the indicated value.
- ⁴) A graticule, consisting of concentric rectangles of 50 mm x 60 mm and 48.4 mm x 58.4 mm is aligned with the electrical x axis of the tube. The edges of a raster will fall between these rectangles with optimum correction potentials applied.
- 4) Values to be taken into account for the calculation of the focus potentiometer.



INSTRUMENT CATHODE-RAY TUBE

Oscilloscope tube with 10 cm diameter flat faceplate and post deflection acceleration by means of a helical electrode. The tube is intended for small compact oscilloscopes.

| | QUICK REFERENCE | DATA | | |
|--------------------|-----------------|--------------------|---|-----------|
| Final accelerator | voltage | V _{g6(1)} | = | 4000 V |
| Display area | horizontal | | = | full scan |
| | vertical | | = | 6 cm |
| Deflection factor, | horizontal | M _x | = | 27.5 V/cm |
| | vertical | My | = | 9.8 V/cm |

SCREEN

| 0 | Colour | Persistence |
|----------|-----------------|--------------|
| D10-12BE | blue | medium short |
| D10-12GH | green | medium short |
| D10-12GP | bluish green | medium short |
| D10-12GM | yellowish green | long |

Useful screen diameter

min. 85 mm

Useful scan at $V_{g_6(l)}/V_{g_4} = 4$

horizontal full scan vertical min. 60 mm

The useful scan may be shifted vertically to a max. of 4 mm with respect to the geometric centre of the faceplate.

HEATING

Indirect by A.C. or D.C.; parallel supply

Heater voltage Heater current $\frac{V_{f}}{I_{f}} = \frac{63}{300} \frac{V}{mA}$ 7Z2 5501



Mounting position: any

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

| Base | 14 pin al | ll glass |
|------|-----------|----------|
|------|-----------|----------|

Dimensions and connections

| Overall length (inclusive socket 55566) | max. | 320 | mm |
|---|-------|--------|----|
| Face diameter | max. | 102 | mm |
| Net weight | appro | x. 480 | g |
| Accessories | | | |
| Socket (supplied with the tube) | type | 55566 | |
| Final accelerator contact connector | type | 55560 | |
| Mu-metal shield | type | 55541 | |
| | | | |

CAPACITANCES

| x_1 to all other elements except x_2 | $C_{x_1(x_2)}$ | = | 4.0 | pF |
|--|-----------------------------------|---|-----|----|
| x_2 to all other elements except x_1 | $C_{x_2(x_1)}$ | = | 4.0 | pF |
| y_1 to all other elements except y_2 | $C_{y_1(y_2)}$ | = | 3.0 | pF |
| y_2 to all other elements except y_1 | Cy ₂ (y ₁) | = | 3.0 | pF |
| x1 to x2 | $C_{x_1x_2}$ | = | 2.0 | pF |
| y ₁ to y ₂ | $C_{y_1y_2}$ | = | 1.7 | pF |
| Control grid to all other elements | C _{g1} | = | 5.0 | pF |
| Cathode to all other elements | Ck | = | 3.0 | pF |

FOCUSING

electrostatic

| DEFLECTION | double electrostatic | |
|------------|----------------------|--|
| x plates | symmetrical | |
| y plates | symmetrical | |

If use is made of the full deflection capabilities of the tube the deflection plates will intercept part of the electron beam; hence a low impedance deflection plate drive is desirable.

Angle between x and y traces

 $90^{\circ} \pm 1^{\circ}$

LINE WIDTH

Measured with the shrinking raster method in the centre of the screen

| Final accelerator voltage | $V_{g_6(l)}$ | = | 4000 | V |
|---------------------------------------|--------------|---|------|------------------|
| Astigmatism control electrode voltage | Vg4 | = | 1000 | v ²) |
| First accelerator voltage | v_{g_2} | = | 1000 | v |
| Beam current | I(l) | = | 10 | μA |
| Line width | 1.w. | = | 0.35 | mm |

HELIX

Post deflection accelerator helix resistance min. 50 $M\Omega$

2) See page 6

| TYPICAL OPERATING CONDITIONS | | | | | |
|--|------------------|----|---------------|-----|------------------|
| Final accelerator voltage | $V_{g_6(l)}$ | = | 40 | 000 | V |
| Geometry control electrode voltage | V _{g5} | = | 1000 ± | 100 | V 1) |
| Astigmatism control electrode voltage | Vg4 | = | 1000 <u>+</u> | 50 | V ²) |
| Focusing electrode voltage | Vg ₃ | = | 50 to 2 | 200 | V |
| First accelerator voltage | Vg2 | := | 10 | 000 | V |
| Control grid voltage for visual extinction of focused spot | -V _{g1} | = | 25 to | 67 | v |
| Deflection factor | | | | | |
| horizontal | M _x | = | 24 to | 31 | V/cm |
| vertical | My | = | 8.6 to | 11 | V/cm |
| Deviation of linearity of deflection | | = | max. | 2 | % ³) |
| Geometry distortion | | | See note | 4 | |
| Useful scan | | | | | |
| horizontal | | = | full scan | | |
| vertical | | = | min. | 60 | mm |

CIRCUIT DESIGN VALUES

| Focusing voltage | Vg3 | Ξ | 50 to | 200 | V per kV of V_{g_4} |
|--|------------------|---|--------|-----|--------------------------|
| Control grid voltage for visual extinction of focused spot | -V _{g1} | = | 25 to | 67 | V per kV of V_{g_2} |
| Deflection factor at | | | | | |
| $V_{g_6(l)}/V_{g_4} = 4$ | | | | | |
| horizontal | $M_{\rm X}$ | = | 24 to | 31 | V/cm per kV of V_{g_4} |
| vertical | My | = | 8.6 to | 11 | V/cm per kV of Vg4 |
| Control grid circuit resistance | Rg1 | = | max. | 1.5 | MΩ |
| Focusing electrode current | Ig3 | = | -30 to | +30 | μA ⁵) |
| | | | | | |

¹)²)³)⁴)⁵) See page 6
D10-12..

| LIMITING VALUES (Absolute max. rati | ng system) | | | | |
|--|----------------------|---|--------------|--------------|--------------------|
| Final accelerator voltage | $V_{g_6(l)}$ | = | max. min. | 5000 1500 | V V |
| Geometry control electrode voltage | vg5 | = | max. | 2200 | V |
| Astigmatism control electrode voltage | vg4 | | max. min. | 2200 900 | V V |
| Focusing electrode voltage | Vg3 | = | max. | 1500 | v |
| First accelerator voltage | Vg2 | = | max. | 2200 | V |
| Control grid voltage | | | | | |
| negative | $-v_{g_1}$ | = | max. | 200 | v |
| positive | v_{g_1} | = | max. | 0 | V |
| Cathode to heater voltage | | | | | |
| cathode positive | V+k/f- | = | max. | 200 | V |
| cathode negative | V-k/f+ | = | max. | 125 | V |
| Voltage between astigmatism control electrode and any deflection plate | Vg4/x | = | max. | 500 | v |
| | Vg4/y | = | max. | 500 | V |
| Screen dissipation | We | = | max. | 3 | mW/cm ² |
| Ratio $V_{g_6(\ell)}/V_{g_4}$ | $v_{g_6(l)}/v_{g_4}$ | = | max. | 4 | |
| Ratio V_{g_2}/V_{g_4} | V_{g_2}/V_{g_A} | = | max. | 1 | |

7Z2 5505

5

- ¹) This tube is designed for optimum performance when operating at the ratio $V_{g_6}(\ell)/V_{g_4} = 4$. Operation at other ratio may result in changes in deflection uniformity and geometry distortion. The geometry control electrode voltage should be adjusted for optimum performance. For any necessary adjustment its potential will be within the stated range.
- ²) The astigmatism control electrode voltage should be adjusted for optimum spot shape. For any necessary adjustment its potential will be within the stated range.
- ³) The sensitivity at a deflection of less than 75% of the useful scan will not differ from the sensitivity at a deflection of 25% of the useful scan by more than the indicated value.
- ⁴) A graticule, consisting of concentric rectangles of 50 mm x 60 mm and 48.4 mm x 58.4 mm is aligned with the electrical x axis of the tube. The edges of a raster will fall between these rectangles with optimum correction potentials applied.
- 5) Values to be taken into account for the calculation of the focus potentiometer.

INSTRUMENT CATHODE-RAY TUBE

13 cm diameter flat faced oscilloscope tube with thin metal backing and post deflection acceleration by means of a helical electrode.

| QUICK REFERENCE DATA | | | | | |
|-------------------------------|---------------------|---|---------------|------|--|
| Final accelerator voltage | V _{g7} (1) | = | 4000 | V | |
| Display area | | = | 6 x 10 | cm | |
| Deflection factor, horizontal | M _x | = | 22.9 | V/cm | |
| vertical | My | = | 5.9 | V/cm | |

SCREEN

| | Colour | Persistence |
|----------|-----------------|--------------|
| D13-15BE | blue | medium short |
| D13-15GH | green | medium short |
| D13-15GP | bluish green | medium short |
| D13-15GM | yellowish green | long |

Useful screen diameter

Useful scan at $V_{g_7(\ell)}/V_{g_4} = 2$

| orizontal | min. | 100 | mm | |
|-----------|------|-----|----|--|
| vertical | min. | 60 | mm | |

The useful scan may be shifted vertically to a max. of 4 mm with respect to the geometric centre of the faceplate.

HEATING

Indirect by A.C. or D.C.; parallel supply

Heater voltage

Heater current

 $\frac{V_f}{I_f} = 6.3 V$

114

min.

mm

MECHANICAL DATA (Dimensions in mm)

- 1) Straight part of the bulb.
- 2) Location of the recessed cavity button contact with respect to the x-trace.



133±1.5

7726

Mounting position : any

Base

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

Diheptal medium shell

Dimensions and connections

| Overall length Face diameter | max. max. l | 468 mm 34.5 mm | |
|-------------------------------------|----------------|-------------------|-----|
| Net weight | approx. | 910 g | |
| Accessories | | | |
| Socket | type | 5914/20 | |
| Final accelerator contact connector | type | 55560 | |
| Side contact connector | type | 55561 | |
| Mu-metal shield | type | 55551 | |
| | | | 7Z2 |

CAPACITANCES

 x_1 to all other elements except x_2 x_2 to all other elements except x_1 y_1 to all other elements except y_2 y_2 to all other elements except y_1 x_1 to x_2 y_1 to y_2 Control grid to all other elements FOCUSING electrostatic

Cathode to all other elements

| DEFI | ECTION | |
|------|--------|--|

x plates symmetrical

y plates symmetrical

If use is made of the full deflection capabilities of the tube the deflection plates will intercept part of the electron beam; hence a low impedance deflection plate drive is desirable.

Angle between x and y traces

 $90^{\circ} \pm 1^{\circ}$

LINE WIDTH

Measured with the shrinking raster method in the centre of the screen

double electrostatic

| Final accelerator voltage | $V_{g7(l)}$ | = | 4000 | V |
|---------------------------------------|-------------|---|------|------------------|
| Astigmatism control electrode voltage | vg4 | = | 2000 | v ³) |
| First accelerator voltage | Vg2 | = | 2000 | V |
| Beam current | I(() | = | 10 | μA |
| Line width | l.w. | = | 0.5 | mm |

HELIX

Post deflection accelerator helix resistance min. 300 M Ω

3) See page 6

| TYPICAL OPERATING CONDITIONS | |
|--|---|
| Final accelerator voltage | $V_{g_7(\ell)} = 4000 V$ |
| Geometry control electrode voltage | $V_{g_6} = 2000 \pm 200 V^1$) |
| Deflection plate shield voltage | $V_{g_5} = 2000 V^2$) |
| Astigmatism control electrode voltage | $V_{g_4} = 2000 \pm 100 \text{ V}^3$) |
| Focusing electrode voltage | $V_{g_3} = 220 \text{ to } 710 \text{ V}$ |
| First accelerator voltage | $V_{g_2} = 2000 V$ |
| Control grid voltage for visual extinction of focused spot | $-V_{g_1} = 60 \text{ to } 96 \text{ V}$ |
| Deflection factor | |
| horizontal | $M_{\rm X}$ = 19.8 to 26.5 V/cm |
| vertical | $M_y = 5.1 \text{ to } 6.7 \text{ V/cm}$ |
| Deviation of linearity of deflection | $=$ max. 2 $\%^4$) |
| Geometry distortion | See note 5 |
| Useful scan | |
| horizontal | = min. 100 mm |
| vertical | = min. 60 mm |

CIRCUIT DESIGN VALUES

| Focusing voltage | Vg3 | = | 110 to | 355 | V per kV of V_{g_4} |
|---|------------|---|---------|------|--------------------------|
| Control grid voltage for visual | | | | | |
| extinction of focused spot | $-v_{g_1}$ | = | 30 to | 48 | V per kV of V_{g_2} |
| Deflection factor at $V_{g7(\ell)}/V_{g_4} = 2$ | | | | | |
| horizontal | M_{x} | = | 11.9 to | 15.6 | V/cm per kV of V_{g_4} |
| vertical | My | = | 3.3 to | 4.0 | V/cm per kV of V_{g_4} |
| Control grid circuit resistance | R_{g_1} | = | max. | 1.5 | MΩ |
| Deflection plate circuit | | | | | |
| resistance | R_x, R_y | = | max. | 5 | MΩ |
| Focusing electrode current | I_{g_3} | = | -15 to | +10 | μA ⁶) |

¹)²)³)⁴)⁵)⁶) See page 6

| LIMITING VALUES (Absolute max. rat | ing system) | | | | |
|--|-------------------------|-----|--------------|--------------|--------------------|
| Final accelerator voltage | V _{g7(1)} | п | max. min. | 8800 2500 | V V |
| Geometry control electrode voltage | Vg ₆ | = | max. | 2200 | v |
| Deflection plate shield voltage | Vg5 | = | max. | 2200 | V |
| Astigmatism control electrode voltage | Vg4 | н н | max. min. | 2200 1000 | V V |
| Focusing electrode voltage | Vg3 | = | max. | 1500 | v |
| First accelerator voltage | Vg ₂ | = | max. | 2200 | V |
| Control grid voltage | | | | | |
| negative | $-V_{g_1}$ | = | max. | 200 | V |
| positive | Vg1 | = | max. | 0 | V |
| positive peak | Vg _{1p} | = | max. | 2 | V |
| Cathode to heater voltage | -1 | | | | |
| cathode positive | V+k/f- | = | max. | 200 | V |
| cathode negative | V-k/f+ | = | max. | 125 | V |
| Voltage between astigmatism control electrode and any deflection plate | V _g /x | = | max. | 500 | V |
| | V _g /v | = | max. | 500 | v |
| Screen dissipation | Wl | = | max. | 3 | mW/cm ² |
| Ratio Vg7(1)/Vg4 | $V_{g_7(\ell)}/V_{g_4}$ | = | max. | 4 | |
| Ratio V_{g_2}/V_{g_4} | v_{g_2}/v_{g_4} | = | max. | 1 | |
| | | | | | |

- ¹) This tube is designed for optimum performance when operating at the ratio $V_{g7(\ell)}/V_{g2} = 2$. Operation at higher ratio may result in changes in deflection uniformity and geometry distortion. The geometry control electrode voltage should be adjusted for optimum performance. For any necessary adjustment its potential will be within the stated range.
 - ²) This voltage should be equal to the mean x- and y plates potential.
 - 3) The astigmatism control electrode voltage should be adjusted for optimum spot shape. For any necessary adjustment its potential will be within the stated range.
 - ⁴) The sensitivity at a deflection of less than 75% of the useful scan will not differ from the sensitivity at a deflection of 25% of the useful scan by more than the indicated value.
 - ⁵) A graticule, consisting of concentric rectangles of 60 mm x 100 mm and 58.5 mm x 98 mm is aligned with the electrical x axis of the tube. The edges of a raster will fall between these ractangles with optimum correction potentials applied.
 - 6) Values to be taken into account for the calculation of the focus potentiometer. 7Z2 5512

INSTRUMENT CATHODE-RAY TUBE

Oscilloscope tube with flat 13 cm diameter face, post deflection acceleration by means of a helical electrode, metal backed screen, deflection blanking and sectioned y deflector plates. The tube is designed to display high frequencies combined with a high writing speed.

| QUICK REFERENCE DATA | | | |
|-------------------------------|-----------------|---------|------|
| Final accelerator voltage | $V_{g_9}(\ell)$ | = 10 | kV |
| Display area | | = 6x10 | cm |
| Deflection factor, horizontal | M _X | max. 18 | V/cm |
| vertical | My | = 6 | V/cm |

SCREEN

| | Colour | Persistence |
|----------|--------------|--------------|
| D13-16BE | blue | medium short |
| D13-16GH | green | medium short |
| D13-16GP | bluish green | medium short |

| Useful screen diameter | | min. | 114 | mm | |
|--|---|------|-----|----|--|
| Useful scan at $V_{g_9(\ell)}/V_{g_5}$ = | 6 | | | | |
| horizonta | 1 | min. | 100 | mm | |
| vertical | | min. | 60 | mm | |

HEATING

Indirect by A.C. or D.C.; parallel supply

Heater voltage

Heater current

 $\frac{V_f}{I_f} = 6.3 V}{I_f} = 300 mA$

7Z2 7859



The socket should under no circumstances be used to support the tube.

Base

1 A 14 pin all glass

Dimensions and connections

| Overall length (inclusive socket 55566) | max. | 600 | mm |
|---|---------|-------|----|
| Face diameter | max. | 134.5 | mm |
| Net weight: | approx. | 1300 | g |
| Accessories | | | |
| Socket (supplied with tube) | type | 55566 | |
| Final accelerator contact connector | type | 55563 | |
| Side contact connector | type | 55561 | |
| Mu-metal shield | type | 55554 | 4) |

1) Straight part

²) The tolerance of the position of the neck pins with respect to the x-trace is $+ 2^{\circ}$.

³) The tolerance of the position of the base pins with respect to the x-trace is $\pm 10^{\circ}$. 7Z2 7860

4) See page 6.

| CAFACITANCES | | | | |
|---|--|---|-----|----|
| \mathbf{x}_1 to all other elements except \mathbf{x}_2 | C _{x1} (x ₂) | = | 2.8 | pF |
| \mathbf{x}_2 to all other elements except \mathbf{x}_1 | C _{x2} (x1) | = | 2.8 | pF |
| y _{1.1} to all other elements except y ₂ ,y _{1.2} ,y _{1.3} ,y _{1.4} | ^C y _{1.1} (y ₂ , y _{1.2} , y _{1.3} , y _{1.4}) | = | 1.6 | pF |
| y _{2.1} to all other elements except y ₁ ,y _{2.2} ,y _{2.3} ,y _{2.4} | $C_{y_{2,1}(y_1, y_{2,2}, y_{2,3}, y_{2,4})}$ | = | 1.6 | pF |
| x_1 to x_2 | $C_{x_1x_2}$ | = | 2.3 | pF |
| y _{1.1} to y _{2.1} | C _{y1.1} ,y _{2.1} | = | 0.7 | pF |
| Control grid to all other elements | Cg1 | = | 5.0 | pF |
| Cathode to all other elements | Ck | = | 3.0 | pF |
| g ₃ to all other elements | Cg3 | = | 9 | pF |
| FOCUSING electrostatic | | | | |
| DEFLECTION double electro | ostatic | | | |

| DEFLECTION | double electrostati |
|------------|---------------------|
| x plates | symmetrical |
| y plates | symmetrical |

If use is made of the full deflection capabilities of the tube the deflection plates will intercept part of the electron beam near the edge of the scan, hence a low impedance deflection plate drive is desirable.

Angle between x and y traces 90° See "Correction Coils"

LINE WIDTH

CADA OFTANOTO

Measured with the shrinking raster method in the centre of the screen

| Final accelerator voltage | $V_{g_9}(l)$ | = | | 10 000 | V |
|---------------------------------------|-----------------|---|------|--------|------------------|
| Astigmatism control electrode voltage | Vg5 | = | | 1670 | V ⁵) |
| First accelerator voltage | Vg2 | = | | 1670 | V |
| Beam current | $I_{g_9}(\ell)$ | = | | 10 | μA |
| Line width | 1.w. | = | | 0.35 | mm |
| HELIX | | | | | |
| Post deflection acc. helix resistance | | | min. | 300 | MΩ |
| | | | | | |

The helix is connected between $g_9(l)$ and g_8

5) See page 6

| Vg9(1) | (± 0) | 10 000 | V |
|----------------------------|---|--|---|
| Vg8 | = | 1670 + 100 | V ¹) |
| Vg7 | = 0 | 1670 | V ²) |
| Vg6 | = | 1670 + 20 | V ³) |
| Vg5 | =() | 1670 + 100 | V 5) |
| Vg4 | = | 230 to 500 | V |
| Vg3 | = | 1670 | V |
| ΔV_{g_3} | = | max. 60 | V 6) |
| Vg2 | = | 1670 | V |
| -Vg1 | = | 50 to 120 | V |
| tal model | | | |
| M_X | = | max. 18 | V/cm |
| My | = | 5.6 to 6.6 | V/cm |
| a service and the | = | max. 2 | % ⁷) |
| See note | e 8 | | |
| na nanga 11. Na kata na | | | |
| | = | 100 | mm |
| | = | 60 | mm |
| | $v_{g_9}(t)$ v_{g_8} v_{g_7} v_{g_6} v_{g_5} v_{g_4} v_{g_3} Δv_{g_3} v_{g_2} $-v_{g_1}$ M_x M_y See note | $V_{g_9}(l) = V_{g_8} = V_{g_7} = V_{g_7} = V_{g_6} = V_{g_5} = V_{g_4} = V_{g_3} = V_{g_3} = V_{g_2} = -V_{g_1} = M_x = M_y = M_y = See note 8$ | $V_{g_9}(t) = 10000$ $V_{g_8} = 1670 + 100$ $V_{g_7} = 1670$ $V_{g_6} = 1670 + 20$ $V_{g_5} = 1670 + 100$ $V_{g_4} = 230 \text{ to } 500$ $V_{g_3} = 1670$ $\Delta V_{g_3} = \text{max. } 60$ $V_{g_2} = 1670$ $-V_{g_1} = 50 \text{ to } 120$ $M_x = \text{max. } 18$ $M_y = 5.6 \text{ to } 6.6$ $= \text{max. } 2$ See note 8 $= 100$ $= 60$ |

| LIMITING VALUES (Absolute limits) | | | | | |
|--|----------------------------|-----|--------------|---------------|--------------------|
| Final accelerator voltage | $V_{gg}(\ell)$ | = | max. min. | 16000 9000 | V V |
| Geometry control electrode voltage | v _{g8} | = | max. | 2500 | v |
| Deflection plate shield voltage | Vg7 | = | max. | 2500 | v |
| Beam centring electrode voltage | V _{g6} | = | max. | 2500 | v |
| Astigmatism control electrode voltage | Vg5 | = | max. | 2500 | v |
| Focusing electrode voltage | Vg4 | = | max. | 2500 | v |
| Deflection blanking electrode voltage | V _{g3} | = | max. | 2500 | v |
| First accelerator voltage | vg2 | = | max. min. | 2500 1250 | v v |
| Control grid voltage | | | | | |
| negative | -v _{g1} | = | max. | 200 | v |
| positive | v _{g1} | = | max. | 0 | v |
| positive peak | v _{g1} p | = | max. | 2 | v |
| Voltage between cathode and heater | | | | | |
| cathode positive | $V_{+k/f}$ - | = | max. | 200 | v |
| cathode negative | V-k/f+ | = | max. | 125 | v |
| Ratio $V_{g_9}(\ell)/V_{g_5}$ | $v_{g_9(l)}/v_{g_5}$ | = | max. | 10 | |
| Ratio V_{g_2}/V_{g_5} | v_{g_2}/v_{g_5} . | = | max. | 1 | |
| Screen dissipation | W _ℓ | = | max. | 3 | mW/cm^2 |
| Average cathode current | ľ _k | Ŧ | max. | 300 | μA |
| CIRCUIT DESIGN VALUES | | | | | |
| Focusing electrode voltage | $V_{g_4} = 138 \text{ to}$ | 30 | 00 V | per kV | of Vg ₂ |
| Control grid voltage for visual extinction of focused spot | $-V_{g_1} = 24 \text{ to}$ | 7 | 2 V | per kV | of V _{g2} |
| Deflection factor at $V_{g_9(\ell)}/V_{g_5} = 6$ | a asin ana bulat | | | | Lon Tot 19 |
| horizontal | $M_X = max$. | 10. | 8 V/ | 'cm per | kV of Vg5 |
| vertical | $M_y = 3.4 \text{ to}$ | 4. | 0 V/ | 'cm per | kV of Vg5 |
| Focusing electrode current | $I_{g_4} = -10 \text{ to}$ | +1 | 5 μΑ | An the | |
| Control grid circuit resistance | $R_{g_1} = max.$ | 1. | 5 M | ດ | |
| Deflection plate circuit resistance | = max. | | kΩ | 2.00000 | 7Z2 6102 |

¹) This tube is designed for optimum performance when operating at the ratio $V_{g_0}(\ell)/V_{g_5} = 6$.

Opération at other ratio may result in changes in deflection uniformity and geometry distortion.

The geometry control electrode voltage should be adjusted for optimum performance. For any necessary adjustment its potential will be within the stated range.

- ²) This voltage should be equal to the mean x and y plates potential.
- ³) The beam centring electrode voltage should be adjusted for equal brightness in the x direction with respect to the electrical centre of the tube.
- ⁴) When putting the tube into the mu-metal shield care should be taken not to damage the side contacts.
- 5) The astigmatism control electrode voltage should be adjusted for optimum spot shape. For any necessary adjustment its potential will be within the stated range.
- 6) For beam blanking of a beam current $I_{g_Q}(\ell)$ of 10 μA .
- 7) The sensitivity at a deflection of less than 75% of the useful scan will not differ from the sensitivity at a deflection of 25% of the useful scan by more than the indicated value.

⁸) A graticule, consisting of concentric rectangles of 100 mm x 60 mm and 98 mm x 58.2 mm is aligned with the electrical x axis of the tube. The edges of a raster will fall between these rectangles with optimum correction potentials applied. 7Z2 7863

D13-16.

CORRECTION COILS

The D13-16.. is provided with a coil unit consisting of a pair of coils for:

- a. Correction of the orthogonality of the x and y traces (which means that at the centre of the screen the angle between the x and y traces can be made exactly 90°).
- b. Vertical shift of the scanned area.

DETAIL DRAWING OF COIL UNIT

Dimensions in mm



The currents required under typical operating conditions, the tube being screened by a mu-metal shield closely surrounding the coils (e.g. 55554), are max. 2.5 mA per degree of angle correction and max. 2 mA per mm of shift. If not such shield is used these values have to be multiplied by a factor k (1 < k < 2), the value of which depends on the diameter of the shield and approaches 2 for the case no shield is present.

The D.C. resistance is approx. 180 Ω per coil.

When designing the supply circuit for these coils it should be considered that the maximum current required in either coil can be 15 mA.

Circuit diagrams

A suitable circuit permitting independent controls of orthogonality correction and vertical shift is given in fig.1.



P1, P4: Potentiometers 220 Ω , 1 Watt, gangedP2, P3: Potentiometers 100 Ω , 0,5 Watt, gangedR1, R2, R3, R4: Resistors56 Ω , 0,5 Watt

Fig.1

The dissipation in the potentiometers can be reduced considerably if the requirement of independent controls is dropped (see fig. 2).



 P_1 , P_2 : Potentiometers, 220 Ω , 0,5 Watt, ganged P_3 , P_4 : Potentiometers, 220 Ω , 0,5 Watt, ganged

Fig.2

A further reduction of the dissipation can be obtained by inserting a commutator for each coil (see fig. 3).

The procedure of adjustment will then become more complicated, but it should be kept in mind that a readjustment is necessary only when the tube has to be replaced.



P₁, P₂ : Potentiometers, 500 Ω , 0,5 Watt. S₁, S₂ : Commutators



For the adjustment of the currents the following procedure is recommended:

- a. With the tube fully scanned in the vertical direction the scanned area must be shifted so that the useful vertical scan on either side of the geometric centre of the screen meets the published value of 30 mm min. With the circuit according to fig.1 this is done by means of the ganged potentiometers P_1 and P_4 .
- b. Adjustment of orthogonality by means of the ganged potentiometers P_2 and P_3 in fig.1. A slight readjustment of P_1 and P_4 may be necessary afterwards.

With a circuit according to fig. 2 or 3 these corrections have to be performed by means of successive adjustments of the currents in the coils.

The most convenient deflection signal is a square waveform permitting an easy and fairly accurate check of orthogonality.

7Z2 7866

9



INSTRUMENT CATHODE-RAY TUBE

The D13-16../01 is equivalent to the D13-16.. but features an internal graticule. This graticule can be illuminated.

MECHANICAL DATA

Dimensions in mm





Maximum angle between x-trace and x-axis of the graticule

 $+5^{0}$

ALIGNMENT

In order to align the x-trace and the x-axis of the graticule an image rotating coil may be used. This coil should be positioned at one third of the cone length, seen from the face end, and can be attached to the inner surface of the mumetal shield.

Under typical operating conditions maximum 50 ampere-turns are required for alignment.

ILLUMINATION

To illuminate the internal graticule the use of a light conductor (e.g. of Perspex) is obligatory. The following design considerations should be observed:

In order to achieve the most efficient light conductance the holes for the light bulb as well as the contact area with the front plate should be polished. The contact with the edges of the front plate should be as close as possible and the edges of the front plate and the corresponding hole in the light conductor should be parallel to achieve light beams perpendicular to the edges. It is advised to apply reflective material to the outer circumference of the conductor and if possible also to both planes (see drawing).



1) Reflective material.

2) Polished.

- ³) Close and constant distance to front plate of tube. It is essential that the light conductor and the front plate of the tube are in plane.
- ⁴) If possible reflective material.

D13-17..

INSTRUMENT CATHODE-RAY TUBE

SCREEN

| $(h_{1}, m_{1}) \in [1, 1, m]$ | colour | persistence |
|--------------------------------|--------------|--------------|
| D13-17BE | blue | medium short |
| D13-17GH | green | medium short |
| D13-17GP | bluish green | medium short |

HEATING: Indirect by A.C. or D.C.; parallel supply

Heater voltage

Heater current

MECHANICAL DATA

Dimensions in mm

6.3 V

300

mA

Vf

If



Socket (supplied with tube)



⁷Z2 7556

9.9.1966

OBSOLESCENT TYPE

1

D13-17..

| FOCUSING | electrostatic |
|------------|----------------------|
| DEFLECTION | double electrostatic |
| x plates | symmetrical |
| y plates | symmetrical |

If use is made of the full deflection capabilities of the tube the deflection plates will intercept part of the electron beam near the edge of the scan, hence a low impedance deflection plate drive is desirable.

Angle between x and y traces $90^{\circ} \pm 1^{\circ}$

TYPICAL OPERATING CONDITIONS

| Final accelerator voltage | $V_{gg(l)}$ | 10 000 | V |
|--|------------------|-------------------------|--------|
| Geometry control electrode voltage | Vg8 | 1670 <u>+</u> 100 | V |
| Deflection plate shield voltage | Vg7 | 1670 | V |
| Beam centring electrode voltage | Vg ₆ | 1670 <u>+</u> 20 | V |
| Astigmatism electrode voltage | Vg5 | 1670 ± 100 | V |
| Focusing electrode voltage | Vg4 | 230 to 500 | V |
| Deflection blanking electrode voltage | Vg3 | 1670 | V |
| Deflection blanking control voltage | ΔV_{g_3} | max. 60 | v |
| First accelerator voltage | v_{g_2} | 1670 | v |
| Control grid voltage for visual extinction of focused spot | -V _{g1} | 50 to 120 | v |
| Deflection factor, horizontal | M _X | max. 18 | V/cm |
| vertical | My | 4.5 to 5.5 | V/cm |
| Deviation of linearity of deflection | | max. 2 | % |
| LIMITING VALUES (Absolute max. rating | g system) | | |
| Final accelerator voltage | $v_{g9}(l)$ | max. 16000 min. 9000 | v v |
| First accelerator voltage | v _{g2} | max. 2500 min. 1250 | V V |

INSTRUMENT CATHODE-RAY TUBE

Oscilloscope tube with flat face post deflection acceleration by means of a helical electrode, side contacts, metal backed screen, 6 cm scan for high frequency and high writing speed applications.

| QUICK REFE | RENCE DATA | S | district. | n traisa |
|-------------------------------|---------------------|---|-----------|----------|
| Final accelerator voltage | Vg ₇ (1) | = | 10 | kV |
| Display area | | = | 6 x 10 | cm |
| Deflection factor, horizontal | M _X | = | 30 | V/cm |
| vertical | My | = | 10.9 | V/cm |

SCREEN

| in the second | colour | persistence |
|----------------------|-----------------------|------------------------------|
| D13-19BE | blue | medium short |
| D13-19GH D13-19GP | green bluish green | medium short medium short |
| D13-19GM | yellowish green | long |

| Useful screen diameter | | min. | 114 | mm |
|---|---|------|-----|----|
| Useful scan at $V_{g_7(l)}/V_{g_4} = 6$ | | | | |
| horizontal | | min. | 100 | mm |
| vertical | * | min. | 60 | mm |

The useful scan may be shifted vertically to a max. of 3 mm with respect to the geometric centre of the faceplate.

HEATING

Indirect by A.C. or D.C.; parallel supply

| Heater | voltage |
|--------|---------|
| Heater | current |

| Vf | = | 6.3 | V |
|----------|-----------------|-----|------|
| If | () = (\$ | 300 | mA |
| Ser Bell | | 772 | 5510 |

MAINTENANCE TYPE

MECHANICAL DATA

Dimensions in mm



Mounting position: any

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

Base

Diheptal

Dimensions and connections

See also outline drawing

| Overall length | max. | 452 | mm |
|--|------------------------------|-----------------------------------|----|
| Face diameter | max. | 134.5 | mm |
| Net weight: | approx. | 910 | g |
| Accessories | | | |
| Socket Final accelerator contact connector Side contact connector Mu-metal shield | type type type type | 5914/3 55563 55561 55551 | 20 |
| | | | |

7Z2 7728

| CAPACITANCES | | | |
|--|--------------------------------|-------|------|
| x_1 to all other elements except x_2 | $C_{x_1}(x_2) =$ | = 3.0 | 0 pF |
| \mathbf{x}_2 to all other elements except \mathbf{x}_1 | $C_{x_2}(x_1) =$ | = 3.0 | 0 pF |
| y_1 to all other elements except y_2 | $C_{y_1}(y_2) =$ | = 3.0 | 0 pF |
| y_2 to all other elements except y_1 | $C_{y_2}(y_1) =$ | = 3. | 0 pF |
| \mathbf{x}_1 to \mathbf{x}_2 | $C_{x_1x_2} =$ | = 1. | 9 pF |
| y_1 to y_2 | Cy ₁ y ₂ | = 1. | 0 pF |
| Control grid to all other elements | Cg1 | = 6. | 0 pF |
| Cathode to all other elements | Ck | = 3. | 5 pF |
| | | | |

| DEFLECTION | double electrostatic | |
|------------|----------------------|--|
| x plates | symmetrical | |
| v plates | symmetrical | |

electrostatic

If use is made of the full deflection capabilities of the tube the deflection plates will intercept part of the electron beam; hence a low impedance deflection plate drive is desirable.

Angle between x and y traces.

90° <u>+</u> 1°

LINE WIDTH

FOCUSING

Measured with the shrinking raster method in the centre of the screen.

| Final accelerator voltage | $V_{g_{7}(0)}$ | = | 10 | kV |
|---------------------------------------|----------------|---|------|---------|
| Astigmatism control electrode voltage | Vg4 | = | 1670 | v^3) |
| First accelerator voltage | Vg2 | = | 1670 | V |
| Beam current | I (ℓ) | = | 10 | μA |
| Line width | 1.w. | = | 0.4 | mm |

HELIX

| Post deflection accelerator helix resistance | = | min. | 200 | MΩ |
|--|---|------|-----|----|
|--|---|------|-----|----|

³) See page 6

TYPICAL OPERATING CONDITIONS

| Final accelerator voltage | Vg7 (1) | = | 10 | kV |
|---------------------------------------|-----------------|---|-------------------------|------------------|
| Geometry control electrode voltage | Vg ₆ | = | 1670 <u>+</u> 170 | V ¹) |
| Deflection plate shield voltage | V _{g5} | = | 1670 <u>+</u> 85 | V ²) |
| Astigmatism control electrode voltage | Vg4 | = | 1670 ± 85 | v ³) |
| Focusing electrode voltage | v_{g_3} | = | 320 to 500 | V |
| First accelerator voltage | Vg2 | = | 1670 | V |
| Control grid voltage for visual | | | | |
| extinction of focused spot | -Vg1 | = | 53 to 82 | V |
| Deflection factor, horizontal | M _X | = | 27 to 33 | V/cm |
| vertical | My | = | 9.5 to 12.4 | V/cm |
| Deviation of linearity of deflection | | = | max. 2 | % ⁴) |
| Geometry distortion | e songelouge | | See note ⁵) | |
| Useful scan, horizontal | | = | min. 100 | mm |
| vertical | | = | min. 60 | mm |
| | | | | |

CIRCUIT DESIGN VALUES

| Focusing voltage | Vg3 | = | 190 to 300 | V per kV of V _{g4} |
|--|---------------------------------|---|------------|-----------------------------|
| Control grid voltage for visual extinction of focused spot | -V _{g1} | = | 32 to 49 | V per kV of V_{g_2} |
| Deflection factor at $V_{g7} (l)^{V_{g4}} = 6$ | | | | |
| horizontal | $M_{\rm X}$ | = | 16 to 20 | V/cm per kV of V_{g_4} |
| vertical | My | = | 5.7 to 7.4 | V/cm per kV of V_{g_4} |
| Control grid circuit resistance | R_{g_1} | = | max. 1.5 | МΩ |
| Deflection plate circuit resistance | R _x , R _y | = | max. 1 | MΩ |
| Focusing electrode current | Ig3 | = | -15 to +10 | μA 6) |

¹)²)³)⁴)⁵)⁶) See page 6

7Z2 5522

4

LIMITING VALUES (Absolute max. rating system)

1 -41 TC

| Einel accelerator veltage | V | = | max. | 12 | kV |
|--|----------------------|---|--------------|--------------|--------------------|
| Final accelerator voltage | vg7(l) | = | min. | 6 | kV |
| Geometry control electrode voltage | Vg6 | = | max. | 2200 | V |
| Deflection plate shield voltage | Vg5 | = | max. | 2100 | V |
| Astigmatism control electrode voltage | Vg4 | = | max. min. | 2100 1000 | V V |
| Focusing electrode voltage | Vg3 | = | max. | 1500 | v |
| First accelerator voltage | V _{g2} | | max. min. | 2100 1000 | V V |
| Control grid voltage | | | | | |
| negative | $-V_{g_1}$ | = | max. | 200 | V |
| positive | Vg1 | = | max. | 0 | V |
| positive peak | Vglp | = | max. | 2 | V |
| Cathode to heater voltage | | | | | |
| cathode positive | V+k/f- | = | max. | 200 | V |
| cathode negative | V-k/f+ | = | max. | 125 | v |
| Voltage between astigmatism control electrode and any deflection plate | Vg4/x | = | max. | 500 | v |
| | Vg4/y | = | max. | 500 | V |
| Screen dissipation | Wl | = | max. | 3 | mW/cm ² |
| Ratio $V_{g_7(\ell)}/V_{g_4}$ | $V_{g_7(a)}/V_{g_4}$ | = | max. | 6 | |

- ¹) This tube is designed for optimum performance when operating at the ratio $Vg_7(\ell)/Vg_4 = 6$. Operation at other ratio may result in changes in deflection uniformity and geometry distortion. The geometry control electrode voltage should be adjusted for optimum performance. For any necessary adjustment its potential will be within the stated range.
- 2) This voltage should be equal to the mean x- and y plates potential.
- 3) The astigmatism control electrode voltage should be adjusted for optimum spot shape. For any necessary adjustment its potential will be within the stated range.
- 4) The sensitivity at a deflection of less than 75 % of the useful scan will not differ from the sensitivity at a deflection of 25 % of the useful scan by more than the indicated value.
- ⁵) A graticule, consisting of concentric rectangles of 100 mm x 60 mm and 98 mm x 58.2 mm is aligned with the electrical x axis of the tube. The edges of a raster will fall between these ractangles with optimum correction potentials applied.
- 6) Values to be taken into account for the calculation of the focus potentiometer.

D13-20..

INSTRUMENT CATHODE-RAY TUBE

SCREEN

| | colour | persistence |
|----------|--------|--------------|
| D13-20BE | blue | medium short |

HEATING: Indirect by A.C. or D.C.; parallel supply

Heater voltage

Heater current

Dimensions in mm

Vf

If

6.3 V

300

mA

MECHANICAL DATA Base: Diheptal 12 pins

 Straight part of the bulb.
 Location of the recessed cavity button contact with respect to the X-trace.

> 2700 2700

x trace

95 012

x2 x1

i.c i.c

12

2

a3



Accessories

x1

VI

g2,g4

q5

Socket

FOCUSING electrostatic DEFLECTION double electrostatic x plates symmetrical y plates symmetrical If use is made of the full deflection comphilities of the tube the deflection plate

If use is made of the full deflection capabilities of the tube the deflection plates will intercept part of the electron beam; hence a low impedance deflection plate drive is desirable.

| Angle between x and y traces | $90^{\circ} \pm 1^{\circ}$ | |
|------------------------------|----------------------------|--|
| | | |

TYPICAL OPERATING CONDITIONS

D13-20..

| Final accelerator voltage | $V_{g_7(\ell)}$ | | 24 | kV |
|--|------------------|-----------------|--------------|--------|
| Geometry control electrode voltage | v _{g6} | 4000 | +400 -200 | V V |
| Deflection plate shield voltage | Vg5 | | 4000 | V |
| Astigmatism control electrode voltage | Vg4,g2 | 4000 | ±200 | V |
| Focusing electrode voltage | v _{g3} | 770 to | 1200 | V |
| Control grid voltage for visual extinction of focused spot | -v _{g1} | 1 2 0 to | 192 | V |
| Deflection factor, horizontal | M _x | 67 to | 80 | V/cm |
| vertical | My | 13.5 to | 18.5 | V/cm |
| Deviation of linearity of deflection | | max. | 2 | % |

LIMITING VALUES (Absolute max. rating system)

| Einel accolonaton voltage | V | max. | 24 | kV |
|---------------------------------------|---------------------------------|------|------|----|
| Final accelerator voltage | ^v g ₇ (l) | min. | 4 | kV |
| | 17 | max. | 4200 | V |
| Astigmatism control electrode voltage | vg4,g2 | min. | 1000 | V |

X-Ray warning

X-ray shielding is advisable to give protection against possible danger of personal injury arising from prolonged exposure at close range to this tube when operated above 16 kV.

INSTRUMENT CATHODE-RAY TUBE

Oscilloscope tube with flat face post deflection acceleration by means of a helical electrode, side contacts, metal backed screen, 4 cm scan for high frequency and high writing speed applications.

| QUICK REFERENC | E DATA | an an Airte anta | naise fr |
|-------------------------------|------------------|---------------------|----------|
| Final accelerator voltage | $V_g(l) =$ | 10 | kV |
| Display area | = | 4 x 10 | cm |
| Deflection factor, horizontal | M _X = | 30 | V/cm |
| vertical | M _y = | 6.4 | V/cm |

SCREEN

| | colour | persistence |
|----------|-----------------|--------------|
| D13-21BE | blue | medium short |
| D13-21GH | green | medium short |
| D13-21GP | bluish green | medium short |
| D13-21GM | yellowish green | long |

| Useful screen diameter | min. | 114 | mm |
|--|------|-----|----|
| Useful scan at $V_{g_7}(\ell)/V_{g_4} = 6$ | | | |
| horizontal | min. | 100 | mm |
| vertical | min. | 40 | mm |

The useful scan may be shifted vertically to a max. of 3 mm with respect to the geometric centre of the faceplate.

HEATING

Indirect by A.C. or D.C.; parallel supply

| Heater voltage | V _f = | 6.3 | V |
|----------------|--------------------|-----|----|
| Heater current | $\overline{I_f} =$ | 300 | mA |

MAINTENANCE TYPE

1



Mounting position: any

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

| Base | Diheptal | 12 | pins |
|------|----------|----|------|
|------|----------|----|------|

| Dimensions and connections | | | |
|-------------------------------------|---------|---------|----------|
| See also outline drawing | | | |
| Overall length | max. | 468 | mm |
| Face diameter | max. | 134.5 | mm |
| Net weight: | approx. | 910 | g |
| Accessories | | | |
| Socket | type | 5914/20 |) |
| Final accelerator contact connector | type | 55563 | |
| Side contact connector | type | 55561 | |
| Mu-metal shield | type | 55551 | |
| | | | 7Z2 7730 |

CAPACITANCES

| x_1 to all other elements except x_2 | $C_{x_{1}}(x_{2})$ | = | 2.8 | pF |
|--|---|---|-----|---------------|
| \mathbf{x}_2 to all other elements except \mathbf{x}_1 | $C_{x_2}(x_1)$ | = | 2.8 | pF |
| y_1 to all other elements except y_2 | ^C y ₁ (y ₂) | = | 2.8 | pF |
| y_2 to all other elements except y_1 | $C_{y_2}(y_1)$ | = | 2.8 | \mathbf{pF} |
| \mathbf{x}_1 to \mathbf{x}_2 | $C_{x_1x_2}$ | = | 1.9 | pF |
| y_1 to y_2 | C _{y1y2} | = | 1.5 | pF |
| Control grid to all other elements | Cg1 | = | 6.0 | pF |
| Cathode to all other elements | C _k | = | 3.5 | pF |

FOCUSING

electrostatic

DEFLECTION

x plates

y plates

double electrostatic symmetrical symmetrical

If use is made of the full deflection capabilities of the tube the deflection plates will intercept part of the electron beam; hence a low impedance deflection plate drive is desirable.

Angle between x and y traces

 $90^{\circ} \pm 1^{\circ}$

LINE WIDTH

Measured with the shrinking raster method in the centre of the screen.

| Final accelerator voltage | Vg7 (1) | = | 10 | kV |
|---------------------------------------|---------|-----|------|---------|
| Astigmatism control electrode voltage | Vg4 | = | 1670 | v^3) |
| First accelerator voltage | Vg2 | = | 1670 | v |
| Beam current | I(l) | = | 10 | μA |
| Line width | l.w. | 5.5 | 0.4 | mm |

HELIX

Post deflection accelerator helix resistance = min. $200 \text{ M}\Omega$

³) See page 6

| TYPICAL OPERATING CONDITIONS | | | | |
|--|-----------------|----|-------------------|------------------|
| Final accelerator voltage | Vg7() | = | 10 | kV |
| Geometry control electrode voltage | Vg ₆ | = | 1670 <u>+</u> 170 | V ¹) |
| Deflection plate shield voltage | Vg5 | = | 1670 ± 85 | V ²) |
| Astigmatism control electrode voltage | V _{g4} | = | 1670 ± 85 | V 3) |
| Focusing electrode voltage | Vg3 | = | 320 to 500 | V |
| First accelerator voltage | Vg2 | = | 1670 | V |
| Control grid voltage for visual extinction of focused spot | vg1 | 10 | -50 to -80 | V |
| Deflection factor, horizontal | M_{X} | = | 27 to 33 | V/cm |
| vertical | My | = | 5.7 to 7.1 | V/cm |
| Deviation of linearity deflection | | | | |
| horizontal | | = | max. 1.5 | % ⁴) |
| vertical | | = | max. 1.0 | % ⁴) |
| Geometry distortion | | | See note 5 | |
| Useful scan, horizontal | | = | min. 100 | mm |
| vertical | | = | min. 40 | mm |

CIRCUIT DESIGN VALUES

| Focusing electrode | Vg | = 190 to | 300 | V per kV of V_{g_4} |
|--|---------------------------------|-----------|------|--------------------------|
| Control grid voltage for visual extinction of focused spot | -Vg1 | = 30 to | 48 | V per kV of Vg2 |
| Deflection factor at $V_{g7} (l) / V_{g4} = 6$ | | | | na nation without an |
| horizontal | M_X | = 16.2 to | 19.8 | V/cm per kV of V_{g_4} |
| vertical | My | = 3.4 to | 4.25 | V/cm per kV of V_{g_4} |
| Control grid circuit resistance | Rg1 | = max. | 1.5 | MΩ |
| Deflection plate circuit | | | | |
| resistance | R _x , R _y | = max. | 1.0 | MΩ |
| Focusing electrode current | Ig | = -15 to | +10 | μA ⁶) |

¹)²)³)⁴)⁵)⁶) See page 6

LIMITING VALUES (Absolute max. rating system)

| T: 1 1 | V | = | max. | 12 | kV |
|---------------------------------------|--------------------------|---|--------------|--------------|--------------------|
| Final accelerator voltage | ^v g7(l) | = | min. | 6 | kV |
| Geometry control electrode voltage | Vg6 | = | max. | 2200 | v |
| Deflection plate shield voltage | v _{g5} | = | max. | 2100 | v |
| Astigmatism control electrode voltage | Vg4 | | max. | 2100 1000 | V V |
| Focusing electrode voltage | Vgg | = | max. | 1500 | v |
| First accelerator voltage | v _{g2} | = | max. min. | 2100 1000 | V V |
| Control grid voltage | | | | | |
| negative | -V _{g1} | = | max. | 200 | V |
| positive | V _{g1} | = | max. | 0 | v |
| positive peak | V _{g1p} | = | max. | 2 | v |
| Cathode to heater voltage | | | | | |
| cathode positive | V+k/f- | = | max. | 200 | v |
| cathode negative | V-k/f+ | = | max. | 125 | v |
| Voltage between astigmatism control | | | | | |
| electrode and any deflection plate | Vg4/x | = | max. | 500 | V |
| | $V_{g_4/y}$ | = | max. | 500 | v · |
| Screen dissipation | Wg | = | max. | 3 | mW/cm ² |
| Ratio $V_{g_7(\ell)}/V_{g_4}$ | $v_{g_{7}(l)}/v_{g_{4}}$ | = | max. | 6 | |

7Z2 5535

Б

- ¹) This tube is designed for optimum performance when operating at the ratio $V_{g_7(\ell)}/V_{g_4} = 6$. Operation at other ratio may result in changes in deflection uniformity and geometry distortion. The geometry control electrode voltage should be adjusted for optimum performance. For any necessary adjustment its potential will be within the stated range.
- ²) This voltage should be equal to the mean x and y plates potential.
- 3) The astigmatism control electrode voltage should be adjusted for optimum spot shape. For any necessary adjustment its potential will be within the stated range.
- ⁴) The sensitivity at a deflection of less than 75 % of the useful scan will not differ from the sensitivity at a deflection of 25 % of the useful scan by more than the indicated value.
- ⁵) A graticule, consisting of concentric rectangles of 100 mm x 40 mm and 98.8 mm x 39 mm is aligned with the electrical x axis of the tube. The edges of a raster will fall between these rectangles with optimum correction potentials applied.

 $^{6}\)$ Values to be taken into account for the calculation of the $\mathrm{V}_{\mathrm{g}_{3}}\-$ potentiometer. 722 7732
INSTRUMENT CATHODE-RAY TUBE

13 cm diameter flat faced oscilloscope tube, with metal-backed screen, helical PDA and side connections to the x and y plates. The y plates are intended to be included in a resonant circuit tunable to frequencies from 300 MHz to 900 MHz by means of adapter units outside the tube. This tube incorporates deflection blanking and is intended for high frequency, narrow bandwidth displays.

| QUICK REFER | ENCE DATA | | | | |
|-------------------------------|----------------|---|-------------|---|------|
| Final accelerator voltage | Vg9(1) | = | and the set | 6 | kV |
| Display area | | = | 5x1 | 0 | cm |
| Deflection factor, horizontal | M _x | = | max. 1 | 4 | V/cm |
| vertical | My | | See note | 1 | |

SCREEN

| | a rebuir bae an | colour | persistence |
|----------------|--------------------------|--------|--------------|
| | D13-23GH | green | medium short |
| Useful screen | diameter | | min. 114 mm |
| Useful scan at | $V_{g_9(l)}/V_{g_5} = 5$ | | |
| | horizontal | | min. 100 mm |
| | vertical | | min. 50 mm |

The useful scan may be shifted vertically to a max. of 5 mm with respect to the geometric centre of the faceplate.

HEATING

Indirect by A C. or D.C.; parallel supply

Heater voltage Heater current $\frac{V_{f}}{I_{f}} = 6.3 V}{I_{f}} = 300 mA$

7Z2 7794



Mounting position: any

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

| 14 pins all glas | S |
|--------------------------------------|--|
| | |
| max. 596 max. 134.5 | mm mm |
| approx. 1300 | g |
| | |
| type55566type55563type55561type55554 | |
| | 14 pins all glas max. 596 max. 134.5 approx. 1300 type 55566 type 55563 type 55561 type 55554 |

1) Straight part

- ²) The tolerance of the position of the neck pins with respect to the x-trace is $\pm 2^{\circ}$.
- ³) The tolerance of the position of the base pins with respect to the x-trace is $\pm 10^{\circ}$.
- 4) When putting the tube into the mu-metal shield care should be taken not to damage the side contacts. 7Z2 7947

CAPACITANCES

| x ₁ to all other elements except x ₂ | $C_{x_1(x_2)}$ | ÷ | 2.8 | pF |
|--|-----------------|---|-----|----|
| \mathbf{x}_2 to all other elements except \mathbf{x}_1 | $C_{x_2(x_1)}$ | = | 2.8 | pF |
| x1 to x2 | $C_{x_1x_2}$ | = | 2.3 | pF |
| Control grid to all other elements | Cg ₁ | = | 5.0 | pF |
| Cathode to all other elements | Ck | = | 3.5 | pF |
| Deflection blanking electrode to all other elements | Cg3 | - | 9 | pF |

| FOCUSING | electrostatic |
|----------|---------------|
| | |

| DEFLECTION | double electrostatic |
|------------|----------------------|
| x plates | symmetrical |
| y plates | symmetrical |

If use is made of the full deflection capabilities of the tube the deflection plates will intercept part of the electron beam; hence a low impedance deflection plate drive is desirable.

Angle between x and y plates $90^{\circ} + 1^{\circ}$

HELIX

Post deflection accelerator helix resistance min. 300 MΩ

CIRCUIT DESIGN VALUES

| Focusing voltage | Vg4 | = | 138 to 300 | V per kV of Vg2 |
|--|----------------|---|------------|-----------------------------|
| Control grid voltage for visual extinction of focused spot | -Vg1 | = | 24 to 72 | V per kV of V _{g2} |
| Deflection factor at $V_{gg(l)}/V_{g_5} = 3$ | 5 | | | |
| horizontal | M _x | = | max. 10.8 | V/cm per kV of Vg5 |
| vertical | My | | See note 1 | |
| Control grid circuit resistance | Rg1 | = | max. 1.5 | MΩ |
| Deflection plate circuit resistance | R_{x}, R_{y} | = | max. 50 | kΩ |
| Focusing electrode current | Iga | = | +15 to -10 | μA ²) |

¹) Depends on the frequency and the adaptors being used.

²⁾ Values to be taken into account for the calculation of the focus potentiometer. 7Z2 5539

TYPICAL OPERATING CONDITIONS

| Final accelerator voltage | $V_{g_9(l)}$ | = | | 6000 | V | |
|--|------------------|----|---------------|------|----|-----|
| Geometry control electrode voltage | Vg8 | = | 1300 <u>+</u> | 100 | V | 1) |
| Deflection plate shield voltage | Vg7 | = | | 1300 | V | 2) |
| Beam centring electrode voltage | V _{g6} | = | 1300 ± | 20 | V | 3) |
| Astigmatism control electrode voltage | Vg5 | = | 1300 ± | 100 | V | 4) |
| Focusing electrode voltage | Vg4 | = | 180 to | 390 | V | |
| Deflection blanking electrode voltage | V _{g3} | = | | 1300 | V | |
| Deflection blanking control voltage | ΔV_{g_3} | = | max. | 60 | V | 5) |
| First accelerator voltage | v _{g2} | = | | 1300 | V | |
| Control grid voltage for visual extinction of focused spot | -v _{g1} | = | 31 to | 93 | v | |
| Deflection factor | teresta all'inte | | | | | |
| horizontal | M _x | - | max. | 14 | V/ | 'cm |
| vertical | | Se | e note 7 | | | |
| Geometry distortion | | Se | e note 6 | | | |
| Useful scan | | | | | | |
| horizontal | | = | min. | 100 | m | m |
| vertical | | = | min. | 50 | m | m |

- ¹) This tube is designed for optimum performance when operating at the ratio $V_{gg(\ell|)}/V_{g5} = 5$. Operation at other ratio may result in changes in deflection uniformity and geometry distortion. The geometry control electrode voltage should be adjusted for optimum performance. For any necessary adjustment its potential will be within the stated range.
- 2) This voltage should be equal to the mean x- and y plates potential.
- 3) The beam centring electrode voltage should be adjusted for equal brightness in the x direction with respect to the electrical centre of the tube.
- 4) The astigmatism control electrode voltage should be adjusted for optimum spot shape. For any necessary adjustment its potential will be within the stated range.
- 5) For beam blanking of a beam current of 10 μ A.
- 6) A graticule, consisting of concentric rectangles of 100 mm x 50 mm and 98 mm x 48.2 mm is aligned with the electrical x aixs of the tube. The edges of a raster will fall between these rectangles with optimum correction potentials applied.
- 7) Depends on the frequency and the adaptors being used.

LIMITING VALUES (Absolute max. rating system)

| | | = | max. | 10000 | V |
|---------------------------------------|--------------------------|---|------|-------|--------------------|
| Final accelerator voltage | $V_{g_9}(l)$ | = | min. | 5000 | V |
| Geometry control electrode voltage | Vg8 | = | max. | 2000 | V |
| Deflection plate shield voltage | Vg7 | = | max. | 2000 | V |
| Beam centring electrode voltage | Vg6 | = | max. | 2000 | V |
| Astigmatism control electrode voltage | Vg5 | = | max. | 2000 | V |
| Focusing electrode voltage | Vg4 | = | max. | 2000 | V |
| Deflection blanking electrode voltage | Vg3 | = | max. | 2000 | V |
| Einst an algoriton voltage | 37 | = | max. | 2000 | V |
| First accelerator voltage | vg ₂ | = | min. | 1200 | V |
| Control grid voltage | | | | | |
| negative | -Vg1 | = | max. | 200 | V |
| positive | v _{g1} | = | max. | 0 | V |
| positive peak | Vg _{1p} | = | max. | 2 | V |
| Cathode to heater voltage | 10.00 | | | | |
| cathode positive | V+k/f- | = | max. | 200 | V |
| cathode negative | $V_{-k/f+}$ | = | max. | 125 | V |
| Voltage between astigmatism electrode | Vor /x | = | max. | 500 | V |
| and any deflection plate | $v_{g_5/y}^{g_5/y}$ | = | max. | 500 | V |
| Cathode current (average) | Ik | = | max. | 300 | mA |
| Screen dissipation | We | = | max. | 3 | mW/cm ² |
| Ratio $V_{g_9(l)}/V_{g_5}$ | $V_{g_{9}(l)}/V_{g_{5}}$ | = | max. | 10 | |
| Ratio Vg9/Vg5 | v_{g_2}/v_{g_5} | = | max. | 1 | |

APPLICATION DATA

The D13-23GH is intended for use at ultra high frequencies as a monitor of transmitter output.

To achieve the necessary sensitivity the y-deflection plates are designed to form part of a tuned circuit, resonant at the carrier frequency of the transmitter. Details of the coupling units and tuning arrangements are given below.

Mechanical construction of the coupling units

| | | Unit 1 | Unit 2 | Unit | t 3 |
|-------------------|------|----------------|---------------|----------------|--------|
| | (47 | 75 to 575 MHz) | (500 to 775 M | Hz) (675 to 90 | 0 MHz) |
| Coil former | | | | | |
| Length | | 20 | 20 | | 18 mm |
| Diameter | | 9 | 9 | | 3 mm |
| Primary | | | | | |
| No. of turns | | 4 | 1.5 | 1 | .5 |
| Wire diameter | | 0.9 | 0.9 | 0 | .9 mm |
| Approx. coil leng | th | 14 | 10 | | 7 mm |
| Secondary | | | | | |
| No. of turns | | 4 | 2 | | 2 |
| Wire diameter | | 0.5 | 1.5 | 0 | .9 mm |
| Approx. coil leng | th | 14 | 10 | | 7 mm |
| Trimming capacita | ince | 0.6 to 12 | 0.5 to 6 | 0.5 to | 6 pF |

Copper wire is used for all primary windings and enamelled copper wire is used for the secondaries.

The secondary turns are wound between the primary turns.

The trimmer capacitors of units 1 and 2 are connected between the secondary transformer windings in order to obtain good symmetry.

For unit 3 the trimmer is connected between secondary transformer windings and one connecting pin of the deflection system in order not to reduce the coupling factor.

APPLICATION DATA (continued)



- Ct = trimmer capacitance
- Cp = plate capacitance
- L = inductivity of the strips between deflection system and pins in the neck of the tube

Measurement of vertical sensitivity as a function of frequency

- 1. Adjust the trimmer so that the trimming capacitance is a minimum, to enaable resonance at the highest frequency to be obtained.
- Change the frequency of the signal generator and adjust the trimming capacitance successively until a maximum deflection is obtained on the tube face. Some care must be taken with these adjustments because several spurious resonances will be observed.
- 3. When the resonance frequency has been found, the input impedance of the tube must be transformed to exactly 50Ω to obtain a well defined signal voltage. For this purpose a transforming circuit is needed as shown in fig.3, and any reflectometer would be suitable. The impedance is matched when no reflection is measured and zero reflection can be obtained by the successive adjustment of the stubs, 1 and 2 shown in fig.3.
- 4. The tube should now be connected to the generator and the output power regulated for a scan of 5 cm.
- 5. Replace the tube by a Watt-meter to measure the output power, see fig.4.

The signal voltage can be calculated from:

 $V_{RMS} = W_{xR} = 7.07 W$

The above procedure must be repeated for matching, each time the operating frequency of the tube is altered.

APPLICATION DATA (continued)

| | Typical po | wer and sensitivity | y values |
|------|-----------------|---------------------|--------------------------------------|
| Unit | Frequency (MHz) | Power (mW) | Sensitivity (V _{RMS} /5 cm) |
| 1 | 445 | 37 | 1.36 |
| 1 | 480 | 39 | 1.40 |
| 1 | 540 | 55 | 1.66 |
| 2 | 565 | 46 | 1.52 |
| 2 | 680 | 69 | 1.86 |
| 3 | 680 | 91 | 2.14 |
| 3 | 750 | 110 | 2.35 |
| 3 | 800 | 195 | 3.12 |
| 3 | 850 | 240 | 3.47 |
| 3 | 900 | 390 | 4.43 |
| | | | |

All measurements:

 $V_{g_{2+5}} = 1300$ V) $V_{g_{0}} = 6000$ V) with respect to cathode

It should be noted that an increase in acceleration voltage will cause a loss of sensitivity at the lowest frequencies. At the higher frequencies this loss will partly be compensated by the decrease of the transit-time so that at 900 MHz the acceleration voltage can be increased to 2000 V, without changing the sensitivity.





7Z2 6129



INSTRUMENT CATHODE-RAY TUBE

The D13-24BE is a wide-band oscilloscope tube especially designed for observation and measurement of high frequency (1000 MHz) phenomena.

| QUICK REFERENCE | CE DAT. | A | | 14-14-184 5-11-14-145 |
|-------------------------------|-------------|------|-------|--------------------------|
| Final accelerator voltage | Vg9 | (1) | 24 | kV |
| Display area | | | 2 x 6 | cm |
| Deflection factor, horizontal | $M_{\rm X}$ | max. | 32 | V/cm |
| vertical | My | max. | 8 | V/cm |

SCREEN

| | | colour | persi | stenc | e | |
|--------------|--------------------------------|---------|----------|-------|------|--|
| 1. 1. | D13-24BE | blue | medium s | | hort | |
| Useful scree | n diameter | a de la | min. | 114 | mm | |
| Useful scan | at $V_{g_9}(\ell)/V_{g_5} = 8$ | | | | | |
| | horizontal | | min. | 60 | mm | |

vertical

The useful scan may be shifted vertically to a max. of 10 mm with respect to the geometric centre of the faceplate. The vertical useful scan will be at least 8 mm in either direction from the position of the undeflected spot, with a total of at least 20 mm. A positive voltage on the vertical deflection system will deflect the beam towards pin no.7.

min.

20

mm

DESCRIPTION

The D13-24BE is a wide-band oscilloscope tube especially designed for observation and measurement of high frequency (1000 MHz) phenomena.

The high-frequency performance of conventional oscilloscope tubes is limited by transit-time effects and by resonance phenomena occurring in the circuit consisting of the deflection plates and their connection leads.

7Z2 7797

TENTATIVE DATA

In order to overcome these limitations a travelling-wave deflection system is used in the D13-24BE. This deflection system consists of a metal tape wound in the shape of a flattened helix and the electron beam is deflected in the region between the flat part of the helix and a metal plate inserted into the helix. This metal plate is interconnected to the shield surrounding the system.

The mechanical dimensions of the helix have so been chosen that the signal delay per turn is equal to the electron transit-time per turn. This means that the transit-time effects are determined by the width of one turn only, whereas the defelction sensitivity is determined by the sum of the deviations of the beam due to the field of all the turns.

As for the transmissions of wide band signals containing ultra-high frequencies coaxial lines are most suitable. The deflection system has been designed for asymmetrical deflection (helix and plate are connected to inner and outer conductor respectively).

For the connection between the deflection system and coaxial plugs a three strip transmission-line is used which is brought out through the tube neck by means of pins sealed into the glass. The transition to coaxial plugs is made outside the tube. The characteristic impedance of the tube is 100 Ohms, and a modified version of the well-known General Radio type 874 coaxial connector is used (The diameter of the inner conductor has been reduced so as to obtain 100 Ohm impedance). Both input and output of the deflection system have been brought out through the tube neck so that it is possible to pick up the signal which is being observed at the output and to use it for other purposes, if desired. The performance of the deflection system may be expressed in terms of bandwidth (min. 1000 MHz for 3 dB down with respect to D.C.) or in terms of rise time of the display of a step-function signal (max. 0.35 nanoseconds for 10% to 90% of the final value).

Great care has been taken in the design to avoid phase distortion which would introduce overshoot in the display of such a signal. The extent to which a constant input impedance has been realized is indicated by the voltage standing-wave ratio (maximum 1.25 up to 1000 MHz). In order to be able to shift the display in vertical direction the deflection system shield is not directly connected but capacitively coupled to the outer connector of the coaxial plugs.

A D.C. shift voltage can be applied to the shield.

The useful vertical scan has been limited to 2 cm in order to obtain the highest possible sensitivity. This is important as in most cases the signal to be observed will be applied directly to the deflection system without any amplification.

The horizontal deflection plates giving 6 cm useful scan, are of conventional design and, of course, also brought out through the neck.

The typical acceleration voltage is 3 kV. Deviations from this value will cause deterioration of band-width and rise time, since the electron velocity will then not be equal to the velocity of signal propagation of the vertical deflection system. However this adjustment is not very critical. The electron gun features apart from astigmatism and geometry control electrodes auxiliary electrodes such as deflection blanking electrodes and a beam centring electrode. The latter can be used to center the beam with respect to the x plates.

Post deflection acceleration is achieved by a helical resistive coating in the innerside of the envelope which allows a P.D.A. to acceleration electrode voltage ratio of 10. The maximum P.D.A. voltage is 24 kV. This high voltage, the metal-backed screen and the small linewidth (0.12 mm) assure a high writingspeed.

In order to make use of the full capabilities of this tube some precautions have to be taken in the way the signal is applied to the tube. First, a good termination at the output of the deflection system is essential when pulse signals are to be observed, otherwise reflections from a mismatch at the output may distort the displayed wave-form.

A coaxial resistor is the most suitable termination.

For signal delays in oscilloscopes a high-quality delay-line should be used in order to avoid deterioration of performance due to band-width limitations of the delay-line.

HEATING

Indirect by A.C. or D.C.; parallel supply

| Heater voltage | V_{f} | 6.3 | V |
|----------------|---------|-----|----|
| Heater current | If | 300 | mA |

CAPACITANCES

| x_1 to all other elements except x_2 | $C_{x_1(x_2)}$ | 3.0 | pF |
|--|----------------|-----|----|
| \mathbf{x}_2 to all other elements except \mathbf{x}_1 | $C_{x_2(x_1)}$ | 3.0 | pF |
| x_1 to x_2 | $C_{x_1x_2}$ | 2.7 | pF |
| Control grid to all other elements | C_{g_1} | 5.0 | pF |
| Cathode to all other elements | Ck | 3.5 | pF |
| Deflection blanking electrode to all other elements | Cg3 | 9.0 | pF |



MECHANICAL DATA

Mounting position: any

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

| 14 pin all glass |
|------------------|
| |

Dimensions and connections

| Overall length | (mu-metal shield included) |) | 642 | mm |
|----------------|----------------------------|--------|-------|----|
| Face diameter | | max. | 134.5 | mm |
| Net weight | | approx | i nad | g |

Accessories

Base

| Socket | supplied with tube | | |
|-------------------------------------|--------------------|--|--|
| Final accelerator contact connector | type 55563 | | |
| Side contact connector | supplied with tube | | |
| Mu-metal shield | supplied with tube | | |

FOCUSING

electrostatic

DEFLECTION

| Horizontal | electrostatic symmetrical | | | | |
|----------------------|----------------------------|--------------|------|------|----|
| Vertical | delay-line system, asymmet | etrical | | | |
| Characteristic imped | ance of delay-line system | | 100 | Ω | |
| VSWR | max. | 1.25 up to 1 | 1000 | MHz | 1) |
| Bandwidth | | STOL | 1000 | MHz | 2) |
| Rise time | | (| 0.35 | nsec | 3) |
| Angle between x and | y traces | 90 | ± 20 | | |

LINE WIDTH

Measured with the shrinking raster method in the centre of the screen. 24000 V Final accelerator voltage Vgg(l) 3000 V 6) Astigmatism control electrode voltage Vg5 First accelerator voltage 3000 V Vg2 I (l) Beam current 0.5 μA Line width 1.w. 0.12 mm

HELIX

| Post deflection accelerator helix resistance mi | n. 300 MΩ |
|---|-----------|
|---|-----------|

TYPICAL OPERATING CONDITIONS

| Final accelerator voltage | $V_{g_9}(l)$ | 2400 | 00 V |
|--|------------------|---------------|---------------------|
| Geometry control electrode voltage | Vg8 | 3000 ± 20 | 00 V |
| Vertical deflection system shield voltage | Vg7 | 300 | 00 V ⁴) |
| Beam centring electrode voltage | Vg6 | 3000 ± 4 | 10 V 5) |
| Astigmatism control electrode voltage | Vg5 | 3000 ± 20 | 00 V 6) |
| Focusing electrode voltage | Vg4 | 400 to 90 | 00 V |
| Deflection blanking electrode voltage | Vg3 | 300 | 00 V |
| Deflection blanking control voltage | ΔV_{g_3} | 1 | 10 V ⁷) |
| First accelerator voltage | Vg ₂ | 300 | 00 V ⁸) |
| Control grid voltage for visual extinction of focused spot | -v _{g1} | 60 to 25 | 50 V |
| Deflection factor, horizontal | M _x | max. 3 | 32 V/cn |
| vertical | My | max. | 8 V/cn |
| Useful scan, horizontal | | min. 6 | 60 mm |
| vertical | | min. 2 | 20 mm |

 $(4)^{5}(6)^{7}$) and (8) see page 8

LIMITING VALUES

| Final accelerator voltage | $V_{g_9}(l)$ | max. min. | 10000 | v V |
|---|----------------------------------|--------------|--------------|--------------------|
| Geometry control electrode voltage | Vg8 | max. | 4400 | V |
| Vertical deflection system shield voltage | Vg7 | max. | 4400 | v |
| Beam centring electrode voltage | Vg6 | max. | 4400 | v |
| Astigmatism control electrode voltage | vg5 | max. min. | 4400 2500 | V V |
| Focusing electrode voltage | Vg4 | max. | 1500 | V |
| Deflection blanking electrode voltage | Sugar (Star) | max. | 4400 | v |
| First accelerator voltage | Vg2 | max. | 4400 | V |
| Control grid voltage, | lan bi Pan | | | |
| negative | -Vg1 | max. | 350 | V |
| positive | Vg1 | max. | 0 | v |
| positive peak | Vglp | max. | 2 | V |
| Cathode to heater voltage | 1. 20 Aug 12780. | | | |
| cathode positive | V+k/f- | max. | 200 | V |
| cathode negative | V-k/f+ | max. | 125 | V |
| Cathode current average | Ikeff | max. | 300 | mA |
| Screen dissipation | We | max. | 3 | mW/cm ² |
| Ratio $V_{g_9}(\ell)/V_{g_5}$ | $V_{g_9}(\ell)/V_{g_5}$ | max. | 10 | |
| Ratio V_{g_2}/V_{g_5} | Vg ₂ /Vg ₅ | max. | 1 | |

WARNING

This tube, when in operation, produces X-rays which may constitute a health hazard unless the tube is adequately shielded.

NOTES

D13-24.

- 1. Measured with coaxial 50 to 100 Ω quarter wavelength transformers with a 50 Ω coaxial precision resistance from Rohde and Schwarz, type RMD 33526/50 as reference standard.
- 2. The bandwidth is defined as the frequency at which the vertical sensitivity is 3 dB down with respect to that at D.C.
- 3. The risetime is defined to be the time interval between 10% and 90% of the final value of deflection, when a stepfunction signal is applied to the vertical deflection system.

The signal source will be built-in step function generator of a Tektronix type 519 oscilloscope with the built-in delay-line included in the signal path and an abrupt 125 to 100 Ω transition between the output of the delay-line and the input of the oscilloscope tube. The output connector of the tube will be terminated with a 100 Ω coaxial resistor type BB 1241. In order to avoid errors due to the angle of traces, two measurements are taken using a positive going and a negative going step function of equal amplitude and the risetime will be taken to be the arithmetic mean of the two values.

- 4. If the external conductors of the coaxial input and output connectors are not directly connected but capacitively coupled to this electrode, a vertical shift of the display can be obtained by varying the potential of this electrode.
- 5. The beam centring electrode voltage should be adjusted for equal deflection defocusing and deflection linearity in the x-direction with respect to the electrical centre of the tube.
- 6. The astigmatism electrode voltage should be corrected for optimum spot shape.
- 7. For visual extinction of a beam current of 10 μ A its potential will not exceed 110 V with respect to Vg₂.
- 8. The delay-line deflection system has been designed for an accelerator voltage of about 3000 V. Deviation from this value will cause deterioration of bandwidth and risetime. The potential of g2 should not vary within the duration of the brightness of the display may occur.

INSTRUMENT CATHODE-RAY TUBE

Oscilloscope tube with flat face, side connections to the deflector plates. The high sensitivities of this mesh tube render it suitable for transistorized equipment. The phosphor screen is metal backed.

| QUICK REFERENCE DATA | | | | |
|-------------------------------|--------------------|---------------|------|--|
| Final accelerator voltage | $V_{g_9}(l)$ | 15 | kV | |
| Display area | | 6 x 10 | cm | |
| Deflection factor, horizontal | M _X max | . 11.5 | V/cm | |
| vertical | M _y = | 2.9 | V/cm | |

SCREEN

| | Colour | Persistence |
|----------|--------------|--------------|
| D13-26GH | green | medium short |
| D13-26GP | bluish green | medium short |

| Useful screen diameter | min. | 114 | mm |
|---|------|-----|----|
| Useful scan at Vg ₉ (ℓ)/Vg4 = 10 | | | |
| horizontal | min. | 100 | mm |
| vertical | min. | 60 | mm |
| | | | |

Heater current

HEATING

| Indirect by A.C. | or D.C.; | parallel supply | |
|------------------|----------|-----------------|--|
| | | Heater voltage | |

| v_{f} | = | 6.3 | V |
|---------|---|-----|----|
| If | = | 300 | mA |

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MECHANICAL DATA Dimensions in mm 133#±1.5 2.0°±0.4 22 35±3min 2 55 R=706 .65±0.40 261±5 297±5 5 5.0°±0.4 Detail of side contact 0°±5° coil unit see detail 99 430±11 q 000 98 51ª ±1.5 i.c 012 X2 © g₉ i.c. 011 -max 19 6±0.5 .Y2 g4 95 Y1 ic -<u>g</u>3 g1 g_2 g_2 98 V g4 95 7207112 Dod 7207375

Mounting position: any

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

| Base | 14 pin all-glass | | | | |
|-------------------------------------|------------------|----------------------|----|--|--|
| Dimensions and connections | | | | | |
| Overall length | max. | 460 | mm | | |
| Face diameter | max. | 134.5 | mm | | |
| Net weight | approx. | 925 | g | | |
| Accessories | | | | | |
| Socket | type | 55566 | | | |
| Final accelerator contact connector | type | 55563 | | | |
| Side contact connector | type | 55561 | | | |
| Mu-metal shield | type | 55555 ¹) |) | | |
| | | | | | |

1) See page 6

| CAPACITANCES | | | | |
|--|-----------------|--------|-----|----|
| x_1 to all other elements except x_2 | $C_{x_1(x_2)}$ | = | 4.5 | pF |
| x_2 to all other elements except x_1 | $C_{x_2(x_1)}$ | = | 4.5 | pF |
| y_1 to all other elements except y_2 | $C_{y_1(y_2)}$ | - | 3.8 | pF |
| y_2 to all other elements except y_1 | $C_{y_2(y_1)}$ | = 1 | 3.8 | pF |
| x_1 to x_2 | $C_{x_1x_2}$ | = | 2.7 | pF |
| y ₁ to y ₂ | $c_{y_1y_2}$ | = | 1.8 | pF |
| Control grid to all other elements | C _{g1} | = | 5.5 | pF |
| Cathode to all other elements | Ck | = | 3.0 | pF |

FOCUSING electrostatic

| DEFLECTION | double electrostatic |
|------------|----------------------|
| x plates | symmetrical |
| y plates | symmetrical |

If use is made of the full deflection capabilities of the tube the deflection plates will intercept part of the electron beam; hence a low impedance deflection plate drive is desirable.

Angle between x and y traces

90° See "Correction coils"

LINE WIDTH

Measured with the shrinking raster method in the centre of the screen

| Final accelerator voltage | $V_{g_9}(l)$ | = | 15 000 | 15 000 | v |
|---------------------------------------|--------------|---|--------|--------|------------------|
| Astigmatism control electrode voltage | Vg4 | = | 2400 | 1500 | v ⁴) |
| First accelerator voltage | Vg2 | = | 2400 | 1500 | V |
| Beam current | I(l) | = | 10 | 10 | μA |
| Line width | 1.w. | = | 0.3 | 0.4 | mm |

⁴) See page 6

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| TYPICAL OPERATING CONDITION | NS | | | | | | |
|--|--|---------------------------------|--|--|---|--|---|
| Final accelerator voltage | | | Vg9() | 2) = | | 15 000 | V |
| Post deflection shield voltage | | | - status | | ionióló. | a dina di | 10.64 |
| (with respect to | v _{g7}) | | Vg8 | = 45 60 | -12 to | o -18 | V |
| Geometry control electrode voltage | | | Vg7 | = | 1500 | <u>+</u> 70 | V ²) |
| Interplate shield voltage | | | Vg6 | = | 1 | 1500 | V |
| Deflection plate shield voltage | | | vg5 | = | | 1500 | V ³) |
| Astigmatism control electrode volta | age | | vg4 | = | 1500 | <u>+</u> 70 | V 4) |
| Focusing electrode voltage | | | Vg3 | = | 375 to | 625 | V |
| First accelerator voltage | | | Vg2 | = | | 1500 | V |
| Control grid voltage for visual extin of focused | nction d spot | | -Vg1 | nautė E | 40 to | 90 | V |
| Deflection factor | | | iself a | | | | |
| horizontal | | | M _x | | 9.4 to | 0 12.5 | V/cm |
| vertical | | | M _v | nini Ta | 2.3 to | 3.5 | V/cm |
| Deviation of linearity of deflection | | | In a lite | o it,₹ | max. | 2 | % ⁵) |
| Geometry distortion | | | | | See not | te 6 | |
| Useful scan | | | | | | | |
| horizontal | | | | = | min. | 100 | mm |
| vertical | | | | = | min. | 60 | mm |
| CIRCUIT DESIGN VALUES | | | | | | | |
| Focusing voltage | Vara | | | | | | The Later |
| | 83 | = | 250 to | 417 | V per | kV of V | g4 |
| Control grid voltage for visual extinction of focused spot | -V _{g1} | = : | 250 to 30 to | 417 56.7 | V per | kV of V kV of V | /g ₄ /g ₂ |
| Control grid voltage for visual extinction of focused spot Deflection factor at $V_{g9(l)}V_{g4} = 10$ | -V _{g1} | = | 250 to 30 to | 417 56.7 | V per | kV of V kV of V | /g ₄ /g ₂ |
| Control grid voltage for visual extinction of focused spot Deflection factor at V _{g9(l)} V _{g4} = 10 horizontal | -V _{g1} M _x | = | 30 to 6.3 to | 417 56.7 8.4 | V per V per V/cm | kV of V kV of V per kV | /g ₄ /g ₂ of V _{g4} |
| Control grid voltage for visual extinction of focused spot Deflection factor at $V_{gg(l)}V_{g_4}$ = 10 horizontal vertical | -Vg ₁ M _x M _y | = = = 1 | 30 to 30 to 6.3 to .53 to | 417 56.7 8.4 2.33 | V per V per V/cm | kV of V kV of V per kV per kV | v_{g_2} of v_{g_4} of v_{g_4} |
| Control grid voltage for visual extinction of focused spot Deflection factor at $V_{gg(l)}V_{g4}$ = 10 horizontal vertical Control grid circuit resistance | Vg1 Mx My Rg1 | = = = 1 = m | 30 to 30 to 6.3 to .53 to nax. | 417 56.7 8.4 2.33 1 | V per V per V/cm V/cm | kV of V kV of V per kV per kV | v_{g_2} of v_{g_4} of v_{g_4} |
| Control grid voltage for visual extinction of focused spot Deflection factor at $V_{g9(\ell)}V_{g4}$ = 10 horizontal vertical Control grid circuit resistance Deflection plate circuit resistance | g3 -Vg1 M _x My Rg1 R _x ,Ry | = = = 1 = m = m | 30 to 30 to 6.3 to .53 to nax. | 417 56.7 8.4 2.33 1 50 | V per V per V/cm V/cm MΩ kΩ | kV of V kV of V per kV per kV | v_{g_2} of v_{g_4} of v_{g_4} |
| Control grid voltage for visual extinction of focused spot Deflection factor at $V_{gg(l)}V_{g4} = 10$ horizontal vertical Control grid circuit resistance Deflection plate circuit resistance Focusing electrode current at a beam current of max. 25 μ A | 93 -V _{g1} M _x My R _{g1} R _x ,Ry I _{g3} | = : = 1 = m = m = . | 30 to 30 to 6.3 to .53 to nax. nax. | 417 56.7 8.4 2.33 1 50 +25 | V per V per V per V/cm γ V/cm γ M Ω k Ω | kV of V kV of V per kV per kV | /g ₂ of V _{g4} of V _{g4} |

LIMITING VALUES (Absolute max. rating system)

| Final accelerator voltage | $v_{g_9(\ell)}$ | = | max. min. | 16500 9000 | V V |
|--|-----------------------------|-----|--------------|---------------|-----------|
| Post deflection shield voltage | v _{g8} | = | max. min. | 2500 1350 | v v |
| Geometry control electrode voltage | vg7 | = | max. min. | 2500 1350 | V V |
| Interplate shield voltage | Vg6 | = | max. min. | 2500 1350 | v v |
| Deflection plate shield voltage | v _{g5} | = | max. min. | 2500 1350 | V V |
| Astigmatism control electrode voltage | v _{g4} | = = | max. min. | 2500 1350 | V V |
| Focusing electrode voltage | v _{g3} | = | max. | 2500 | v |
| First accelerator voltage | v _{g2} | = | max. min. | 2500 1350 | v v |
| Control grid voltage | | | | | |
| negative | -v _{g1} | = | max. | 200 | v |
| positive | V _{g1} | 3 | max. | 0 | v |
| Voltage between astigmatism electrode and any deflection plate | $V_{g_4/x}$ $V_{g_4/y}$ | = = | max. max. | 500 500 | V V |
| Cathode to heater voltage | | | | | |
| cathode positive | V+k/f- | = | max. | 200 | `v |
| cathode negative | V-k/f+ | = | max. | 125 | v |
| Screen dissipation | Wl | = | max. | 3 | mW/cm^2 |
| Ratio $V_{g_9(l)}/V_{g_4}$ | $v_{g_{9}(\ell)}/v_{g_{4}}$ | = | max. | 10 | |
| Cathode current, average | Ik | = | max. | 300 | μA |

- 1) When putting the tube into the mu-metal shield care should be taken not to damage the side contacts.
 - ²) This tube is designed for optimum performance when operating at the ratio $V_{gg(\ell)}/V_{g_4} = 10$. Operation at other ratio may result in changes in deflection uniformity and geometry distortion. The geometry control electrode voltage should be adjusted for optimum performance. For any necessary adjustment its potential will be within the stated range.
 - ³) This voltage should be equal to the mean x- and y plates potential.
 - 4) The astigmatism control electrode voltage should be adjusted for optimum spot shape. For any necessary adjustment its potential will be within the stated range.
 - 5) The sensitivity at a deflection of less than 75% of the useful scan will not differ from the sensitivity at a deflection of 25% of the useful scan by more than the indicated value.
 - 6) A graticule, consisting of concentric rectangles of 100 mm x 60 mm and 98 mm x 58.2 mm is aligned with the electrical x axis of the tube. The edges of a raster will fall between these rectangles with optimum correction potentials applied.
 - ⁷) Values to be taken into account for the calculation of the focus potentiometer.

CORRECTION COILS

The D13-26.. is provided with a coil unit consisting of a pair of coils for:

- a. Correction of the orthogonality of the x and y traces (which means that at the centre of the screen the angle between the x and y traces can be made exactly 90°).
- b. Vertical shift of the scanned area.

DETAIL DRAWING OF COIL UNIT

Dimensions in mm



The currents required under typical operating conditions, the tube being screened by a mu-metal shield closely surrounding the coils (e.g. 55555), are max. 7 mA per degree of angle correction and max. 4 mA per mm of shift. If no such shield is used these values have to be multiplied by a factor k (1 < k < 2), the value of which depends on the diameter of the shield and approaches 2 for the case no shield is present.

The D.C. resistance is approx. 180 Ω per coil.

When designing the supply circuit for these coils it should be considered that the maximum current required in either coil can be 34 mA.

Circuit diagrams

A suitable circuit permitting independent controls of orthogonality correction and vertical shift is given in fig.1.



Fig.1

The dissipation in the potentiometers can be reduced considerably if the requirement of independent controls is dropped (see fig.2).



P₁, P₂ : Potentiometers, 220 Ω , 1 Watt, ganged P₃, P₄ : Potentiometers, 220 Ω , 1 Watt, ganged

Fig.2

A further reduction of the dissipation can be obtained by inserting a commutator for each coil (see fig.3).

The procedure of adjustment will then become more complicated, but it should be kept in mind that a readjustment is necessary only when the tube has to be replaced.



 P_1 , P_2 : Potentiometers, 500 Ω , 0,5 Watt S_1 , S_2 : Commutators



For the adjustment of the currents the following procedure is recommended:

- a. With the tube fully scanned in the vertical direction the scanned area must be shifted so that the useful vertical scan on either side of the geometric centre of the screen meets the published value of 30 mm min. With the circuit according to fig.l this is done by means of the ganged potentiometers P_1 and P_4 .
- b. Adjustment of orthogonality by means of the ganged potentiometers P_2 and P_3 in fig.1. A slight readjustment of P_1 and P_4 may be necessary afterwards.

With a circuit according to fig. 2 or 3 these corrections have to be performed by means of successive adjustments of the currents in the coils.

The most convenient deflection signal is a square waveform permitting an easy and fairly accurate check of orthogonality.

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INSTRUMENT CATHODE-RAY TUBE

The D13-26../01 is equivalent to the D13-26.. but features an internal graticule. This graticule can be illuminated.

MECHANICAL DATA

Dimensions in mm





Maximum angle between x-trace and x-axis of the graticule

 $\pm 5^{\circ}$

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ALIGNMENT

In order to align the x-trace and the x-axis of the graticule an image rotating coil may be used. This coil should be positioned at one third of the cone length, seen from the face end, and can be attached to the inner surface of the mumetal shield.

Under typical operating conditions maximum 90 ampere-turns are required for alignment.

ILLUMINATION

To illuminate the internal graticule the use of a light conductor (e.g. of Perspex) is obligatory. The following design considerations should be observed:

In order to achieve the most efficient light conductance the holes for the light bulb as well as the contact area with the front plate should be polished. The contact with the edges of the front plate should be as close as possible and the edges of the front plate and the corresponding hole in the light conductor should be parallel to achieve light beams perpendicular to the edges. It is advised to apply reflective material to the outer circumference of the conductor and if possible also to both planes (see drawing).



1) Reflective material.

- 3) Close and constant distance to front plate of tube. It is essential that the light conductor and the front plate of the tube are in plane.
- ⁴) If possible reflective material.

²⁾ Polished.

INSTRUMENT CATHODE-RAY TUBE

13 cm diameter flat faced short oscilloscope tube (max. 35 cm) with post-deflection acceleration by means of a helical electrode. The tube is provided with deflection blanking.

| QUICK REFEREN | NCE DATA |
|-------------------------------|--------------------------|
| Final accelerator voltage | $V_{g_8(\ell)} = 3000 V$ |
| Display area | 8 cm x full scar |
| Deflection factor, horizontal | $M_x = 24 V/cn$ |
| vertical | $M_y = 11.5 V/cm$ |

SCREEN

| | Colour | Persistence |
|----------|--------|--------------|
| D13-27GH | green | medium short |

Useful screen diameter

min. 114 mm

Useful scan at $V_{g_8(\ell)}/V_{g_5} = 2$

horizontal full scan vertical min. 80 mm

The useful scan may be shifted vertically to a max. of 4 mm with respect to the geometric centre of the faceplate.

HEATING

Indirect by A.C. or D.C.; parallel supply

Heater voltage Heater current $\frac{V_f}{I_f} = 6.3 \text{ V}$

MECHANICAL DATA

Dimensions in mm



Mounting position: any

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

Base 14 pin all glass

Dimensions and connections

| Overall length (also with socket type 55566) | max. | 350 | mm |
|--|-------|--------|----|
| Face diameter | max. | 135 | mm |
| Net weight | appro | x. 680 | g |
| Accessories | | | |
| Socket (supplied with tube) | type | 55566 | |
| Final accelerator contact connector | type | 55563 | |
| Mu metal shield | type | 55557 | |

CAPACITANCES

| \mathbf{x}_1 to all other elements except \mathbf{x}_2 | $C_{x_1(x_2)}$ | = | 4.5 | pF |
|--|---|---|-----|----|
| \mathbf{x}_2 to all other elements except \mathbf{x}_1 | $C_{x_2(x_1)}$ | = | 4.5 | pF |
| \mathbf{y}_1 to all other elements except \mathbf{y}_2 | ^C y ₁ (y ₂) | = | 5 | pF |
| \mathtt{y}_2 to all other elements except \mathtt{y}_1 | c _{y2} (y1) | = | 5.5 | pF |
| \mathbf{x}_1 to \mathbf{x}_2 | $C_{x_1x_2}$ | = | 2.5 | pF |
| y ₁ to y ₂ | $C_{y_1y_2}$ | = | 1.2 | pF |
| Grid No.1 to all other elements | Cg1 | 1 | 5.5 | pF |
| Cathode to all other elements | Ck | = | 5 | pF |
| Grid No.3 to all other elements | c_{g_3} | = | 10 | pF |
| FOCUSING electrostatic | | | | |
| DEFLECTION double electrostatic | | | | |

x plates symmetrical

y plates symmetrical

If use is made of the full deflection capabilities of the tube the deflection plates will intercept part of the electron beam; hence a low impedance deflection plate drive is desirable.

 $90^{\circ} \pm 1^{\circ}$

Angle between x and y traces

LINE WIDTH

Measured with the shrinking raster method in the centre of the screen.

| Final accelerator voltage | $v_{g_8(\ell)}$ | = | 3000 | V |
|---------------------------------------|-----------------|---|------|---------|
| Astigmatism control electrode voltage | vg5 | = | 1500 | v^3) |
| First accelerator voltage | vg2 | = | 1500 | V |
| Beam current | $I_{g_8(l)}$ | = | 10 | μA |
| Line width | 1.w. | = | 0.25 | mm |

HELIX

Post deflection accelerator helix resistance min. 50 M Ω The helix is connected between $g_8(\ell)$ and g

³) See page 5

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ODED ATTING

| I IPICAL OPERATING CONDITIONS | | | | |
|---|---------------------|---|---------------|------------------|
| Final accelerator voltage | Vg ₈ (l) | = | 3000 | V |
| Geometry control electrode voltage | Vg7 | = | 1500 ± 75 | V ¹) |
| Deflection plate shield voltage | V _{g6} | = | 1500 | v ²) |
| Astigmatism control electrode voltage | Vg5 | = | 1500 ± 75 | v ³) |
| Focusing electrode voltage | Vg4 | = | 300 to 550 | V |
| Deflection blanking electrode voltage | V _{g3} | = | 1500 | V |
| Deflection blanking control voltage | ΔV_{g_3} | = | max60 | V ⁴) |
| First accelerator voltage | Vg ₂ | = | 1500 | V |
| Control grid voltage for visual extinction of focused spot | v _{g1} | = | -38 to -135 | V |
| Deflection factor | | | | |
| horizontal | M _x | = | 21 to 27 | V/cm |
| vertical | M _v | = | 9.8 to 12.2 | V/cm |
| Deviation of linearity of deflection | and departure . | = | max. 2 | % ⁵) |
| Geometry distortion | | | See note 6 | |
| Useful scan | | | | |
| horizontal | | | full scan | |
| vertical | | = | min. 80 | mm |
| | | | | |

CIRCUIT DESIGN VALUES

| Focusing voltage | Vg4 | = 200 to 370 | V per kV of V _{g5} |
|--|------------------|----------------|-------------------------------|
| Control grid voltage for visual extinction of focused spot | -V _{g1} | = 25 to 90 | V per kV of V_{g_2} |
| Deflection factor at $V_{g_8(\ell)}/V_{g_5} = 2$ | | | |
| horizontal | $M_{\rm X}$ | = 14 to 18 | V/cm per kV of Vg5 |
| vertical | My | = 6.5 to 8.2 | V/cm per kV of Vg5 |
| Control grid circuit resistance | R _{g1} | = max. 1.5 | MΩ |
| Deflection plate circuit | | | |
| resistance | R_x, R_y | = max. 50 | kΩ |
| Focusing electrode current | Ig4 | = -15 to +10 | μA ⁷) 7Z2 7807 |
| Notes see page 5 | | | |

| stores of a birth of the state | | the strength of the second strength of the se | | |
|---|---|--|---|---|
| g system) | | | | |
| Vacion | = | max. | 3300 | V |
| 58(1) | Ξ | min. | 1800 | V |
| Vg7 | = | max. | 1700 | V |
| Vg ₆ | = | max. | 1700 | V |
| V | = | max. | 1700 | V |
| vg5 | = | min. | 1200 | V |
| Vg4 | = | max. | 1200 | V |
| Vg3 | = | max. | 1700 | V |
| Vg2 | = | max. | 1700 | V |
| | | | | |
| $-v_{g_1}$ | = | max. | 200 | V |
| -Vg1 | = | min. | 0 | V |
| | | | | |
| Vg5/x | = | max. | 500 | V |
| Vg5/y | = | max. | 500 | V |
| Wl | = | max. | 3 | mW/cm^2 |
| $V_{g_8(l)}/V_{g_5}$ | = | max. | 2 | |
| Ik | = | max. | 300 | μA |
| | g system) V _{g8} (ℓ) V _{g7} V _{g6} V _{g5} V _{g4} V _{g3} V _{g2} -V _{g1} -V _{g1} V _{g5/x} V _{g5/y} W _ℓ V _{g8} (ℓ)/V _{g5} I _k | g system) $V_{g_8(\ell)} =$ $V_{g_7} =$ $V_{g_6} =$ $V_{g_5} =$ $V_{g_3} =$ $V_{g_2} =$ $-V_{g_1} =$ $-V_{g_1} =$ $V_{g_5/x} =$ $V_{g_5/y} =$ $W_{\ell} =$ $V_{g_8(\ell)}/V_{g_5} =$ $I_k =$ | g system) $V_{g_8(\ell)} = \max$. $V_{g_7} = \max$. $V_{g_7} = \max$. $V_{g_6} = \max$. $V_{g_5} = \max$. $V_{g_5} = \max$. $V_{g_3} = \max$. $V_{g_2} = \max$. $-V_{g_1} = \max$. $-V_{g_1} = \max$. $V_{g_5/x} = \max$. $V_{g_5/y} = \max$. $V_{g_5/y} = \max$. $V_{g_8(\ell)}/V_{g_5} = \max$. $I_k = \max$. | g system) $V_{g_8(\ell)} = \max 3300$ $= \min 1800$ $V_{g_7} = \max 1700$ $V_{g_6} = \max 1700$ $V_{g_6} = \max 1700$ $V_{g_5} = \min 1200$ $V_{g_4} = \max 1200$ $V_{g_3} = \max 1700$ $V_{g_2} = \max 1700$ $V_{g_2} = \max 1700$ $V_{g_2} = \max 1700$ $V_{g_2} = \max 1700$ $V_{g_1} = \max 1700$ $V_{g_1} = \max 1700$ $V_{g_5/x} = \max 500$ $V_{g_5/y} = \max 500$ $V_{g_5/y} = \max 500$ $V_{g_8(\ell)}/V_{g_5} = \max 2$ $I_k = \max 300$ |

- ¹) This tube is designed for optimum performance when operating at the ratio $V_{gg(\ell)}/V_{g5} = 2$. Operation at other ratio may result in changes in deflection uniformity and geometry distortion. The geometry control electrode voltage should be adjusted for optimum performance. For any necessary adjustment its potential will be within the stated range.
- 2) This voltage should be equal to the mean x- and y plates potential.
- 3) The astigmatism control electrode voltage should be adjusted for optimum spot shape. For any necessary adjustment its potential will be within the stated range.
- ⁴) For beam blanking of a beam current of $10 \,\mu\text{A}$.
- 5) The sensitivity at a deflection of less than 75% of the usefull scanwill not differ from the sensitivity at a deflection of 25% of the useful scan by more than the indicated value.
- 6) A graticule, consisting of concentric rectangles of 100 mm x 60 mm and 97 mm x 58 mm is aligned with the electrical x axis of the tube. The edges of a raster will fall between these rectangles with optimum correction potentials applied.
- 7) Values to be taken into account for the calculation of the focus potentiometer.


INSTRUMENT CATHODE-RAY TUBE

Low accelerator voltage cathode-ray tube for monitoring purpose

| QUICK REFERENCE DATA | | | | | |
|-------------------------------|-----------------------------------|--|--|--|--|
| Accelerator voltage | $V_{g_4, g_2, y_2}(\ell) = 500 V$ | | | | |
| Display area | Both directions full scan | | | | |
| Deflection factor, horizontal | M _x = 56.5 V/cm | | | | |
| vertical | $M_v = 49 V/cm$ | | | | |

SCREEN

| linen i hallos | Colour | Persistence |
|----------------|--------|--------------|
| DH3-91 | green | medium short |

Useful screen diameter

min. 28 mm

Useful scan

| horizontal | full scan |
|------------|-----------|
| vertical | full scan |

HEATING:

Indirect by A.C. or D.C.; parallel supply

Heater voltage Heater current $\frac{V_f}{I_f} = 6.3 V}{I_f} = 300 mA$

MECHANICAL DATA

Dimensions in mm



Mounting position: any

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube

| Base | | English I | Loctal 8 | 8 pins | |
|-------------------|------------|-----------|----------|-------------|---|
| Dimensions and co | onnections | | | | |
| See also outline | drawing | | | | |
| Overall length | | max. | 105 | mm | |
| Face diameter | | max. | 30 | mm | |
| Net weight: | | approx. | 39 | g | |
| Accessories | | | | | |
| Socket | | type | 5902/ | 20 or 40213 | 3 |
| Mu-metal shield | d | type | 55525 | | |
| | | | | | |

| CA | PACITANCES | | | | | |
|----------------|------------------------------|-------------------|-----------------------------------|---|-----|----|
| \mathbf{x}_1 | to all other elements exce | pt x ₂ | $C_{x_1(x_2)}$ | = | 4.5 | pF |
| x2 | to all other elements exce | pt x ₁ | $C_{x_2(x_1)}$ | = | 4.5 | pF |
| У1 | to all other elements exce | pt y ₂ | Cy ₁ (y ₂) | = | 3.5 | pF |
| \mathbf{x}_1 | to x ₂ | | $C_{x_1x_2}$ | = | 1.0 | pF |
| Co | ntrol grid to all other elen | nents | Cg1 | = | 5.6 | pF |

FOCUSING

ADACITANCES

electrostatic self focusing

| DEFLECTION | double electrostatic |
|------------|----------------------|
| x plates | symmetrical |
| y plates | asymmetrical |

LINE WIDTH

| Measured on a circle of 25 mm diameter | Response | | | |
|--|------------------------------|---|-----|----|
| Accelerator voltage | $v_{g_4, g_2, y_2(\ell)}$ | = | 500 | v |
| Beam current | I(() | = | 0.5 | μΑ |
| Line width | l.w. | = | 0.6 | mm |

TYPICAL OPERATING CONDITIONS

| Accelerator voltage | $v_{g_4, g_2, y_2(l)}$ | = | | 500 | V |
|--|------------------------|----|---------|-----|------|
| Control grid voltage for visual extinction of focused spot | -Vg ₁ | н | 8 to | 27 | v |
| Deflection factor | | | | | |
| horizontal | M _X | = | 41 to | 72 | V/cm |
| vertical | My | = | 35 to | 63 | V/cm |
| Useful scan | | | | | |
| horizontal | | fu | ll scan | | |
| vertical | | fu | ll scan | | |

7Z2 5558

3

LIMITING VALUES (Absolute max. rating system)

| Accelerator voltage | $v_{g_4,g_2,y_2(\ell)}$ | = = | max. min. | 1000 350 | V V |
|---------------------------|-------------------------|-----|--------------|-------------|--------------------|
| Control grid voltage | | | | | |
| negative | -v _{g1} | = | max. | 200 | v |
| positive | Vg1 | = | max. | 0 | v |
| positive peak | Vglp | = | max. | 2 | v |
| Cathode to heater voltage | e la constantiantera L | | | | |
| cathode positive | V _{+k/f} - | = | max. | 200 | V |
| cathode negative | V-k/f+ | ≐ | max. | 125 | V |
| Screen dissipation | Wl | = | max. | 3 | mW/cm ² |

CIRCUIT DESIGN VALUES

| Control grid voltage for visual extinction of | | | | |
|---|-------------------------------|---|--------------|------------------------------------|
| focused spot | $-v_{g_1}$ | = | 16 to 54 | V per kV of V_{g_4, g_2, y_2} |
| Deflection factor | | | | |
| horizontal | $M_{\mathbf{X}}$ | = | 90 to 120 | V/cm per kV of Vg4, g2, y2 |
| vertical | My | = | 38.5 to 52.5 | V/cm per kV of V_{g_4, g_2, y_2} |
| Control grid circuit | | | | |
| resistance | R_{g_1} | = | max. 1 | MΩ |
| Deflection plate circuit resistance | R _x R _y | = | max. 5 | MΩ |

REMARK

A contrast improving transparent conductive coating connected to the accelerator electrode is present between glass and fluorescent layer. This enables the application of a high potential with respect to earth to the accelerator electrode, without the risk of picture distortion by touching the face (electrostatic body-effect).

INSTRUMENT CATHODE-RAY TUBE

Cathode-ray tube for monitoring purposes.

| QUICK REFERENCE DATA | | | | |
|-------------------------------|-------------------------------------|------|--|--|
| Accelerator voltage | $V_{g_3}(\ell) = 800 V_{g_3}(\ell)$ | 1 | | |
| Display area | Both directions full s | scan | | |
| Deflection factor, horizontal | $M_{\rm X}$ = 62.5 V | //cm | | |
| vertical | M _y = 40 V | //cm | | |

SCREEN

| datus Witter | colour | persistence |
|--------------|-----------------|--------------|
| DB7-5 | blue | medium short |
| DG7-5 | yellowish green | medium short |
| DP 7-5 | yellowish green | long |

min. 65 mm

full scan

full scan

Useful screen diameter

Useful scan

horizontal

vertical

HEATING

Indirect by A.C. or D.C.; parallel supply

| | Heater voltage | $\underline{v_{f}}$ | = | 6.3 | v |
|--|----------------|---------------------|---|-----|----|
| | Heater current | I_{f} | = | 310 | mA |



Mounting position: any

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

English Lostal Onin

| Dimensions and connections | | |
|----------------------------|-------|------------------|
| See also outline drawing | | |
| Overall length | max. | 160 mm |
| Face diameter | max. | 71 mm |
| Net weight: | appro | ox. 140 g |
| Accessories | | |
| Socket | type | 5906/20 or 40212 |
| Mu-metal shield | type | 55530 |
| | | |

| | D.7-5 |
|--|---|
| CAPACITANCES | |
| x_1 to all other elements except x_2 | $C_{x_1}(x_2) = 2.8 \text{ pF}$ |
| \mathbf{x}_2 to all other elements except \mathbf{x}_1 | $C_{x_2(x_1)} = 2.8 \text{ pF}$ |
| \mathbf{y}_1 to all other elements except \mathbf{y}_2 | $C_{y_1}(y_2) = 3.0 \text{ pF}$ |
| y_2 to all other elements except y_1 | $C_{y_2}(y_1) = 3.3 \text{ pF}$ |
| x_1 to x_2 | $C_{x_1x_2} = 0.8 \text{ pF}$ |
| y_1 to y_2 | $C_{y_1y_2} = 0.6 \text{ pF}$ |
| Control grid to all other elements | $C_{g_1} = 7.0 \text{ pF}$ |
| Cathode to all other elements | $C_k = 3.2 \text{ pF}$ |
| FOCUSING electrostatic | |
| DEFLECTION double electrost | atic |
| x plates symmetrical | |
| y plates symmetrical | |
| Angle between x and y traces | 90 ⁰ ±1.5 ⁰ |
| | |
| LINE WIDTH | |
| Measured on a circle of 50 mm diamete | r · |
| Accelerator voltage | $V_{g_3}(l) = 800 V$ |
| Beam current | $I_{(l)} = 0.5 \ \mu A$ |
| Line width | l.w. = 0.4 mm |
| | |
| TYPICAL OPERATING CONDITIONS | |
| Accelerator voltage | $V_{g_3(l)} = 800 V$ |
| Focusing electrode voltage | V_{g_2} = 200 to 300 V |
| Control grid voltage for visual extinction of focused spot | $-V_{g_1} = 0 \text{ to } 50 \text{ V}$ |
| Deflection factor, horizontal | $M_{\rm X}$ = 53 to 72 V/cm |
| vertical | $M_y = 33 \text{ to } 45 \text{ V/cm}$ |
| Geometry distortion | See note 1 page 4 |
| Useful scan, horizontal | full scan |
| vertical | full scan 7Z2 5574 |

| LIMITING VALUES (Absolute ma | ax. rating | sy | stem) | | | | 800 (APA) |
|--|---------------------------------|-----|--------------------|--------|--------------|-------------|--------------------|
| Accelerator voltage | | V | g ₃ (1) | = = | max. min. | 1000 800 | V V |
| Focusing electrode voltage | | V | g2 | = | max. | 400 | V |
| Control grid voltage | | V | | | max | 200 | V |
| negative | | - v | g ₁ | - | max. | 200 | v |
| positivé | | V | g ₁ | = | max. | 0 | V |
| positive peak | | V | g _{1p} | = | max. | 2 | V |
| Cathode to heater voltage cathode positive | | V | +k/f- | = | max. | 200 | V |
| cathode negative | | V | -k/f+ | = | max. | 125 | V |
| Voltage between accelerator elec and any deflection | ctrode plate | v | g3/x | = | max. | 500 | V |
| | | V | g3/y | = | max. | 500 | V |
| Screen dissipation | | W | l | = | max. | 3 | mW/cm^2 |
| CIRCUIT DESIGN VALUES | | | | | | | |
| Focusing voltage | vg2 | = | 250 to | 37 | 5 V p | er kV | of V _{g3} |
| Control grid voltage for visual extinction of focused spot | $-v_{g_1}$ | = | 0 to | 62. | 5 V p | er kV | of Vg3 |
| Deflection factor horizontal | M _X | = | 66 to | 9 | 0 V/c | m per | kV of Vg3 |
| vertical | My | = | 41 to | 5 | 6 V/c | m per | kV of Vg3 |
| Control grid circuit resistance | Rg1 | = | max. | 0. | 5 ΜΩ | | |
| Deflection plate circuit resistance | R _x , R _y | н | max. | | 5 ΜΩ | | |

4

¹) A graticule, consisting of concentric rectangles of 43.2 mm x 43.2 mm and 40 mm x 40 mm is aligned with the electrical x axis of the tube. The edges of a raster will fall between these rectangles with optimum correction potentials applied. 7Z2 5575

INSTRUMENT CATHODE-RAY TUBE

Cathode-ray tube for monitoring purposes.

| QUICK REFERE | NCE DATA | | | Lin |
|-------------------------------|----------------|-------|----------|--------|
| Accelerator voltage | Vg3(l |) = | 800 | V |
| Display area | Both di | recti | ions ful | l scan |
| Deflection factor, horizontal | M _x | s.5. | 62.5 | V/cm |
| vertical | My | = | 40 | V/cm |

SCREEN

| | colour | persistence |
|-------|-----------------|--------------|
| DB7-6 | blue | medium short |
| DG7-6 | yellowish green | medium short |
| DP7-6 | yellowish green | long |

| Useful screen diameter | min. 65 mm |
|------------------------|------------|
| Useful scan | |
| horizontal | full scan |
| vertical | full scan |
| HEATING | |

HEATING

| indiffect by A.C. of D.C. | ., parallel supply | | | | |
|---------------------------|--------------------|---------------------|---|-----|----|
| | Heater voltage | $\underline{v_{f}}$ | = | 6.3 | V |
| | Heater current | If | = | 310 | mA |

1

7Z2 5576

1

MECHANICAL DATA

Dimensions in mm



Mounting position: any

Base

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

English Loctal 9 pins

| Dimensions and connections | | |
|----------------------------|---------|-----------------|
| See also outline drawing | | |
| Overall length | max. | 160 mm |
| Face diameter | max. | 71 mm |
| Net weight: | approx. | 140 g |
| Accessories | | |
| Socket | type 5 | 906/20 or 40212 |
| Mu-metal shield | type 5 | 5530 |
| | | |

| | | | D | .7 | - 6 | 3 | |
|---|------------------|-----------------|-------------------|--------------|--------------|-----------|--|
| CAPACITANCES | | | | ्र । । | | | |
| \mathbf{x}_1 to all other elements except \mathbf{x}_2 | | C_{X_1} | (x_2) | = 2 | .8 | pF | |
| \mathbf{x}_2 to all other elements except \mathbf{x}_1 | | C_{X_2} | (x_1) | = 2 | .8 | pF | |
| y_1 to all other elements except y_2 | | C_{y_1} | (y ₂) | = 3 | .0 | pF | |
| y_2 to all other elements except y_1 | | C_{y_2} | (y ₁) | = 3 | .3 | pF | |
| x_1 to x_2 | | C _{x1} | x ₂ | = 0 | .8 | pF | |
| y_1 to y_2 | | Cy ₁ | y ₂ | = 0 | .6 | pF | |
| Control grid to all other elements | | C _{g1} | | = 7 | .0 | pF | |
| Cathode to all other elements | | Ck | | = 3 | .2 | pF | |
| FOCUSING electrostatic | | | | | | | |
| DEFLECTION double electrostatic | | | | | | | |
| x plates asymmetrical x_1 has to be connected Earthing of the accelerat | to the a | accelo de is | erator reco | ele mme | ctro ndec | de. 1. | |
| y plates symmetrical | | | | | | | |
| Angle between x and y traces $90^{\circ}\pm1.5$ | ;0 | | | | | | |
| LINE WIDTH | | | | | | | |
| Measured on a circle of 50 mm diameter | | | | | | | |
| Accelerator voltage | $V_{g_3(a)}$ | 1038 = | | 800 | v | | |
| Beam current | I(ℓ) | = | | 0.5 | μΑ | | |
| Line width | 1.w. | = | | 0.4 | mr | n | |
| TYPICAL OPERATING CONDITIONS | | | | | | | |
| Accelerator voltage | $V_{g_3(\ell)}$ | = | | 800 | v | | |
| Focusing electrode voltage | Vg2 | = | 200 to | 300 | v | | |
| Control grid voltage for visual extinction of focused spot | -V _{g1} | = | 0 to | 50 | v | | |
| Deflection factor, horizontal | M _x | = | 53 to | 72 | v/ | cm | |
| vertical | M _V | = | 33 to | 45 | v/ | cm | |
| Geometry distortion | | See | note | l pag | e 4 | | |
| Useful scan, horizontal | | full | scan | | | | |
| vertical | | full | scan | 72 | 22 58 | 578 | |

| LIMITING VA | ALUES (Absolute ma | x. rating | sy | stem) | | | | |
|----------------------------|--|---------------------------------|----|-----------------|-----|--------------|-------------|--------------------|
| Accelerator | voltage | | V | g3(l) | = | max. min. | 1000 800 | V V |
| Focusing elec | ctrode voltage | | v | g ₂ | = | max. | 400 | v |
| Control grid | voltage negative | | -V | g ₁ | = | max. | 200 | v |
| lla shu | positive | | V | g ₁ | = | max. | 0 | V |
| | positive peak | | V | g _{1p} | = | max. | 2 | v |
| Cathode to he | ater voltage cathode positive | | v | +k/f- | = | max. | 200 | v |
| | cathode negative | | V | -k/f+ | = | max. | 125 | v |
| Voltage betwe | een accelerator electand any deflection | trode plate | v | g3/x | = | max. | 500 | v |
| | | | V | g3/y | = | max. | 500 | v |
| Screen dissip | pation | | И | 'e | = | max. | 3 | mW/cm ² |
| CIRCUIT DES | SIGN VALUES | | | | | | | |
| Focusing volt | age | v_{g_2} | = | 250 to | 37 | 5 V pe | er kV | of Vg3 |
| Control grid extinction | voltage for visual on of focused spot | -v _{g1} | = | 0 to | 62. | 5 V pe | er kV | of V _{g3} |
| Deflection fac ho | ctor rizontal | M _X | - | 66 to | 9 | 0 V/c | m per | kV of Vg3 |
| ve | rtical | My | = | 41 to | 5 | 6 V/c | m per | kV of Vg3 |
| Control grid | circuit resistance | Rg1 | = | max. | 0. | 5 MΩ | | |
| Deflection pla | ate circuit resistance | R _x , R _y | = | max. | | 5 MΩ | | |

¹) A graticule, consisting of concentric rectangles of 43.2 mm x 43.2 mm and 40 mm x 40 mm is aligned with the electrical x axis of the tube. The edges of a raster will fall between these rectangles with optimum correction potentials applied. 7Z2 5575

INSTRUMENT CATHODE-RAY TUBE

Oscilloscope tube with 7 cm diameter flat face plate and post deflection acceleration by means of a helical electrode. The low heater consumption together with the high sensitivity render this tube suitable for transistorized equipment.

| QUICK REFERENCE DATA | | | | | | | | |
|-------------------------------|----------------|----------------|-------|------|--|--|--|--|
| Final accelerator voltage | $V_{g_6(l)}$ | = | 1200 | V | | | | |
| Display area | | = | 4.5x6 | cm | | | | |
| Deflection factor, horizontal | M _x | (= | 10.7 | V/cm | | | | |
| vertical | M _v | 9 - | 3.65 | V/cm | | | | |

SCREEN

| | Colour | Persistence |
|--------|-----------------|--------------|
| DB7-11 | blue | medium short |
| DH7-11 | green | medium short |
| DN7-11 | bluish green | medium short |
| DP7-11 | yellowish green | long |

| Useful screen | diameter | min. |
|----------------|-----------------------------|------|
| Useful scan at | $V_{g_6(\ell)}/V_{g_4} = 4$ | |
| | horizontal | min. |
| | vertical | min. |

HEATING

Indirect by A.C. or D.C.; parallel supply

Heater voltage Heater current $\frac{V_{f}}{I_{f}} = 6.3 V$

68

60 mm

45

mm

mm





Mounting position: any

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube

Base 14 pins all glass

Dimensions and connections

| Overall length | max. | 296 | mm |
|-------------------------------------|-------|--------|----|
| Face diameter | max. | 77.8 | mm |
| | | | |
| Net weight | appro | x. 370 | g |
| Accessories | | | |
| Socket (supplied with tube) | type | 40467 | |
| Final accelerator contact connector | type | 55563 | |
| Mu-metal shield | type | 55532 | |
| | | | |

CAPACITANCES

| x_1 to all other elements except x_2 | $C_{x_1(x_2)}$ | = | 4.0 | pF |
|--|-----------------------------------|---|-----|----|
| \mathbf{x}_2 to all other elements except \mathbf{x}_1 | $C_{x_2(x_1)}$ | = | 4.0 | pF |
| y_1 to all other elements except y_2 | $C_{y_1(y_2)}$ | = | 3.5 | pF |
| y_2 to all other elements except y_1 | C _{y2} (y ₁) | = | 3.5 | pF |
| x_1 to x_2 | $C_{x_1x_2}$ | = | 1.9 | pF |
| y ₁ to y ₂ | $c_{y_1y_2}$ | = | 1.7 | pF |
| Control grid to all other elements | C _{g1} | = | 5.7 | pF |
| Cathode to all other elements | C _k | = | 3.0 | pF |

FOCUSING

electrostatic

double electrostatic

DEFLECTION

x plates symmetrical y plates symmetrical

If use is made of the full deflection capabilities of the tube the deflection plates will intercept part of the electron beam; hence a low impedance deflection plate drive is desirable.

Angle between x and y traces

 $90^{\circ} \pm 1^{\circ}$

LINE WIDTH

Measured with the shrinking raster method in the centre of the screen.

| Final accelerator voltage | $v_{g_6(\ell)}$ | = 10 | 1200 | V |
|---------------------------------------|-----------------|------|------|------------------|
| Astigmatism control electrode voltage | Vg ₄ | = | 300 | V ²) |
| First accelerator voltage | Vg2 | = | 1200 | V |
| Beam current | I(l) | = | 10 | μA |
| Line width | 1.w. | = | 0.65 | mm |

HELIX

Post deflection accelerator helix resistance min. 40 M Ω

2) See page 6

| TYPICAL OPERATING CONDITIONS | | | |
|--|--------------------|---|------------------|
| Final accelerator voltage | $V_{g_6(l)} =$ | 1200 | V |
| Geometry control electrode voltage | V _{g5} = | 300 <u>+</u> 30 | V ¹) |
| Astigmatism control electrode voltage | Vg ₄ = | $300 \pm \begin{array}{c} 40 \\ 15 \end{array}$ | V ²) |
| Focusing electrode voltage | V _{g3} = | 20 to 150 | V |
| First accelerator voltage | Vg ₂ = | 1200 | V |
| Control grid voltage for visual extinction of focused spot | -V _{g1} = | 30 to 80 | V |
| Deflection factor | | | |
| horizontal | M _X = | 9.4 to 12 | V/cm |
| vertical | M _y = | 3.2 to 4.1 | V/cm |
| Deviation of linearity of deflection | | max. 2 | % ³) |
| Geometry distortion | | See note 4) | |
| Useful scan | | | |
| horizontal | e north hout | min. 60 | mm |
| vertical | and birth the | min. 40 | mm |
| | | | |

CIRCUIT DESIGN VALUES

| Focusing voltage | Vg3 | Ξ | 35 to | 165 | V per kV of V_{g_4} |
|--|-------------|---|---------|------|--------------------------|
| Control grid voltage for visual extinction of focused spot | -Vg1 | = | 30 to | 60 | V per kV of V_{g_2} |
| Deflection factor at | | | | | |
| $V_{g_6(\ell)}/V_{g_4} = 4$ | | | | | |
| horizontal | $M_{\rm X}$ | = | 31.3 to | 40.0 | V/cm per kV of V_{g_4} |
| vertical | My | Ξ | 10.7 to | 13.7 | V/cm per kV of V_{g_4} |
| Control grid circuit resistance | Rg1 | = | max. | 1.5 | MΩ |
| Deflection plate circuit | | | | | |
| resistance | R_x, R_y | = | max. | 50 | kΩ |
| Focusing electrode current | Ig3 | = | —15 to | +10 | μA ⁵) |

¹)²)³)⁴)⁵) See page 6

| Line in the second seco | ing of occurry | | | | |
|--|--------------------|---|------|------|--------------------|
| Final accelerator voltage | Vala | = | max. | 5000 | V |
| i mai accelerator voltage | ·g6(1) | = | min. | 1200 | V |
| Geometry control electrode voltage | Vg5 | = | max. | 2200 | V |
| Astigmatism control electrode | | - | max | 2100 | V |
| voltage | Vg4 | = | min. | 300 | V |
| Focusing electrode voltage | Vg3 | = | max. | 1000 | V |
| First appelarator voltage | V | = | max. | 1600 | V |
| First accelerator voltage | vg ₂ | = | min. | 800 | V |
| Control grid voltage | | | | | |
| negative | $-v_{g_1}$ | = | max. | 200 | V |
| positive | V _{g1} | = | max. | 0 | V |
| positive peak | Vglp | = | max. | 2 | V |
| Cathode to heater voltage | | | | | |
| cathode positive | V+k/f- | = | max. | 100 | V |
| cathode negative | V-k/f+ | = | max. | 15 | V |
| Voltage between astigmatism control electrode and any deflection plate | Vg4/x | = | max. | 500 | v |
| · · · · · · · · · · · · · · · · · · · | Vg4/y | = | max. | 500 | V |
| Screen dissipation | Wl | = | max. | 3 | mW/cm ² |
| Ratio Vg6(1)/Vg4 | $V_{g6(l)}/V_{g4}$ | - | max. | 4 | |

Statistics of the second

LIMITING VALUES (Absolute max. rating system)

- ¹) This tube is designed for optimum performance when operating at the ratio $V_{g6(\ell)}/V_{g4} = 4$. Operation at other ratio may result in changes in deflection uniformity and geometry distortion. The geometry control electrode voltage should be adjusted for optimum performance. For any necessary adjustment its potential will be within the stated range.
- ²) The astigmatism control electrode voltage should be adjusted for optimum spot shape. For any necessary adjustment its potential will be within the stated range.
- ³) The sensitivity at a deflection of less than 75% of the useful scan will not differ from the sensitivity at a deflection of 25% of the useful scan by more than the indicated value.
- 4) A graticule, consisting of concentric rectangles of 40.8 mm x 40.8 mm and 39.2 mm x 39.2 mm is aligned with the electrical x axis of the tube. The edges of a raster will fall between these rectangles with optimum correction potentials applied.
- 5) Values to be taken into account for the calculation of the focus potentiometer.



A



INSTRUMENT CATHODE-RAY TUBE

Low accelerator voltage cathode-ray tube for monitoring purposes.

| QUICK REFERENCE DATA | | | | | | | |
|-------------------------------|---------------------------|--|--|--|--|--|--|
| Final accelerator voltage | $V_{g_4,g_2(l)} = 500 V$ | | | | | | |
| Display area | Both directions full scan | | | | | | |
| Deflection factor, horizontal | M _x = 37 V/cm | | | | | | |
| vertical | M _y = 21 V/cm | | | | | | |

SCREEN

| | Colour | Persistence |
|--------|-----------------|-------------|
| DG7-31 | yellowish green | medium |

Useful screen diameter

Useful scan

horizontal vertical

HEATING

Indirect by A.C. or D.C.; parallel supply

| Heater | voltage | V_{f} | = | 6.3 | V |
|--------|---------|---------|---|-----|----|
| Heater | current | I_{f} | = | 300 | m. |

min. 65 mm

full scan full scan

MECHANICAL DATA

Dimensions in mm



Mounting position: any

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

Base Duodecal 12 pins

| Dimensions and connections | | a sha si | |
|----------------------------|---------|----------|----|
| See also outline drawing | | | |
| Overall length | max. | 172 | mm |
| Face diameter | max. | 71 | mm |
| Net weight: | approx. | 120 | g |
| Accessories | | | |
| Socket | type 5 | 5912/2 | 0 |
| Mu-metal shield | type 5 | 55530 | |

| CAPACITANCES | | | | | | | | |
|--|--|---------------------------------------|-------------------|----------------|-----|------|------|---|
| \mathbf{x}_1 to all other eleme | | | $C_{x_1(x_2)}$ | = | 3.7 | pF | | |
| x ₂ to all other elements except x ₁ | | | | $C_{x_2(x_1)}$ | = | 3.0 | pF | : |
| y_1 to all other elem | ents except y ₂ | | | $C_{y_1(y_2)}$ | = | 2.5 | pF | |
| y_2 to all other elem | ents except y ₁ | | | $C_{y_2(y_1)}$ | = | 2.5 | pF | |
| \mathbf{x}_1 to \mathbf{x}_2 | | | | $C_{x_1x_2}$ | = | 1.7 | pF | |
| y_1 to y_2 | | | | $C_{y_1y_2}$ | = | 1.0 | pF | |
| Control grid to all o | ther elements | | | C_{g_1} | = | 7.6 | pF | |
| Cathode to all other | elements | | | C _k | = | 3.2 | pF | |
| FOCUSING | electrostatic | | | | | | | |
| DEFLECTION | double electrost | atic | | | | | | |
| x plates | asymmetrical | | | | | | | |
| y plates | symmetrical | | | | | | | |
| Angle between x | and y traces | $90^{\circ} \pm 1.5^{\circ}$ | | | | | | |
| LINE WIDTH | | | | | | | | |
| Measured on a circl | e of 50 mm diameter | | | | | | | |
| Accelerator voltage | | $V_{g_4, g_2(\ell)}$ | = | | 50 | 00 1 | V | |
| Beam current | | I(l) | = | | 0. | .5 ¢ | AL | |
| Line width | diu maja i | 1.w. | = | | 0. | .4 1 | mm | |
| TYPICAL OPERATIN | NG CONDITIONS | | | | | | | |
| Accelerator voltage | | $V_{g_4,g_2(\ell)}$ | = | | 50 | 00 | v | |
| Focusing electrode | voltage | V _{g3} | = | 0 to | 12 | 20 7 | V | |
| Control grid voltage extinction of fo | e for visual ocused spot | -V _{g1} | = | 50 to | 1(| . 00 | v | |
| Deflection factor, h | norizontal | M _X | = | 33.3 to | 41 | .5 | V/cm | |
| v | vertical | M _v | = | 18.8 to | 23 | .2 | V/cm | |
| Geometry distortion | n litudia operati di ne a un si 1 ₉₁₇ - permit un coperativi | theonical patron total solida mice | See note 1 page 4 | | | | | |
| Useful scan, horizontal | | | full scan | | | | | |
| vertic | | fu | ll scan | | | | | |

1.1.1966

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D.7-31

| LIMITING VA | LUES (Absolute max. | . rating | sy | stem) | | | | | |
|----------------|------------------------|----------------|-----|-----------------|-----|-----|-------|----------------|------------------------|
| Asselsmatan | alta an | | V | | | = | max. | 800 | V |
| Accelerator | onage | | ٧g | 54,g2 | (1) | = | min. | 400 | V |
| Focusing elec | trode voltage | | Vg | 33 | | = | max. | 200 | v |
| Control grid | voltage | | | | | | | | |
| 20 6 S 1 1 | negative | - | -Vg | 51 | | = | max. | 200 | V |
| I | positive | | Vg | 31 | | = | max. | 0 | V |
| 14. De 16 - 1 | positive peak | | Vg | g1p | | = | max. | 2 | V |
| Cathode to he | ater voltage | | | | | | | | |
| (| cathode positive | | V- | -k/f- | | = | max. | 200 | V |
| | cathode negative | | v- | -k/f+ | | = | max. | 125 | V |
| Voltage betwe | en accelerator electr | ode | | | | | | | |
| | and any deflection pla | ate | Vg | f_{Λ}/x | | = | max. | 500 | V |
| | | | Vg | 34/y | | = | max. | 500 | V |
| Screen dissip | ation | | W | l | | = | max. | 3 | mW/cm^2 |
| CIRCUIT DES | GIGN VALUES | | | | | | | | |
| Focusing volt | age | Vg3 | = | 0 | to | 24 | 0 V p | er kV | of Vg |
| Control grid | voltage for visual | | | | | | | | |
| extinctio | on of focused spot | $-Vg_1$ | = | 100 | to | 20 | 0 V p | er kV | of V_{g_2} |
| Deflection fac | tor at $V_g(l)/V_g$ | | | | | | | | |
| | horizontal | M _x | Ξ | 67 | to | 8 | 3 V/d | cm pe | r kV of V _g |
| | vertical | My | = | 37.6 | to | 46. | 4 V/a | cm pe | r kV of Vg |
| Control grid | circuit resistance | Rg1 | = | max. | | 0. | 5 MΩ | 2 | |
| Deflection pla | te circuit | | | | | | | | |
| F | resistance | R_x, R_y | = | max. | | | 5 MS | 2 | |
| Focusing elec | trode current | Ig | = | -15 | to | +1 | 0 μΑ | ²) | |

1) A graticule, consisting of concentric rectangles of 43.2 mm x 43.2 mm and 40 mm x 40 mm is aligned with the electrical x axis of the tube. The edges of a raster will fall between these rectangles with optimum correction potentials applied.

2) Values to be taken into account for the calculation of the focus potentiometer.

Remark: A contrast improving transparent conductive coating connected to g_4, g_2 is present between glass and fluorescent layer. This enables the application of a high potential to g_4, g_2 with respect to earth, without the risk of picture distortion by touching the face (electrostatic body-effect)

INSTRUMENT CATHODE-RAY TUBE

Low accelerator voltage cathode-ray tube for monitoring purposes.

| QUICK REFERENCE DATA | | | | | | | | |
|-------------------------------|---------------------------|--|--|--|--|--|--|--|
| Final accelerator voltage | V_{g} (1) = 500 V | | | | | | | |
| Display area | Both directions full scan | | | | | | | |
| Deflection factor, horizontal | M _x = 37 V/cm | | | | | | | |
| vertical | M _y = 21 V/cm | | | | | | | |

SCREEN

| | Colour | Persistence |
|--------|-----------------|-------------|
| DG7-32 | yellowish green | medium |

min. 65

mm

Useful screen diameter

Useful scan

horizontal full scan vertical full scan

HEATING

Indirect by A.C. or D.C.; parallel supply

| Heater voltage | V_{f} | = | 6.3 | V |
|----------------|---------|---|-----|----|
| Heater current | If | = | 300 | mA |

MECHANICAL DATA

Dimensions in mm



Mounting position: any

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

| Base | Duodecal 12 | pins |
|------|-------------|------|
| | | |

| Dimensions and connections | | |
|----------------------------|--------|---------|
| See also outline drawing | | |
| Overall length | max. | 172 mm |
| Face diameter | max. | 71 mm |
| Net weight: | approx | . 120 g |
| Accessories | | |
| Socket | type | 5912/20 |
| Mu-metal shield | type | 55530 |

| | | | | D .1 | -32 |
|----------------------------------|------------------------------|---|---------------------|-----------------|-------|
| CAPACITANCES | | | | | |
| x_1 to all other ele | ements except x ₂ | | $C_{x_1}(x_2)$ |) = 3 | .7 pF |
| x_2 to all other ele | ements except x ₁ | | $C_{x_2}(x_1)$ |) = 3 | .0 pF |
| y_1 to all other ele | ements except y ₂ | | C _{y1} (y2 |) = 2 | .5 pF |
| y_2 to all other ele | ements except y ₁ | | $C_{y_2}(y_1)$ |) = 2 | .5 pF |
| \mathbf{x}_1 to \mathbf{x}_2 | | | $C_{x_1x_2}$ | = 1 | .7 pF |
| y_1 to y_2 | | | $C_{y_1y_2}$ | = 1 | .0 pF |
| Control grid to al | l other elements | | C _{g1} | = 7 | .6 pF |
| Cathode to all oth | er elements | | Ck | = 3 | .2 pF |
| FOCUSING | electrostatic | | | | |
| DEFLECTION | double electrosta | tic | | | |
| x plates | symmetrical | | | | |
| x plates | symmetrical | | | | |
| Angle between | x and y traces | 900 ± 1.50 | | | |
| Tingle Detween | r w und y truces | <u>, , , , , , , , , , , , , , , , , , , </u> | | | |
| LINE WIDTH | | | | | |
| Measured on a ci | rcle of 50 mm diamete | er | | | |
| Accelerator volta | ge | $V_{g_4, g_2(\ell)}$ | - 2011 - 2010 ≓ | 500 | V |
| Beam current | | I(L) | - | 0.5 | μA |
| Line width | | l.w. | - | 0.4 | mm |
| TYPICAL OPERA | TING CONDITIONS | | | | |
| Accelerator volta | ge | V_{σ} | = | 500 | v |
| Focusing electroc | le voltage | V_{σ_2} | = 0 t | o 120 | v |
| Control grid volta | ige for visual | 53 | | | |
| extinction of | focused spot | -v _{g1} | = 50 t | o 100 | V |
| Deflection factor, | horizontal | M _x | = 33.3 t | o 41.5 | V/cm |
| | vertical | My | = 18.8 t | o 23.2 | V/cm |
| Geometry distort | ion | | See note | 1 page | 4 |
| Useful scan, hor: | izontal | | full scar | id uses | |
| vert | tical | | full scar | u di setta L | |

7Z2 5582

7-22

| LIMITING VALUE | S (Absolute max | . rating | sy | stem) | | | | |
|--------------------------------------|---|------------------|----------|--|----------|--------------|----------------|------------------------|
| Accelerator voltag | re | | v | $g_{4}, g_{2}(l)$ | п п | max. min. | 800 400 | V V |
| Focusing electrode | voltage | | V | g3 | = | max. | 200 | V |
| Control grid voltag | ge | | | | | | | |
| negat | ive | | $-V_g$ | g1 | = | max. | 200 | V |
| positi | ve | | V | g1 | . = | max. | 0 | V |
| positi | ve peak | | Vg | g _{1p} | = | max. | 2 | V |
| Cathode to heater catho | voltage de positive | | V- | +k/f- | = | max. | 200 | V |
| catho | de negative | | V | -k/f+ | = | max. | 125 | V |
| Voltage between ac and | ccelerator electr any deflection pl | ode ate | Vg Vg | g ₄ /x g ₄ /y | II South | max. max. | 500 500 | V V |
| Screen dissipation | | | W | l | = | max. | 3 | mW/cm ² |
| CIRCUIT DESIGN | VALUES | | | | | | | |
| Focusing voltage | | Vg3 | = | 0 to | 24 | 40 V p | er kV | of Vg |
| Control grid voltage extinction of a | ge for visual focused spot | -V _{g1} | . = | 100 to | 20 | 00 V p | er kV | of V _{g2} |
| Deflection factor a | t V _{g(l)} /V _g horizontal | M _x | = | 67 to | 8 | 33 V/c | em per | r kV of V _s |
| | vertical | My | = | 37.6 to | 46. | 4 V/c | m per | r kV of Vg |
| Control grid circu | it resistance | Rg1 | = | max. | 0. | 5 MΩ | ! | tis key bi |
| Deflection plate cit | rcuit | R R | _ | max | | 5 MO | | |
| Focusing electrode | e current | I _a | = | -15 to | +1 | $0 \mu A$ | ²) | |

¹) A graticule, consisting of concentric rectangles of 43.2 mm x 43.2 mm and 40 mm x 40 mm is aligned with the electrical x axis of the tube. The edges of a raster will fall between these rectangles with optimum correction potentials applied.

 2) Values to be taken into account for the calculation of the focus potentiometer.

Remark: A contrast improving transparent conductive coating connected to g_4, g_2 is present between glass and fluorescent layer. This enables the application of a high potential to g_4, g_2 with respect to earth, without the risk of picture distortion by touching the face (electrostatic body-effect)

INSTRUMENT CATHODE-RAY TUBE

Oscilloscope tube with 7 cm diameter flat face-plate. The tube is intended for small service oscilloscopes.

| QUICK REFERENCE DATA | | | | | | | | | |
|-------------------------------|--------------------|---|-----------|------|--|--|--|--|--|
| Final accelerator voltage | V _g (l) | = | 1500 | V | | | | | |
| Display area | | = | 5.7 x 6.8 | cm | | | | | |
| Deflection factor, horizontal | M _x | = | 27.3 | V/cm | | | | | |
| vertical | My | = | 18.8 | V/cm | | | | | |

SCREEN

| | Colour | Persistence |
|--------|-----------------|--------------|
| DB7-36 | blue | medium short |
| DG7-36 | yellowish green | medium |

Useful scan

| horizontal | min. | 68 | mm | |
|------------|------|----|----|--|
| vertical | min. | 57 | mm | |

HEATING

Indirect by A.C. or D.C.; parallel supply

| Heater voltage | V _f | = | 6.3 | v |
|----------------|--------------------|---|-----|----|
| Heater current | $\overline{I_{f}}$ | = | 300 | mA |

7Z2 5620

11.11.1966

MAINTENANCE TYPE

1

MECHANICAL DATA

Dimensions in mm



Mounting position: any

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

| ecal 12 pins |
|--------------|
| e |

Dimensions and connections

See also outline drawing

| Overall length | max. 296 | mm |
|-----------------|--------------|----|
| Face diameter | max. 77.8 | mm |
| Net weight: | approx. 370 | g |
| Accessories | | |
| Socket | type 5912/20 | |
| Mu-metal shield | type 55531 | |

pF

pF

pF

pF

pF

pF

 $C_{x_1(x_2)} = 6.0 \text{ pF}$

 $C_{x_2(x_1)} = 6.0$

 $C_{y_1}(y_2) = 4.7$

 $C_{y_2(y_1)} = 4.7$

 $C_{X_1X_2} = 1.9$

= 1.7

=

=

5.7

3.3 pF

 $C_{y_1y_2}$

Cg₁

Ck

CAPACITANCES

x1 to all other elements except x_2 x2 to all other elements except x_1 y1 to all other elements except y_2 y2 to all other elements except y_1 x1 to x_2 y1 to y2 Control grid to all other elements Cathode to all other elements

FOCUSING

electrostatic

symmetrical

double electrostatic

DEFLECTION

x plates symmetrical

y plates

If use is made of the full deflection capabilities of the tube the deflection plates will intercept part of the electron beam; hence a low impedance deflection plate drive is desirable.

Angle between x and y traces

 $90^{\circ} \pm 1^{\circ}$

LINE WIDTH

Measured on a circle of 50 mm diameter

| Final accelerator voltage | $v_{g_4, g_2(l)}$ | = | 1500 | V |
|---------------------------|-------------------|---|------|----|
| Beam current | I(1) | = | 0.5 | μA |
| Line width | l.w. | = | 0.4 | mm |

7Z2 5622

3

TYPICAL OPERATING CONDITIONS

| Accelerator voltage | $V_{g_4,g_2(\ell)}$ | = | | 1500 | V |
|--|---------------------|----|-----------|------|------------------|
| Focusing electrode voltage | Vg3 | = | 247 to | 397 | V |
| Control grid voltage for visual extinction of focused spot | -Vg1 | - | 40 to | 80 | V |
| Deflection factor | | | | | |
| horizontal | M _X | = | 24.5 to | 30 | V/cm |
| vertical | My | = | 17.0 to | 20.5 | V/cm |
| Deviation of linearity of deflection | | = | max. | 2 | % ¹) |
| Geometry distortion | | Se | ee note 2 | | |
| Useful scan | | | | | |
| horizontal | | Ξ | min. | 68 | mm |
| vertical | | = | min. | 57 | mm |
| LIMITING VALUES (Absolute max. ratir | ig system) | | | | |

= max. 2500 V Final accelerator voltage $V_{g_4}, g_2(l) = min. 1000$ V Focusing electrode voltage Vg3 = max. 1000 V Control grid voltage $-v_{g_1}$ 200 negative = max. V v_{g_1} positive = max. 0 V Vg_{1p} 2 V positive peak = max. Cathode to heater voltage cathode positive $V_{+k/f}$ -200 V = max. cathode negative $V_{-k/f+}$ 125 V = max. Voltage between final accelerator and any deflection plate $V_{g_4,g_2/x_p}$ = max. 500 V $V_{g_4,g_2/y_p} = \max$. 500 V 3 mW/cm^2 Screen dissipation Wo = max.

1)2) See page 5

CIRCUIT DESIGN VALUES

| Focusing voltage | Vg3 | = 165 to 2 | 265 | V per kV of V_{g_4,g_2} |
|---|---------------------------------|--------------|-----|--------------------------------|
| Control grid voltage for vis- ual extinction of focused spot | -v _{g1} | = 27 to | 53 | V per kV of V _{g4,g2} |
| Deflection factor | | | | |
| horizontal | M _x | = 16.3 to 20 | 0.0 | V/cm per kV of $V_{g4,g2}$ |
| vertical | My | = 11.2 to 13 | 3.7 | V/cm per kV of V_{g_4, g_2} |
| Control grid circuit | | | | |
| resistance | R_{g_1} | = max. | 1.5 | MΩ |
| Deflection plate circuit | | | | |
| resistance | R _x , R _y | = max. | 5 | MΩ |
| Focusing electrode current | Ig3 | = -15 to $+$ | +10 | μΑ ³) |

 3) Values to be taken into account for the calculation of the focus potentiometer.

¹) The sensitivity at a deflection of less than 75% of the useful scan will not differ from the sensitivity at a deflection of 25% of the useful scan by more than the indicated value.

²) A graticule, consisting of concentric rectangles of 40.8 mm x 40.8 mm and 39.2 mm x 39.2 mm is aligned with the electrical x axis of the tube. The edges of a raster will fall between these rectangles with optimum correction potentials applied.



INSTRUMENT CATHODE-RAY TUBE

Oscilloscope tube with 7 cm diameter flat faceplate and post deflection acceleration by means of a helical electrode. The tube is intended for small service oscilloscopes.

| QUICK REFERENCE DATA | | | | | |
|-------------------------------|----------------|---|-------|------|--|
| Final accelerator voltage | Vg6(1) | = | 1200 | V | |
| Display area | | = | 4.5x6 | cm | |
| Deflection factor, horizontal | M _x | = | 10.7 | V/cm | |
| vertical | M _v | = | 3.65 | V/cm | |

SCREEN

| 1 | Colour | Persistence | | |
|--------|-----------------|--------------|--|--|
| DB7-78 | blue | medium short | | |
| DH7-78 | green | medium short | | |
| DN7-78 | bluish green | medium short | | |
| DP7-78 | yellowish green | long | | |

| Useful screen diameter | min. | 68 | mm | |
|--|------|----|----|--|
| Useful scan at $V_{g_6(\ell)}/V_{g_4}$ = 4 | | | | |
| horizontal | min. | 60 | mm | |
| vertical | min. | 45 | mm | |
| | | | | |

HEATING

Indirect by A.C. or D.C.; parallel supply

| Heater voltage | $\underline{V_{f}}$ | = | 6.3 | v |
|----------------|---------------------|------------|-----|----|
| Heater current | I_{f} | (* = ·) (| 300 | mA |

MECHANICAL DATA

Dimensions in mm



Mounting position: any

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

| Base | 14 pins | 14 pins all gla | | | |
|-------------------------------------|---------|-----------------|----|--|--|
| Dimensions and connections | | | | | |
| Overall length | max. | 296 | mm | | |
| Face diameter | max. | 77.8 | mm | | |
| Net weight | approx | . 370 | g | | |
| Accessories | | | | | |
| Socket (supplied with the tube) | type | 40467 | | | |
| Final accelerator contact connector | type | 55563 | | | |
| Mu-metal shield | type | 55532 | | | |
D.7-78

CAPACITANCES

| x_1 to all other elements except x_2 | $C_{x_1(x_2)}$ | 1 <u>–</u> 1919 | 3.5 | pF |
|--|-----------------------------------|--------------------|-----|----|
| x ₂ to all other elements except x ₁ | $C_{x_2(x_1)}$ | Ŧ | 3.5 | pF |
| y_1 to all other elements except y_2 | C _{y1} (y ₂) | = | 3.0 | pF |
| y_2 to all other elements except y_1 | C _{y2} (y1) | = | 3.0 | pF |
| x_1 to x_2 | $C_{x_1x_2}$ | (7 06) | 1.7 | pF |
| y ₁ to y ₂ | $C_{y_1y_2}$ | a≣jin | 1.6 | pF |
| Control grid to all other elements | C _{g1} | = / b | 3.5 | pF |
| Cathode to all other elements | C _k | = | 2.6 | pF |

FOCUSING electrostatic

| DEFLECTION | double electrostatic | | |
|------------|----------------------|--|--|
| x plates | symmetrical | | |
| y plates | symmetrical | | |

If use is made of the full deflection capabilities of the tube the deflection plates will intercept part of the electron beam; hence a low impedance deflection plate drive is desirable.

| Aligie between x and y traces 9 | U | + | • 1 | Ľ | ~ |
|---------------------------------|---|---|-----|---|---|
|---------------------------------|---|---|-----|---|---|

LINE WIDTH

Measured with the shrinking raster method in the centre of the screen.

| Final accelerator voltage | $V_{g_6(\ell)}$ | = | 1200 | V |
|---------------------------------------|-----------------|---|------|------------------|
| Astigmatism control electrode voltage | Vg4 | = | 300 | V ²) |
| First accelerator voltage | Vg ₂ | = | 1200 | v |
| Beam current | $I(\ell)$ | = | 10 | μA |
| Line width | l.w. | = | 0.65 | mm |
| | | | | |

HELIX

Post deflection accelerator helix resistance min. 40 $M\Omega$

2) See page 5

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D.7-78

TYPICAL OPERATING CONDITIONS

| Final accelerator voltage | $v_{g_6(\ell)}$ | = | 1 | 1200 | and the second | 4000 | V |
|--|------------------|-----|----------|------|----------------|--------|------------------|
| Geometry control electrode voltage | Vg5 | = | 300 ± | 30 | 1000 ± | 100 | V ¹) |
| Astigmatism control electrode voltage | Vga | = | 300 ± | 40 | 1000 <u>+</u> | 50 | v ²) |
| Focusing electrode voltage | Vg ₃ | = | 20 to 15 | 5015 | 35 to | 165 | V |
| First accelerator voltage | Vg2 | = | 1 | 200 | | 1000 | V |
| Control grid voltage for visual extinction of focused spot | -v _{g1} | п | 36 to | 72 | 30 to | 60 | V |
| Modulation voltage for $I(\ell) = 10 \ \mu A$ | V _{g1} | = | max. | 25 | max. | 25 | V |
| Deflection factor | 01 | | | | | | |
| horizontal | M _x | = | 9.4 to | 12 | 31.3 to | 40.0 | V/cm |
| vertical | My | = | 3.2 to | 4.1 | 10.7 to | 13.7 | V/cm |
| Deviation of linearity of deflection | | - | max. | 2 | max. | 2 | % ³) |
| Geometry distortion | | | See note | 4 | | | |
| Useful scan | | | | | | | |
| horizontal | | = | min. | 60 | | 60 | mm |
| vertical | | = | min. | 45 | | 45 | mm |
| CIRCUIT DESIGN VALUES | | | | | | | |
| Focusing voltage | Vg | - | 35 to | 165 | V per k | V of V | g4 |
| Control grid voltage for visual extinction of focused spot | -v _{g1} | - | 30 to | 60 | V per k | V of V | g ₂ |
| Deflection factor at $V_{g_6(l)}/V_{g_4}$ | = 4 | | | | | | |
| horizontal | M _x | - | 31.3 to | 40.0 | V/cm p | er kV | of V_{g_4} |
| vertical | My | = | 10.7 to | 13.7 | V/cm p | er kV | of V_{g_4} |
| Control grid circuit resistance | R _{g1} | 1 | max. | 1.5 | MΩ | | |
| Deflection plate circuit resistance | | | | | | | |
| | R_{x}, R_{y} | 7 = | max. | 50 | kΩ | | |

| D. | 7- | 78 |
|----|----|----|
|----|----|----|

LIMITING VALUES (Absolute max. rating system)

| Final accelerator voltage | $V_{g_{\ell}(n)}$ | = | max. 500 | 0 | V |
|---|--------------------------|---|----------|---|--------------------|
| | 80(1) | - | min. 120 | 0 | V |
| Geometry control electrode voltage | Vg5 | = | max. 220 | 0 | V |
| Astigmatism control electrode voltage | V | = | max. 210 | 0 | V |
| istigination control chectroac voltage | 'g4 | = | min. 30 | 0 | V . |
| Focusing electrode voltage | Vg3 | = | max. 100 | 0 | v |
| There are been been been been been been been be | 37 | = | max. 160 | 0 | V |
| First accelerator voltage | vg2 | = | min. 80 | 0 | V |
| Control grid voltage | | | | | |
| negative | -V _{g1} | = | max. 20 | 0 | V |
| positive | vg1 | = | max. | 0 | V |
| positive peak | V _{g1p} | = | max. | 2 | V |
| Cathode to heater voltage | | | | | |
| cathode positive | V _{+k/f} - | = | max. 20 | 0 | v |
| cathode negative | Vk/f+ | = | max. 12 | 5 | v |
| Voltage between astigmatism control | Vou/v | = | max. 50 | 0 | V |
| electrode and any deflection plate | $V_{g_A/V}^{B4/X}$ | = | max. 50 | 0 | V |
| Screen dissipation | Wl | = | max. | 3 | mW/cm ² |
| Ratio $V_g 6_{(\ell)} / V_g 4$ | $V_g 6_{(\ell)} / V_g 4$ | = | max. | 4 | |

- ¹) This tube is designed for optimum performance when operating at the ratio $V_{g_6(\ell)}/V_{g_4} = 4$. Operating at other ratio may result in changes in deflection uniformity and geometry distortion. The geometry control electrode voltage should be adjusted for optimum performance. For any necessary adjustment its potential will be within the stated range.
- ²) The astigmatism control electrode voltage should be adjusted for optimum spot shape. For any necessary adjustment its potential will be within the stated range.
- ³) The sensitivity at a deflection of less than 75% of the useful scan will not differ from the sensitivity at a deflection of 25% of the useful scan by more than the indicated value.
- ⁴) A graticule, consisting of concentric rectangles of 40.8 mm x 40.8 mm and 39.2 mm x 39.2 mm is aligned with the electrical x axis of the tube. The edges of a raster will fall between these rectangles with optimum correction potentials applied.
- 5) Values to be taken into account for the calculation of the focus potentiometer.

D.7-78



A

D.7-78



В



7Z2 7560

type 5911/20

D.10 - 6

6.3

300

Dimensions in mm

Vf

If

V

mA

INSTRUMENT CATHODE-RAY TUBE

SCREEN

| 1.2 - 1.5 | colour | persistence |
|-----------|-----------------|--------------|
| DB10-6 | blue | medium short |
| DG10-6 | yellowish green | medium |
| DP10-6 | yellowish green | long |

HEATING: Indirect by A.C. or D.C.; parallel supply

Heater voltage

Heater current

MECHANICAL DATA



Accessories

Socket

Base: Magnal

x1

y1

gЗ

g1

FOCUSING

| | 1 | ì | | į |
|---|---|----|---|---|
| | | | | |
| | 1 | 1 | ð | |
| 0 | ŝ | ī. | 2 | 1 |
| | | | | |
| | | | | |
| | | | | |

electrostatic

| DEFLECTION | double electrostatic |
|---------------|----------------------|
| x plates | symmetrical |
| y plates | symmetrical |
| Angle between | n x and y traces |

$90 + 1.5^{\circ}$

TYPICAL OPERATING CONDITIONS

| Final accelerator voltage | $v_{g_5(\ell)}$ | 4000 | V |
|--|------------------|------------|------|
| First accelerator voltage | Vg4,g2 | 2000 | V |
| Focusing electrode voltage | v_{g_3} | 400 to 720 | V |
| Control grid voltage for visual extinction of focused spot | -v _{g1} | 45 to 100 | v |
| Deflection factor, horizontal | M _x | 40 to 52.5 | V/cm |
| vertical | My | 32 to 40 | V/cm |

LIMITING VALUES

| Final | accelerator | voltage |
|-------|-------------|---------|
| First | accelerator | voltage |

| $v_{g_5(l)}$ | max. | 5000 | V |
|---------------|------|------|---|
| v_{g_4,g_2} | max. | 2500 | V |

INSTRUMENT CATHODE-RAY TUBE

SCREEN

| | colour | persistence |
|---------|-----------------|--------------|
| DB10-74 | blue | medium short |
| DG10-74 | yellowish green | medium |
| DP10-74 | yellowish green | long |

HEATING: Indirect by A.C. or D.C.; parallel supply

Heater voltage

Heater current

MECHANICAL DATA



max 341

320±

6.3 V

300

mA

Vf

I_f

Base: Magnal

x1

y1.





Accessories

Socket

type 5911/20

7Z2 7562

OBSOLESCENT TYPE

| FOCUSING | electrostatic |
|-----------------|---------------------------------|
| DEFLECTION | double electrostatic |
| x plates | symmetrical |
| y plates | symmetrical |
| Angle between x | and y traces $90 + 1.5^{\circ}$ |
| | |

TYPICAL OPERATING CONDITIONS

| Final accelerator voltage | $v_{g_5(l)}$ | 4 | 1000 | V |
|--|----------------|---------|------|------|
| First accelerator voltage | Vg4,g2 | 2 | 2000 | V |
| Focusing electrode voltage | Vg3 | 400 to | 720 | V |
| Control grid voltage for visual extinction of focused spot | -Vg1 | 45 to | 100 | v . |
| Deflection factor, horizontal | M _X | 40 to 5 | 52.5 | V/cm |
| vertical | My | 32 to | 40 | V/cm |

LIMITING VALUES

| Final accelerator voltage | $v_{g_5(\ell)}$ | max. | 5000 | V |
|---------------------------|-----------------|------|------|---|
| First accelerator voltage | Vg2, g4 | max. | 2500 | V |

INSTRUMENT CATHODE-RAY TUBE

General purpose cathode-ray tube with flat face and post deflection acceleration by means of a helical electrode.

| QUICK REFERENCE DATA | | | | |
|-------------------------------|----------------|-----|-------|------|
| Final accelerator voltage | Vg(l) |) = | 4 | kV |
| Display area | | = | 55x75 | cm |
| Deflection factor, horizontal | M _X | = | 34 | V/cm |
| vertical | M _v | = | 11 | V/cm |

SCREEN

| | | Colour | Persistence |
|---|---------|-----------------|--------------|
| 1 | DB10-78 | blue | medium short |
| | DH10-78 | green | medium short |
| | DN10-78 | bluish green | medium short |
| | DP10-78 | yellowish green | long |

Useful scan diameter min. 90 mm Useful scan at $V_{g_6(\ell)}/V_{g_4,g_2} = 4$ horizontal min. 75 mm vertical min. 55 mm

HEATING

| Indirect by A.C. or D.C.; | parallel supply | | | | |
|---------------------------|-----------------|---------------------|---|-----|----|
| | Heater voltage | $\underline{V_{f}}$ | = | 6.3 | V |
| | Heater current | Ι _f | = | 300 | mA |

7Z2 5644

MAINTENANCE TYPE



Mounting position: any

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

| Diheptal 12 pin | | S | |
|-----------------|---|---|--|
| | | | |
| ax. | 305 | mm | |
| ax. | 102 | mm | |
| oprox. | 660 | g | |
| | | | |
| pe 5 | 914/2 | 20 | |
| pe 5 | 5560 | | |
| pe 5 | 5541 | | |
| | heptal ax. ax. prox. pe 5 pe 5 pe 5 | heptal 12 pm ax. 305 ax. 102 pprox. 660 pe 5914/2 pe 55560 pe 55541 | |

CAPACITANCES

| x_1 to all other elements except x_2 | $C_{x_1(x_2)}$ | = | 4 | pF |
|--|-----------------|---|-----|----|
| x_2 to all other elements except x_1 | $C_{x_2(x_1)}$ | = | 4 | pF |
| y_1 to all other elements except y_2 | $C_{y_1(y_2)}$ | = | 3.5 | pF |
| y_2 to all other elements except y_1 | $C_{y_2(y_1)}$ | = | 3.5 | pF |
| x_1 to x_2 | $C_{x_1x_2}$ | = | 2.1 | pF |
| y_1 to y_2 | Cy1y2 | = | 1.7 | pF |
| Control grid to all other elements | Cg ₁ | = | 5.0 | pF |
| Cathode to all other elements | Ck | = | 3.4 | pF |

FOCUSING

electrostatic

| DEF | LECTION | |
|-----|---------|--|
| X | plates | |

y plates

double electrostatic symmetrical symmetrical

Is use is made of the full deflection capabilities of the tube the deflection plates will intercept part of the electron beam; hence a low impedance deflection plate drive is desirable.

 $90 + 1^{0}$

Angle between x and y traces

LINE WIDTH

Measured with the shrinking raster method in the centre of the screen.

| Final accelerator voltage | $V_{g_6(l)}$ | 1 = 1 | 4000 | V |
|---------------------------------------|--------------|-------|------|------------------|
| Astigmatism control electrode voltage | Vg4,g2 | = | 1000 | V ²) |
| Beam current | I(() | Ξ | 10 | μΑ |
| Line width | 1.w. | = | 0.35 | mm |
| | | | | |

HELIX

Post deflection accelerator helix resistance min. 50 $M\Omega$

2) See page 5

| TYPICAL OPERATING CONDITIONS | | | | | | |
|--|----------------------------------|------------------|--------------|--------------|--------|-------------------|
| Final accelerator voltage | Vg ₆ (|) = | e pal an D | 40 | 000 | V |
| Geometry control electrode voltage | V _g | 19. 8 | 1000 |) + | 100 | V ¹) |
| Astigmatism control electrode voltag | e V _{g4,g} | 2 | = 1000 |) ± | 50 | V ²) |
| Focusing electrode voltage | V _{g3} | - | = 150 |)to 3 | 350 | V |
| Control grid voltage for visual extinction of focused spot | t -V _{g1} | = | = 22.5 | 5 to 3' | 7.5 | V |
| Deflection factor | | | | | | |
| horizontal | M _X | - A- | - 29 |) to | 39 | V/cm |
| vertical | My | ទុកាភ្ | 9.4 | 1 to 12 | 2.6 | V/cm |
| Deviation of linearity of deflection | | - | max | 1. | 2 | % ³) |
| Geometry distortion | | = | See | note 4 | 1 | |
| Useful scan | | | | | | |
| horizontal | | - | min | · //() | 75 | mm |
| vertical | | 7 | min | • | 55 | mm |
| LIMITING VALUES (Absolute max. 1 | ating system) | | | | | |
| Final accelerator voltage | $V_{g_6(\ell)}$ | = | max. min. | 8000 1500 | V V | |
| Geometry control electrode voltage | Vg5 | = | max. | 2200 | V | |
| Astigmatism control electrode voltage | V _{g4} , g ₂ | = | max. min. | 2100 1000 | V V | |
| Focusing electrode voltage | Vg3 | = | max. | 1500 | V | |
| Control grid voltage, | | | | | | |
| negative | $-V_{g_1}$ | = | max. | 200 | V | |
| positive | V _{g1} | = | max. | 0 | V | |
| positive peak | Vgln | = | max. | 2 | V | |
| Cathode to heater voltage, | тр | | | | | |
| cathode positive | $V_{+k/f}$ - | = | max. | 200 | V | |
| cathode negative | V-k/f+ | = | max. | 125 | V | |
| Voltage between astigmatism control electrode | Vg4,g2/x | 190. = 0. | max. | 500 | v | |
| and any deflection plate | Vg4,g2/y | = | max. | 500 | V | |
| Screen dissipation | W | = | max. | 3 | m | W/cm ² |
| Ratio $V_{g_6(l)}V_{g_4,g_2}$ | $V_{g_6(l)}/V_{g_4,g_2}$ | = | max. | 4 | | |

7Z2 5647

| CIRCUIT DESIGN VALUES | | | | |
|--|---------------------------------|---|--------------|--|
| Focusing voltage | Vg3 | = | 150 to 350 | V per kV of V _{g4} , g ₂ |
| Control grid voltage for visual extinction of focused spot | -v _{g1} | = | 22.5 to 37.5 | V per kV of V _{g4} , g ₂ |
| Deflection factor at | | | | |
| $V_{g_6(l)}/V_{g_4,g_2} = 4$ | | | | |
| horizontal | $M_{\rm X}$ | = | 29 to 39 | V/cm per kV of Vg4,g2 |
| vertical | My | = | 9.4 to 12.6 | V/cm per kV of V_{g_4}, g_2 |
| Control grid circuit | | | | |
| resistance | Rg1 | = | max. 1.5 | MΩ |
| Deflection plate circuit resistance | R _x , R _y | = | max. 1 | MΩ |
| Focusing electrode | | | | |
| current | Ig | = | +15 to -30 | μA ⁵) |

- 1) This tube is designed for optimum performance when operating at the ratio $Vg_6(\ell)/Vg_4, g_2 = 4$. Operation at other ratio may result in changes in deflection uniformity and geometry distortion. The geometry control electrode voltage should be adjusted for optimum performance. For any necessary adjustment its potential will be within the stated range.
- 2) The astigmatism control electrode voltage should be adjusted for optimum spot shape. For any necessary adjustment its potential will be within the stated range.
- 3) The sensitivity at a deflection of less than 75% of the useful scan will not differ from the sensitivity at a deflection of 25% of the useful scan by more than the indicated value.
- ⁴) A graticule, consisting of concentric rectangles of 51 mm x 51 mm and 49 mm x 49 mm is aligned with the electrical x axis of the tube. The edges of a raster will fall between these rectangles with optimum correction potentials applied.
- ⁵) Values to be taken into account for the calculation of the focus potentiometer. 7Z2 5648



INSTRUMENT CATHODE-RAY TUBE

The DG13-2 is a 13 cm spherical faced cathode ray tube primarily intended for inexpensive service oscilloscopes.

| QUICK REFERENCE DATA | | | | |
|-------------------------------|---------------------------|--|--|--|
| Final accelerator voltage | $V_{g_5}(l)$ 4 kV | | | |
| Display area | Both directions full scan | | | |
| Deflection factor, horizontal | M _X 31 V/cm | | | |
| vertical | M _y 26.5 V/cm | | | |

SCREEN

| | colour | persistence |
|---------|-----------------|--------------|
| DB 13-2 | blue | medium short |
| DG13-2 | yellowish green | medium |
| DP 13-2 | yellowish green | long |

Useful screen diameter Useful scan, horizontal vertical min. 114 mm full scan full scan

HEATING

Indirect by A.C. or D.C.; parallel supply

| leater voltage | V_{f} | 6.3 V | | |
|----------------|---------|---------|-----|----|
| Heater | current | I_{f} | 300 | mA |

| MAINIENANCE | TY | PE |
|-------------|----|----|
|-------------|----|----|

MECHANICAL DATA

Dimensions in mm



Mounting position: any

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

| e Dihepta | | al |
|-------------------------------------|------|---------|
| Dimensions and connections | | |
| Overall length | max. | 435 mm |
| Face diameter | max. | 135 mm |
| Accessories | | |
| Socket | type | 5914/20 |
| Final accelerator contact connector | type | 55560 |
| Mu-metal shield | type | 55550 |

| | C | 0.13-2 | |
|--|-----------------------------------|---------------|--|
| CAPACITANCES | torracio oralisa | n a principal | |
| \mathbf{x}_1 to all other elements except \mathbf{x}_2 | $C_{x_1(x_2)}$ | 5.5 pF | |
| \mathbf{x}_2 to all other elements except \mathbf{x}_1 | $C_{x_2(x_1)}$ | 5.5 pF | |
| y_1 to all other elements except y_2 | C _{y1} (y ₂) | 4.7 pF | |
| y_2 to all other elements except y_1 | C _{y2} (y ₁) | 4.7 pF | |
| x_1 to x_2 | $C_{x_1x_2}$ | 2.5 pF | |
| y_1 to y_2 | Cy ₁ y ₂ | 1.9 pF | |
| Control grid to all other elements | c_{g_1} | 4.6 pF | |
| Cathode to all other elements | Ck | 6.0 pF | |

FOCUSING

electrostatic

| DEFLECTION | double electrostatic | |
|-----------------|--------------------------|--|
| x plates | symmetrical | |
| y plates | symmetrical | |
| Angle between x | and y traces 90 ± 10 | |

LINE WIDTH

| $V_{g5}(l)$ | | 4000 | V |
|-------------|--|---|---|
| Vg4,g2 | | 2000 | V |
| I(l) | 6 | 0.5 | μΑ |
| 1.w. | | 0.3 | mm |
| | $V_{g5}(\ell)$ V_{g4}, g_2 I(ℓ) 1.w. | $V_{g_5}(\ell)$ V_{g_4,g_2} I(ℓ) 1.w. | $V_{g5}(\ell)$ 4000 V_{g4}, g_2 2000 $I(\ell)$ 0.51.w.0.3 |

| TYPICAL OPERATING CONDITIONS | | | | |
|--|-----------------|-----------------|---------|--------------------|
| Final accelerator voltage | Vg5 | (l) | 4000 | V |
| First accelerator voltage | Vg4 | ,g ₂ | 2000 | V |
| Focusing electrode voltage | Vg3 | 400 | to 720 | V |
| Control grid voltage for visual extinction of focused spot | -Vg1 | 45 | to 100 | V |
| Deflection factor, horizontal | M _x | 27 | to 35 | V/cm |
| vertical | My | 24 | to 29 | V/cm |
| Useful scan, horizontal | | ful | ll scan | |
| vertical | | ful | ll scan | |
| LIMITING VALUES | | | | |
| Final accelerator voltage | $V_{g_5}(l)$ | max. | 5000 | V |
| Final accelerator voltage | V_{g_4,g_2} | max. | 2500 | V |
| Focusing electrode voltage | Vg ₃ | max. | 1000 | V |
| Control grid voltage, | - Saint | | | |
| negative | -Vg1 | max. | 200 | V |
| positive | Vg1 | max. | 0 | V |
| positive peak | Vglp | max. | 2 | V |
| Cathode to heater voltage, | Р | | | |
| cathode positive | $V_{+k/f}$ - | max. | 200 | V |
| cathode negative | V-k/f+ | max. | 125 | V |
| Voltage between accelerator and any deflection plate | Vg4/x | max. | 500 | V |
| | Vg4/y | max. | 500 | V |
| Screen dissipation | Wo | max. | 3 | mW/cm ² |

INSTRUMENT CATHODE-RAY TUBE

13 cm diameter oscilloscope tube for inexpensive oscilloscopes.

| QUICK REFERENC | E DATA | - | |
|-------------------------------|-------------------|----------|---------|
| Final accelerator voltage | $V_{g_4, g_2(l)}$ | 2 | kV |
| Display area | Both direc | tions fu | ll scan |
| Deflection factor, horizontal | M _X | 26 | V/cm |
| vertical | My | 21 | V/cm |

SCREEN

| | colour | persistence |
|---------|-----------------|-------------|
| DG13-32 | yellowish green | medium |

Useful screen diameter

min.

114 mm

Useful scan

horizontal vertical full scan full scan

HEATING

Indirect by A.C. or D.C.; parallel supply

| Heater | voltage |
|--------|---------|
| Heater | current |

 $\frac{V_f}{I_f} \frac{6.3}{600} \frac{V}{mA}$

7Z2 5995

1.1.1966

MAINTENANCE TYPE

MECHANICAL DATA

Dimensions in mm



Mounting position: any

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

| Duodeca | al 12 p | |
|---------|--|--|
| | | |
| max. | 384.5 | mm |
| max. | 135.4 | mm |
| approx. | 790 | g |
| | | |
| type | 5912/20 | |
| type | 55560 | |
| type | 55550 | |
| | Duodeca max. max. approx. type type type | Duodecal 12 p max. 384.5 max. 135.4 approx. 790 type 5912/20 type 55560 type 55550 |

| | | | D.1. | 3-32 |
|---|----------------------------|-------------------------|------------------|---------|
| CAPACITANCES | | | 34,867,196 | UMLI |
| \mathbf{x}_1 to all other elem | ents except x ₂ | C _{x1} (x | 2) 9. | 3 pF |
| \mathbf{x}_2 to all other elem | ents except x ₁ | $C_{x_2(x)}$ | $\frac{1}{1}$ 5. | 0 pF |
| y_1 to all other elem | ents except y ₂ | C _{y1(y} | (2) 4. | 6 pF |
| y_2 to all other elem | ents except y ₁ | C _{v2(v} | (1) 4. | 6 pF |
| x_1 to x_2 | | $C_{x_1x_2}$ | 2. | 0 pF |
| y_1 to y_2 | | C _{y1y} | - , 1. | 5 pF |
| Control grid to all o | other elements | C _{g1} | 4. | 3 pF |
| Cathode to all other | elements | C _k | 6 | 5 pF |
| | | | | |
| FOCUSING | electrostatic | | | |
| DEFLECTION | double electrostatic | | | |
| x plates | symmetrical | | | |
| y plates | symmetrical | | | |
| Angle between | x and y traces 90 | <u>+</u> 1° , | | |
| LINE WIDTH | | | | |
| Measured on a circ | le of 50 mm diameter. | | | |
| Accelerator voltage | | $V_{g_A, g_2}(l)$ | 2000 | v |
| Beam current | | I(1) | 0.5 | μA |
| Line width | | 1.w. | 0.4 | mm |
| | | | | |
| TYPICAL OPERATI | NG CONDITIONS | | | |
| Accelerator voltage | | $v_{g_{4},g_{2}(\ell)}$ | 2000 | V |
| Focusing electrode | voltage | Vg3 | 340 to 640 | V |
| Control grid voltage of focused spot | e for visual extinction | -V _{g1} | max. 90 | v |
| Deflection factor, h | norizontal | M _x | 22 to 30 | V/cm |
| V | vertical | M _y 1 | 8.2 to 24.2 | V/cm |
| Useful scan, horizo | ontal | | full scan | |
| vertic | al | | full scan 7 | Z2 5997 |

-

| LIMITING VALUES | | | | | |
|---------------------------------|-----------------|--------------------|---------------------|---------|-------------------------------------|
| Final accelerator voltage | | $V_{g_4, g_2}(l)$ | max. | 2500 | V |
| Focusing electrode voltage | | V _{g3} | max. | 1000 | V |
| Control grid voltage, | | and the second | | | |
| negative | | -V _{g1} | max. | 200 | V |
| positive | | V _{g1} | max. | 0 | V |
| positive peak | | Vglp | max. | 2 | V |
| Cathode to heater voltage, | | Р | | | |
| cathode positive | | $V_{+k/f}$ - | max. | 200 | V |
| cathode negative | | V _{-k/f+} | max. | 125 | V |
| Voltage between | | theres as | | | |
| and any deflection plate | | Vg4/x | max. | 500 | V |
| | | Vg4/y | max. | 500 | V |
| Screen dissipation | | We | max. | 3 | mW/cm^2 |
| | | | | | |
| CIRCUIT DESIGN VALUES | | | | | |
| Focusing voltage | v_{g_3} | 170 to 32 | 0 V per | kV of V | g. |
| Control grid voltage for | | | | | |
| visual extinction of focused | $-V_{\alpha}$ | max. 4 | 5 V per | kV of V | a go |
| Deflection factor | 81 | | | | 54,52 |
| horizontal | M _x | ll to l | 5 V/cm | per kV | of Vg ₄ , g ₂ |
| vertical | M _V | 9.1 to 12. | 1 V/cm | per kV | of V_{g_4, g_2} |
| Control grid circuit resistance | R _{g1} | max. 1. | 5 ΜΩ | | |
| Deflection plate circuit | | | | | |
| resistance | R_{x}, R_{y} | max. | 5 MΩ | | |
| Focusing electrode current | Ig3 | -15 to +1 | 5 μA ¹) | | |

 $^{\rm l}$) Values to be taken into account for the calculation of the focus potentiometer. $$722\ 5998$$

INSTRUMENT CATHODE-RAY TUBE

13 cm diameter flat faced oscilloscope tube for general purpose oscilloscopes.

| QUICK REFERENCE DATA | | | | |
|-------------------------------|-----------------|-------------|------|--|
| Final accelerator voltage | $V_{g_5}(\ell)$ | 4 | kV | |
| Display area | | 10.2 x 10.2 | cm | |
| Deflection factor, horizontal | M _X | 23.7 | V/cm | |
| vertical | My | 17.7 | V/cm | |

SCREEN

| | colour | persistence |
|----------|-----------------|--------------|
| DB 13-34 | blue | medium short |
| DG13-34 | yellowish green | medium short |
| DP 13-34 | yellowish green | long |

| Useful screen diameter | min. | 114 | mm | |
|--|------|-----|----|--|
| Useful scan at $V_{g_5}(\ell)/V_{g_4,g_2} = 2$ | | | | |
| horizontal | min. | 102 | mm | |
| vertical | min. | 102 | mm | |

HEATING

Indirect by A.C. or D.C.; parallel supply

| Heater voltage | v_{f} | 6.3 | V |
|----------------|--------------------|-----|----|
| Heater current | $\overline{I_{f}}$ | 600 | mA |

7Z2 5999

MAINTENANCE TYPE



Mounting position: any

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

| Base | Diheptal 12 p | |
|---|------------------|-----------|
| Dimensions and connections | , รู้เหน่งไร่เหง | |
| Overall length | max. 430 i | nm on and |
| Face diameter | max. 134.5 n | nm |
| Net weight | approx. 1100 g | ç |
| Accessories | o rehail | |
| Socket | type 5914/20 | |
| Final accelerator contact connector | type 55560 | |
| Mu-metal shield | type 55550 | |
| ¹) Lower side of straight part. | | 7Z2 6000 |
| | | |

| CAPACITANCES | | |
|--|-------------------------------------|----|
| x_1 to all other elements except x_2 | $C_{x_1(x_2)}$ 4 | pF |
| \mathbf{x}_2 to all other elements except \mathbf{x}_1 | $C_{x_2(x_1)}$ 4 | pF |
| y_1 to all other elements except y_2 | Cy ₁ (y ₂) 4 | pF |
| y_2 to all other elements except y_1 | C _{y2} (y ₁) 4 | pF |
| \mathbf{x}_1 to \mathbf{x}_2 | C _{x1x2} 2.5 | pF |
| y_1 to y_2 | C _{y1y2} 1.1 | pF |
| Control grid to all other elements | С _{g1} 5 | pF |
| Cathode to all other elements | C _k 4 | pF |
| | | |

FOCUSING

electrostatic

| DEFLECTION | double electrostatic | |
|------------|----------------------|--|
| x plates | symmetrical | |
| y plates | symmetrical | |

If use is made of the full deflection capabilities of the tube the deflection plates will intercept part of the electron beam; hence a low impedance deflection plate drive is desirable.

| Angel between x and y traces | 90 + 1 | 0 |
|------------------------------|--------|---|
|------------------------------|--------|---|

LINE WIDTH

Measured on a circle of 50 mm diameter.

| Final accelerator voltage | $v_{g_5(l)}$ | 4000 | V |
|---------------------------|--------------------|------|----|
| First accelerator voltage | V _{g4,g2} | 2000 | V |
| Beam current | I(l) | 0.5 | μA |
| Line width | l.w. | 0.3 | mm |

| TYPICAL OPERATING CONDITIONS | | | |
|--|----------------|--------------|------------------|
| Final accelerator voltage | $V_{g_5}(l)$ | 4000 | V |
| First accelerator voltage | Vg4,g2 | 2000 | V |
| Focusing electrode voltage | Vg3 | 400 to 690 | V |
| Control grid voltage for visual extinction of focused spot | -Vg1 | · 45 to 75 | V |
| Deflection factor, horizontal | M _X | 21.2 to 26.2 | V/cm |
| vertical | My | 15.8 to 19.6 | V/cm |
| Deviation of linearity of deflection | max. | 2 | % ¹) |
| Geometry distortion | | see note 2 | |
| Useful scan, horizontal | min. | 102 | mm |
| vertical | min. | 102 | mm |
| | | | |

LIMITING VALUES

| Final accelerator voltage | $v_{g_5(\ell)}$ | max. min. | 1000 | V V |
|--------------------------------|--------------------------|--------------|------|-------------------|
| First accelerator voltage | Vg4,g2 | max. | 2600 | V |
| Focusing electrode voltage | Vg3 | max. | 1000 | V |
| Control grid voltage, | | min. | 1000 | V |
| negative | $-v_{g_1}$ | max. | 200 | V |
| positive | vg1 | max. | 0 | V |
| positive peak | $v_{g_{1_D}}$ | max. | 2 | V |
| Cathode to heater voltage, | F | | | |
| cathode positive | V+k/f- | max. | 200 | v |
| cathode negative | V _{-k/f+} | max. | 125 | v |
| Voltage between | | | | |
| and any deflection plate | Vg4/x | max. | 500 | V |
| | Vg4/y | max. | 500 | V |
| Cathode current | Ikeff | max. | | mA |
| Screen dissipation | Wl | max. | 3 | W/cm ² |
| Ratio $V_{g_5}(l)/V_{g_4,g_2}$ | $v_{g_5}(l)/v_{g_4,g_2}$ | max. | 2.3 | |

| CIRCUIT DESIGN VALUES | | | | |
|--|-----------------------------------|---------|------|-------------------------------|
| Focusing voltage | v_{g_3} | 200 to | 345 | V per kV of V_{g_4, g_2} |
| Control grid voltage for visual extinction of focused spot | -v _{g1} | 22.5 to | 37.5 | V per kV of V_{g_4,g_2} |
| Deflection factor at $V_{g_5}(l)/V_{g_4}$ | = 2 | | | |
| horizontal | M _X | 10.6 to | 13.1 | V/cm per kV of V_{g_4,g_2} |
| vertical | My | 7.9 to | 9.8 | V/cm per kV of V_{g_4, g_2} |
| Control grid circuit resistance | Mg1 | max. | 1.5 | ΜΩ ' |
| Deflection plate circuit resistar | nceR _x ,R _y | max. | 1 | MΩ |
| Focusing electrode current | Ig3 | -15 to | +15 | μA ³) |

¹) The sensitivity at a deflection of less than 75% of the useful scan will not differ from the sensitivity at a deflection of 25% of the useful scan by more than the indicated value.

²) A graticule, consisting of concentric rectangles of 81.6 mm x 81.6 mm and 78.4 mm x 78.4 mm is aligned with the electrical x axis of the tube. The edges of a raster will fall between these rectangles with optimum correction potentials applied.

³) Values to be taken into account for the calculation of the focus potentiometer. 7Z2 6003



10 cm diameter flat faced double gun oscilloscope tube, post-deflection acceleration by means of a helical electrode and low interaction between traces. The tube features beam-blanking.

| QUICK REFERENCE DATA | | | |
|-------------------------------|---------------------------|---------------|------|
| Final accelerator voltage | Vg9(1) | 3000 | V |
| Display area | horizontal fu vertical | ull scan 7 | cm |
| Deflection factor, horizontal | M _X | 15 | V/cm |
| vertical | My | 7 | V/cm |

SCREEN

| | | Concession of the second se |
|----------|-----------------|---|
| | colour | persistence |
| E10-12BE | blue | medium short |
| E10-12GH | green | medium short |
| E10-12GM | yellowish green | long |
| E10-12GP | bluish green | medium short |

Useful screen diameter

Useful scan (each gun) at $V_{g_9}(\ell)/V_{g_5} = 3$ horizontal

norizontal

full scan min. 70 mm

min.

85 mm

vertical

The useful scan may vertically be shifted to a max. of 5 mm with respect to the geometric centre of the face plate.

HEATING

Indirect by A.C. or D.C.; parallel supply

Heater voltage

each gun

 $\begin{array}{ccc} V_{f} & 6.3 & V \\ \hline I_{f} & 300 & mA \\ & & 7Z2 & 6180 \end{array}$

Heater current

11.11.1966

TENTATIVE DATA



Mounting position: any

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

| Base | 14 pin all glass | | SS |
|-------------------------------------|------------------|-------|----|
| Dimensions and connections | | | |
| Overall length | max. | 410 | mm |
| Face diameter | max. | 102 | mm |
| Net weight | approx | . 800 | g |
| Accessories | | | |
| Socket, supplied with tube | type | 55566 | |
| Final accelerator contact connector | type | 55563 | |
| Side contact connector | type | 55561 | |
| Mu-metal shield ⁸) | type | 55545 | |

⁸) See page 6.

CAPACITANCES (each gun) x_1 to all other elements except x_2 $C_{x_1(x_2)}$ 3 pF 4.5 pF x_2 to all other elements except x_1 $C_{x_2(x_1)}$ $C_{y_1(y_2)}$ 3.5 pF y_1 to all other elements except y_2 y_2 to all other elements except y_1 $C_{y_2(y_1)}$ 3.5 pF $C_{x_1x_2}$ x_1 to x_2 2 pF $C_{y_1y_2}$ 1.5 pF y_1 to y_2 Grid No.1 to all other elements Cg1 pF 6 Cathode to all other elements Ck 5 pF

FOCUSING

electrostatic

| DE | FLECTION | double electrostatic | |
|----|-----------------------|--------------------------|------------------|
| | x plates | symmetrical | |
| | y plates | symmetrical | |
| | Angle between x and y | traces | 90 ± 10 |
| | Corresponding traces | of each gun align within | 1.5 ⁰ |

If use is made of the full deflection capabilities of the tube the deflection plates will intercept part of the electron beam; hence a low impedance deflection plate drive is desirable.

LINE WIDTH

Measured with the shrinking raster method in the centre of the screen.

| Final accelerator voltage | Vg9(1) | 3000 | V |
|---------------------------------------|-----------------|------|------------------|
| Astigmatism control electrode voltage | Vg5 | 1000 | v ³) |
| First accelerator voltage | vg2 | 1000 | V |
| Beam current | Ig9 (() | 10 | μA |
| Line width | 1.w. | 0.50 | mm |

HELIX

Post deflection accelerator helix resistance: min. $100 M\Omega$

³) See page 6.

7Z2 7810

E10-12...

| TYPICAL | OPERATING | CONDITIONS(| each | gun) |
|---------|------------------|-------------|------|------|
|---------|------------------|-------------|------|------|

| Final accelerator voltage | $V_{g_9}(\ell)$ | 3000 | V |
|--|------------------|-------------------|-----------------------|
| Intergun shield voltage | Vg8 | 1000 <u>+</u> 100 | V ¹) |
| Geometry control electrode voltage | Vg7 | 1000 <u>+</u> 100 | V ¹) |
| Deflection plate shield voltage | Vg6 | 1000 | V ²) |
| Astigmatism control electrode voltage | Vg5 | 1000 <u>+</u> 100 | V ³) |
| Focusing electrode voltage | Vg4 | 180 to 380 | V |
| Deflection blanking electrode voltage | Vg3 | 1000 | V |
| Deflection blanking control voltage for beam blanking of a current $I_{g_9}(\ell) = 10 \ \mu A$ | ΔV_{g_3} | max. 40 | V |
| First accelerator voltage | Vg2 | 1000 | V |
| Control grid voltage for visual extinction of focused spot | Vg1 | -25 to -90 | V |
| Deflection factor, horizontal | M _X | 10 to 20 | V/cm |
| vertical | My | 6 to 8 | V/cm |
| Deviation of linearity of deflection | | max. 2.5 | % ⁴) |
| Geometry distortion | | See note 5 | |
| Interaction factor | | 2.10-3 | mm/Vdc ⁶) |
| Tracking error | | 1.5 | mm ⁷) |

1)2)3)4)5)6)7) See page 6

| Final accelerator voltage | Vg9(l) | max. min. | 3300 2700 | V V |
|---------------------------------------|-------------------------|--------------|--------------|-----------|
| Intergun shield voltage | Vg8 | max. | 1200 | V |
| Geometry control electrode voltage | Vg7 | max. | 1200 | V |
| Deflection plate shield voltage | Vg6 | max. | 1200 | V |
| Astigmatism control electrode voltage | Vg5 | max. min. | 1200 800 | V V |
| Focusing electrode voltage | Vg4 | max. | 1200 | V |
| Beam blanking electrode voltage | Vg3 | max. | 1200 | V |
| First accelerator voltage | v _{g2} | max. min. | 1200 200 | V V |
| Control grid voltage, | | | | |
| negative | -Vg1 | max. | 200 | v |
| positive | Vg1 | max. | 0 | V |
| positive peak | Vglp | max. | 2 | V |
| Cathode to heater voltage, | | | | |
| cathode positive | V+k/f- | max. | 200 | V |
| cathode negative | V-k/f+ | max. | 125 | V |
| Average cathode current | Ik | max. | 300 | μA |
| Screen dissipation | Wé | max. | 3 | mW/cm^2 |
| Ratio $V_{g_9}(\ell)/V_{g_5}$ | $V_{g_9}(\ell)/V_{g_5}$ | max. | 3 | |

LIMITING VALUES (each gun, if applicable) (Absolute max. rating system)

CIRCUIT DESIGN VALUES (each gun, if applicable)

| Focusing voltage | V | 180 to 380 | V/kV of V _{g2} |
|--|----|--------------|--|
| Control grid voltage for visual cut-off focused spot | v | 31 25 to −90 | V/kV of Vg2 |
| Deflection factor $V_{g_9}(l)/V_{g_5} = 3$ | | | |
| horizontal | М | x 10 to 20 |) V/cm per kV of V_{g_5} |
| vertical | М | y 6 to 8 | $V/cm \text{ per } kV \text{ of } V_{g_5}$ |
| Focusing electrode current | Ig | -15 to $+10$ |) μA |
| Control grid circuit resistance | R | max. 1.5 | 5 ΜΩ |

- ¹) This tube is designed for optimum performance when operating at the ratio $V_{g9}(\ell)/V_{g5} = 3$. Operation at other ratio may result in changes in deflection uniformity and geometry distortion. The geometry control electrode voltage and the intergunshield voltage should be adjusted for optimum performance. For any necessary adjustment its potential will be within the stated range.
- ²) This voltage should be equal to the mean x and y plates potential.
- 3) The astigmatism control electrode voltage should be adjusted for optimum spot shape. For any necessary adjustment its potential will be within the stated range.
- ⁴) The sensitivity at a deflection of less than 75% of the useful scan will not differ from the sensitivity at a deflection of 25% of the useful scan by more than the indicated value.
- 5) A graticule consisting of concentric rectangles of 60 mm x 60 mm and 57 mm x 57 mm is aligned with electrical x axis of the tube. The edges of a raster will fall between these rectangles with optimum potentials applied.
- ⁶) The deflection of one beam when balanced dc voltage are applied to the deflection plates of the other beam, will not be greater than the indícated value.
- ⁷) With 50 mm vertical traces superimposed at the tube face centre and deflected horizontally ± 4 cm by voltages proportional to the relative deflection factors, horizontal separation of the corresponding points of the traces shall not be greater than the indicated value.
- ⁸) Due to the maximum length of side contacts the inner diameter of the mumetal shield at the smaller end is advised not to be less than 100 mm.
M21-11W

MONITOR TUBE

21 cm rectangular television tube with metal-backed screen primarily intended for use as a precision monitor.

| QUICK REFERE | ENCE DATA |
|------------------|----------------|
| Deflection angle | 90 o |
| Focusing | electrostatic |
| Resolution | min. 650 lines |
| Overall length | max. 222 mm |

SCREEN

Metal backed phosphor

| the second s | |
|--|-------------|
| Lumenescence | white |
| Useful diagonal | min. 195 mm |
| Useful width | min. 180 mm |
| Useful height | min. 135 mm |

HEATING

| Indirect by A.C. or D.C.; | parallel supply | | | | |
|---------------------------|-----------------|------------------|---|----|---------------|
| | heater voltage | \underline{Vf} | = | 11 | $V \pm 10 \%$ |
| | heater current | I_{f} | = | 70 | mA |

CAPACITANCES

| Final accelerator to external | | | | |
|---------------------------------|------------|-----|----------|----|
| conductive coating | Cg3,g5(1)/ | m = | max. 375 | pF |
| Cathode to all other elements | Ck | = | 5.0 | pF |
| Grid No.1 to all other elements | Cg1 | = | 9.0 | pF |

M21-11W

MECHANICAL DATA

Dimensions in mm



Mounting position: any

Except vertical with the screen downward and the axis of the tube making an angle of less than 20 $^{\rm O}$ with the vertical. 7Z2 7813

M21_11W

Dimensions in mm

MECHANICAL DATA (continued)

Base:

Cavity contact

CT8

Neo Eightar (B8H)

Accessories

Final accelerator connector

type 55563

FOCUSING electrostatic

The range of focus voltage shown under "Typical operating conditions" results in optimum focus at a beam current of 100 μ A.

DEFLECTION magnetic

Diagonal deflection angle 90⁰

REFERENCE LINE GAUGE

96.8±0.4 88.9±0.4 82.5±0.1 R=1.0±0.4 53.9 ± 0.05 30.75 ±0.07 14.3±0.1 6.4±0.4 90 Reference line R=127±04 R=127±01 778+ 15.57±0.10 16.9±0.1 29.67+007 7201932. 43±04

TYPICAL OPERATING CONDITIONS

| Final accelerator voltage | $V_{g_3,g_5}(l)$ | = | 12 | kV |
|---|------------------|---|----------|----|
| Focusing electrode voltage | v _{g4} | = | 0 to 400 | V |
| First accelerator voltage | vg2 | = | 400 | V |
| Grid No.1 voltage for visual extinction of focused raster (grid drive service) | -v _{g1} | = | 32 to 69 | v |
| Cathode voltage for visual extinction of focused raster (cathode drive service) | v _k | = | 29 to 62 | v |

1) Reference line

 2) The maximum dimension is determined by the reference line gauge

7Z2 7814

3

M21-11W

RESOLUTION

| Resolution at screen centre | | | min. | 650 | lines |
|-----------------------------|-------------------|---|------|-----|-------|
| Measured at: | $v_{g_3, g_5(l)}$ | = | | 12 | kV |
| | v _{g2} | = | | 400 | V |

61.1.1

This tube will resolve 650 lines measured at a brightness of 340 Nits based on a picture height of 135 mm.

The focus voltage is adjusted to obtain the smallest roundest spot. For optimum overall resolution an external centring magnet may be required.

LIMITING VALUES (Absolute max. rating system)

| Final accelerator voltage | 17 (| = | max. | 16 | kV |
|---------------------------------------|--|----------|------|-------------|------------|
| Final accelerator voltage | $vg_{3},g_{5}(l)$ | 0=0 | min. | 9 | kV |
| Focus voltage | | | | | |
| positive | Vg4 | = | max. | 1000 | V |
| negative | $-v_{g_4}$ | = | max. | 500 | V |
| First accelerator voltage | Vg2 | = | max. | 800 | V |
| Grid No.1 voltage | | | | | |
| positive | v _{g1} | = | max. | 0 | V |
| positive peak | Vglp | = | max. | 2 | V |
| negative | $-v_{g_1}$ | = | max. | 180 | V |
| Cathode to heater voltage | and the second s | | | | |
| positive | V _{k-f} | = | max. | 80 | V |
| positive peak | V _{k-fp} | 57 | max. | 130 | V |
| Focusing electrode current | Ig4 | = | max. | <u>+</u> 25 | μA |
| Accelerator current | Ig2 | 7 | max. | <u>+</u> 5 | μA |
| MAXIMUM CIRCUIT VALUES | | | | | |
| Resistance between cathode and heater | R _{k/f} | = | max. | 1 | MΩ |
| Impedance between cathode and heater | Z _{k/f} (50 Hz) | <u> </u> | max. | 500 | kΩ |
| Impedance between cathode and earth | Z _k (50 Hz) | = | max. | 100 | kΩ |
| Grid No.1 circuit resistance | Rg1 | = | max. | 1.5 | MΩ |
| Grid No.1 circuit impedance | Zg ₁ (50 Hz) | = | max. | 500 | kΩ |
| Accelerator circuit resistance | Rg ₂ | = | max. | 1 | MΩ |
| Focusing electrode circuit resistance | R _{g4} | = | max. | 3 | MΩ 7815 |
| | | | | 1 | 1010 |

M21-11W



A



В



M21-11W



D

M21-11W







MONITOR TUBE

21 cm rectangular television tube with metal backed screen primarily intended for use as a picture monitor tube.

| QUICK REFERE | NCE DATA |
|------------------|------------------|
| Deflection angle | 110 ^o |
| Focusing | electrostatic |
| Resolution | 625 lines |
| Overall length | max. 205 mm |

SCREEN

Metal backed phosphor

| Lumenescence | white | | | |
|----------------------------------|-------|-------|----|--|
| Light transmission of face glass | | 80 | % | |
| Useful diagonal | min. | 200 | mm | |
| Useful width | min. | 190.5 | mm | |
| Useful height | min. | 149.2 | mm | |

HEATING

| Indirect by A.C. or D.C.; | parallel supply | | | | |
|---------------------------|-----------------|---------------------|---|-----|----|
| | Heater voltage | $\underline{v_{f}}$ | = | 6.3 | v |
| | Heater current | I_{f} | = | 300 | mA |

CAPACITANCES

| Final accelerator to external conductive | | | | |
|--|------------------------|---|-------|-----|
| coating | $C_{g_3, g_5}(\ell)/m$ | = | 250 | pF |
| Cathode to all other elements | Ck | = | 4.0 | pF |
| Grid No.1 to all other elements | c_{g_1} | = | 7.0 | pF |
| | | | 7Z2 5 | 653 |

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TENTATIVE DATA

MECHANICAL DATA

Dimensions in mm





7Z2 7816

2



Dimensions in mm



Mounting position: any

Except vertical with the screen downward and the axis of the tube making an angle of less than 20° with the vertical.

Base:

Cavity contact

Neo Eightar (B8H) CT8

Accessories

Final accelerator connector

type 55563

¹) Reference line, determined by the plane of the upper edge of the flange of the reference line gauge JEDEC 126 when the gauge is resting on the cone.

2) The maximum dimension is determined by the reference line gauge. 7Z2 7817

FOCUSING

electrostatic

'The range of focus voltage shown under "Typical operating conditions" results in optimum focus at a beam current of 100 μ A.

DEFLECTION magnetic

Diagonal deflection angle

110⁰

PICTURE CENTRING MAGNET

Field intensity perpendicular to the tube axis adjustable from 0 to 79.6 A/m (0 to 10 Oerstedt).

Adjustment of the centring magnet should not be such that a general reduction in brightness or shading of the raster occurs.

TYPICAL OPERATION

| Final accelerator volt | age | $V_{g_3}, g_5(l)$ | = | 16 | kV | 7 |
|------------------------|---------------------------------|-------------------|---|------------|----|----|
| Focusing electrode vo | ltage | Vg ₄ | = | 0 to 400 | V | 1) |
| First accelerator volt | age | Vg2 | = | 300 | V | |
| Grid No.1 voltage for | extinction of focused raster | Vg1 | = | -35 to -72 | V | |

RESOLUTION

| Resolution | at | scre | en | cent | re n | nea | asur | ed |
|----------------------|------------------|------|----|------|------|-----|------|----|
| at Vg ₃ , | g ₅ (| l) = | 16 | kV, | Vg2 | = | 300 | V |

BRIGHTNESS

Brightness at $V_{g_3}, g_5(\ell) = 16 \text{ kV}$, $I_{g_3}, g_5(\ell) = 80 \mu \text{A}$ measured with a raster of 14 x 14 cm² 625 lines

450 Nit

With the small change in focus spot size with variation of focus voltage, the limit of 0 to 400 V is such that an acceptable focus quality is obtained within this range. If it is required to pass through the point of focus, a voltage of at least -100 to +500 V will be required. 7Z2 7818

LIMITING VALUES (Absolute max. rating system)

| Final accelerator voltage | $v_{g_3,g_5}(\ell)$ | = | max. 20 min. 13 | kV kV |
|---------------------------------------|------------------------|-----|----------------------|------------------|
| Focusing electrode voltage | $v_{g_4} - v_{g_4}$ | 8 | max. 1 max. 500 | kV V |
| First accelerator voltage | Vg ₂ | н н | max. 450 min. 200 | V V |
| Cathode to heater voltage | V _{+k/f} - | = | max. 200 | V |
| | $V_{+k/f-p}$ | = | max. 300 | V 1) |
| | V-k/f+ | = | max.125 | V |
| | V-k/f+p | = | max. 250 | V , |
| Grid No.1 voltage | | | | |
| positive | Vg ₁ | = | max. 0 | V ²) |
| positive peak | Vglp | = | max. 2 | V |
| negative | $-V_{g_1}$ | =. | max. 150 | V |
| Focusing electrode current | Ig4 | = | max. <u>+</u> 25 | μA |
| First accelerator current | Ig ₂ | = | max. <u>+</u> 5 | μΑ |
| ODCHUT DESIGN VALUES | | | | |
| CIRCUIT DESIGN VALUES | | | | |
| Resistance between cathode and heater | Rkf | = | max. 1 | MΩ |
| Impedance between cathode and heater | Z_{kf} (50 Hz) | = | max. 0.5 | MΩ |
| Impedance between cathode and earth | Z _k (50 Hz) | = | max. 0.1 | MΩ |
| Grid No.1 circuit resistance | Rg ₁ | = | max. 1.5 | MΩ |
| Grid No.1 circuit impedance | Zg1(50 Hz) | = | max. 0.5 | MΩ |

¹) During a warm-up period not exceeding 45 s the heater may be 410 V negative with respect to the cathode.

Rg₂

Rg4

First accelerator circuit resistance

Focusing electrode circuit resistance

7Z2 7951

MΩ

 $3 M\Omega$

1

max.

max.

 \equiv

²⁾ The d.c. value of bias must not be such as to allow the grid to become positive with respect to the cathode, except during the period immediately after switching the receiver on or off when it may be allowed to rise to +1 V. The maximum positive excursion of the video signal must not exceed +2 V, and at this voltage the grid current may be expected to be approximately 2 mA.



MONITOR TUBE

The M28-12W is a rectangular $28 \text{ cm} 90^\circ$ deflection angle direct viewing picture tube primarily intended as a monitor tube.

| QUICK REFERENCE DATA | | | | | | |
|----------------------------------|----------|---------------|--|--|--|--|
| Face diagonal | 28 | cm (11 inch) | | | | |
| Deflection angle | 900 |) | | | | |
| Overall length | 245 | mm | | | | |
| Neck length | 105.5 | mm | | | | |
| Neck diameter | 20 | mm | | | | |
| Light transmission of face glass | 50 | % | | | | |
| Focusing | | electrostatic | | | | |
| Bulb | | reinforced | | | | |
| Heating | 11 V, 68 | mA | | | | |
| Resolution | min. 850 | lines | | | | |

SCREEN

| Metal backed phosphor | | | |
|----------------------------------|-------|-------|----|
| Luminescence | white | | |
| Light transmission of face glass | | 50 | % |
| Useful diagonal | min. | 262.5 | mm |
| Useful width | min. | 228 | mm |
| Useful height | min. | 171 | mm |

HEATING

Indirect by A.C. or D.C.

| Heater voltage | Vf | 11 | V |
|----------------|--------------------|-----|------|
| Heater current | $\overline{I_{f}}$ | 68 | mA |
| | | 7Z2 | 7979 |

11.11.1966

TENTATIVE DATA

1

MECHANICAL DATA

Dimensions in mm





MECHANICAL DATA (continued)

Dimensions in mm



Mounting position: any

Base

Net weight

. .

: 7 pins miniature, with pumping stem : approx. 2.2 kg

The socket for the base should not be rigidly mounted; it should have flexible leads and be allowed to move freely.

For notes see page 5

MAXIMUM CONE CONTOUR DRAWING

(Dimensions in mm)



| | istance int Z | | | | | Distan | ce from | centre (| max. va | lues) | | | | |
|---------|-------------------|--------------------------------|-----------------|-----------------|-----------------|-----------------|--|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|----------------------------------|
| Section | Nom. d from pc | Long axis 0 ⁰ | 10 ⁰ | 20 ⁰ | 25 ⁰ | 30 ⁰ | 34 ⁰ 40 ⁰ Diag. | 40 ⁰ | 45 ⁰ | 50 ⁰ | 60 ⁰ | 70 ⁰ | 80 ⁰ | Short axis 90 ⁰ |
| 1 | 27.5 | 130.00 | 131.62 | 136.64 | 140.59 | 145.50 | 147.50 | 144.87 | 136.81 | 127.86 | 114.90 | 106.84 | 102.41 | 101.00 |
| 2 | 37.5 | 127.35 | 128.90 | 133.85 | 137.70 | 142.40 | 144.90 | 141.80 | 133.30 | 124.85 | 112.60 | 105.15 | 101.15 | 99.90 |
| 3 | 47.5 | 121.10 | 122.60 | 126.85 | 130.45 | 134.70 | 137.55 | 133.90 | 125.55 | 118.45 | 108.25 | 102.00 | 98.95 | .97.90 |
| 4 | 57.5 | 114.05 | 115.15 | 118.70 | 121.65 | 125.25 | 127.30 | 124.50 | 117.50 | 111.55 | 103.10 | 98.10 | 95.75 | 95.20 |
| 5 | 67.5 | 106.35 | 107.20 | 110.00 | 112.25 | 114.85 | 116.40 | 114.25 | 108.85 | 104.00 | 97.20 | 93.50 | 92.00 | 91.75 |
| 6 | 77.5 | 97.60 | 98.25 | 100.05 | 101.45 | 103.30 | 104.45 | 102.80 | 98.80 | 95.10 | 90.00 | 87.45 | 86.85 | 86.95 |
| 7 | 87.5 | 87.40 | 87.75 | 88.85 | 89.70 | 90.70 | 91.40 | 90.25 | 87.70 | 85.15 | 81.70 | 80.40 | 80.50 | 81.00 |
| 8 | 97.5 | 75.05 | 75.35 | 76.15 | 76.70 | 76.95 | 76.85 | 76.05 | 74.90 | 73.85 | 72.45 | 72.15 | 72.75 | 73.40 |
| 9 | 107.5 | 60.65 | 60.65 | 60.65 | 60.65 | 60.65 | 60.65 | 60.65 | 60.55 | 60.35 | 60.20 | 60.60 | 61.00 | 61.35 |
| 10 | 117.5 | 48.00 | 48.00 | 48.00 | 48.00 | 48.00 | 48.00 | 48.00 | 48.00 | 48.00 | 48.00 | 48.00 | 48.00 | 48.00 |

CAPACITANCES

| Final accelerator to ex | ternal | | - 950 | nΕ | COLOR OF C |
|-------------------------|---------------|------------------------|-------|----------|------------|
| conductive coating | | C _{a,g3,g5/m} | > 550 | pr pF | |
| Final accelerator to me | etal band | $C_{a, g_3, g_5/m}$ | 150 | pF | |
| Cathode to all | | Ck | 3 | pF | |
| Grid No.1 to all | | Cg1 | 7 | pF | |
| FOCUSING | electrostatic | | | | |

| DEFLECTION | magnetic | |
|---------------------|------------|-----------------|
| Diagonal deflectí | on angle | 900 |
| Horizontal deflec | tion angle | 800 |
| Vertical deflection | on angle | 63 ⁰ |

PICTURE CENTRING MAGNET

Field intensity perpendicular to the tube axis adjustable from 0 to 800 A/m (0 to 10 Oerstedt).

Maximum distance between centre of field of this magnet and reference line: 55mm. The centring magnet should be mounted as close to the deflection coils as possible.

NOTES TO OUTLINE DRAWING

- 1. The reference line is determined by the plane of the upper edge of the flange of the reference line gauge when the gauge is resting on the cone.
- 2. The configuration of the external conductive coating is optional but contains the contact area shown in the drawing.

The external conductive coating must be earthed.

- 3. End of guaranteed contour. The maximum neck and cone contour is given by the reference line gauge.
- 4. This area must be kept clean.
- 5. Recessed cavity contact.
- 6. Maximum unflatness of the rim is 1 mm.
- 7. The mounting screws in the cabinet must be situated inside a circle with a diameter of 5 mm drawn around the corner points of a geometrical rectangle of 240 mm x 182.5 mm.

FACE PLATE CONTOUR



Dimensions of the outer contour of the face plate on the mold match line.

REFERENCE LINE GAUGE

Dimensions in mm



The reference line is determined by the plane of the upper edge of the flange of the reference line gauge when the gauge is resting on the cone.

| Grid drive service | | | | |
|---|-----------------------|------------|------------|------|
| Final accelerator voltage | V _{a,g3} ,g5 | 11 | 13 | kV |
| Focusing electrode voltage | Vg4 | 50 to 350 | 0 to 400 | V 1) |
| Grid No.2 voltage | Vg ₂ | 250 | 350 | V |
| Grid No.l voltage for visual extinction of focused raster | v _{g1} | -35 to -69 | -46 to -91 | v |
| Cathode drive service | | | | |
| Voltages are specified with res | spect to grid N | lo.1 | | |
| Final accelerator voltage | V _{a,g3,g5} | 11 | 13 | kV |
| Focusing electrode voltage | Vg ₄ | 0 to 350 | 50 to 400 | V 1) |
| Grid No.2 voltage | Vg ₂ | 200 to 350 | 350 | V |
| Cathode voltage for visual extinction of focused raster | V _k | approx.45 | 44 to 80 | v |

| Final accelerator voltage | V _a , g ₃ , g ₅ | min. | 7.5 | k V kV |
|--------------------------------|--|--------------|------------|-----------|
| Grid No.4 voltage | Vg | | | |
| positive | Vg4 | max. | 500 | V |
| negative | -Vg4 | max. | 50 | V |
| Grid No.2 voltage | Vg2 | max. min. | 350 200 | V V |
| Grid No.2 to grid No.1 voltage | v_{g_2}/v_{g_1} | max. | 450 | V |
| Grid No.1 voltage | | | | |
| positive | v_{g_1} | max. | 0 | V |
| positive peak | Vg _{1p} | max. | 2 | V |
| negative | -V _{g1} | max. | 100 | V |
| negative peak | -V _{g1p} | max. | 350 | V 2 |

1) Voltage range to obtain optimum overall focus at 100 μ A beam current.

²) Maximum pulse duration 22% of a cycle but max. 1.5 ms.

7Z2 7980

M28-12W

| LIMITING VALUES | (continued) |
|-----------------|-------------|
|-----------------|-------------|

Cathode to grid No.1 voltage

| positive | v_{k/g_1} | max. | 100 | V |
|--|-------------------------|------|-----|------|
| positive peak | V _{k/g1p} | max. | 350 | V 1) |
| negative | $-v_{k/g_1}$ | max. | 0 | v |
| negative peak | $-V_{k/g_{1p}}$ | max. | 2 | v |
| Cathode to heater voltage | s start had | | | |
| positive | V _{k/f} | max. | 110 | v |
| positive peak | V _{k/fp} | max. | 130 | v |
| CIRCUIT DESIGN VALUES | | | | |
| Grid No.4 current | | | | |
| positive | Ig4 | max. | 25 | μA |
| negative | -Ig4 | max. | 25 | μA |
| Grid No.2 current | | | | |
| positive | Ig2 | max. | 5 | μΑ |
| negative | -Ig2 | max. | 5 | μA |
| MAXIMUM CIRCUIT VALUES | | | | |
| Resistance between cathode and heater | R _{k/f} | max. | 1 | MΩ |
| Impedance between cathode and heater | $Z_{k/f}$ (50 Hz) | max. | 0.1 | MΩ |
| Grid No.1 circuit resistance | Rg1 | max. | 1.5 | MΩ |
| Grid No.1 circuit impedance | Z _{g1} (50 Hz) | max. | 0.5 | MΩ |
| Resistance between external conductive | | | | |

coating and rimband

 $R_{m/m}$ ' max. 2 M Ω

1) Maximum pulse duration 22% of a cycle but max. 1.5 ms.



11.11.1966

A



В

MONITOR TUBE

36 cm rectangular television tube with metal backed screen primarily intended for use as a precision monitor.

| QUICK REFERENCE DATA | | | | |
|----------------------|-----------------|--|--|--|
| Deflection angle | 90 ⁰ | | | |
| Focusing | electrostatic | | | |
| Resolution | min. 650 lines | | | |
| Overall length | max. 317 mm | | | |

SCREEN

Metal backed phosphor

| Lumenescence | white |
|-----------------|---------------|
| Useful diagonal | min. 330 mm |
| Useful width | min. 306.5 mm |
| Useful height | min. 241 mm |

HEATING

| Indirect by A.C. or D.C. | ; parallel supply | | | | | | |
|--------------------------|-------------------|---------------------|-----|----|----|-----|---|
| | Heater voltage | $\underline{V_{f}}$ | = - | 11 | V | ±10 | % |
| | Heater current | I_{f} | = | 70 | mA | 4 | |

CAPACITANCES

| Final accelerator to external co | nductive | | | | |
|----------------------------------|----------|---------------------------|---|-----|----|
| | coating | $C_{g_{3},g_{5}}(\ell)/m$ | = | 800 | pF |
| Cathode to all other elements | | Ck | = | 5.0 | pF |
| Grid No.1 to all other elements | | Cg1 | = | 9.0 | pF |

7Z2 7820

TENTATIVE DATA

MECHANICAL DATA

Dimensions in mm



¹) Reference line is determined by the plane of the upper edge of the flange of the reference line gauge when the gauge is resting on the cone.

 2) The maximum dimension is determined by the reference line gauge.

Dimensions in mm

MECHANICAL DATA (continued)



Mounting position: any

Except vertical with the screen downward and the axis of the tube making an angle of less than 20° with the vertical.

CT8

Neo Eightar (B8H)

Base:

Cavity contact

Accessories:

Socket

Final accelerator connector type 55563

FOCUSING

electrostatic

The range of focus voltage shown under typical operating conditions results in optimum focus at a beam current of 100 μ A.

90⁰

DEFLECTION

magnetic

Diagonal deflection angle

PICTURE CENTRING MAGNET

Field intensity perpendicular to the tube axis adjustable from 0 to 79.6 A/m (0 to 10 Oerstedt).

Adjustment of the centring magnet should not be such that a general reduction in brightness or shading of the raster occurs.

REFERENCE LINE GAUGE



TYPICAL OPERATION

| Final accelerator voltage | $V_{g_{3},g_{5}(l)}$ | = | | 16 | kV |
|--|----------------------|---|--------|-----|------|
| Focusing electrode voltage | Vg4 | = | 0 to 5 | 500 | V 1) |
| First accelerator voltage | Vg2 | = | (| 500 | V |
| Grid No.1 voltage for extinction of focused raster (grid drive service) | -Vg1 | = | 43 to | 98 | V |
| Cathode voltage for extinction of focused raster (cathode drive service) | Vk | = | 40 to | 90 | v |
| RESOLUTION | | | | | |

Resolution at screen centremin. 650linesMeasured at: $V_{g_3,g_5(\ell)} = 16$ kV $V_{g_2} = 600$ V

This tube will resolve 650 lines measured at a brightness of 340 Nits based on a picture height of 237 mm.

The focus voltage is adjusted to obtain the smallest roundest spot. For optimum overall resolution an external centring magnet may be required.

 With the small change in focus spot size with variation of focus voltage, the limit of 0 to 500 V is such that an acceptable focus quality is obtained within this range. If it is required to pass through the point of focus, a voltage of at least -100 V to +600 V will be required.

LIMITING VALUES (Absolute max. rating system)

| Final accelerator voltage | $V_{g_{3},g_{5}}(\ell)$ | = | max. 18 min. 12 | kV kV |
|--------------------------------|-------------------------|----|--------------------|------------------|
| Focusing electrode voltage | $-v_{g_4}^{v_{g_4}}$ | = | max. l max. 500 | kV V |
| First accelerator voltage | v _{g2} | = | max. 800 | V |
| Grid No.1 voltage | | | | |
| positive | Vg1 | = | max. 0 | V ¹) |
| positive peak | Vglp | = | max. 2 | V |
| negative | $-V_{g_1}$ | = | max. 180 | V |
| Cathode to heater voltage | V _{k/f} | = | max. 80 | V |
| Cathode to heater peak voltage | $V_{k/f_{p}}$ | =, | max. 130 | V |
| Focusing electrode current | Ig4 | = | max. <u>+</u> 25 | μA |
| First accelerator current | Ig2 | = | max. <u>+</u> 5 | μA |
| | | | | |

MAXIMUM CIRCUIT VALUES

| Resistance between cathode and heater | R _{k/f} | = | max. 1 | MΩ |
|---------------------------------------|-------------------------------------|---|----------|----|
| Impedance between cathode and heater | $\mathrm{Z}_{k/\mathrm{f}}$ (50 Hz) | = | max. 500 | kΩ |
| Impedance between cathode and earth | $\mathrm{Z}_{k/f}$ (50 Hz) | = | max. 100 | kΩ |
| Grid No.1 circuit resistance | Rg1 | = | max. 1.5 | MΩ |
| Grid No.1 circuit impedance | z_{g_1} (50 Hz) | = | max. 500 | kΩ |
| First accelerator circuit resistance | R _{g2} | = | max. 1 | MΩ |
| Focusing electrode circuit resistance | Rga | = | max. 3 | MΩ |

¹) The d.c. value of bias must not be such as to allow the grid to become positive with respect to the cathode, except during the period immediately after switching the receiver on or off when it may be allowed to rise to +1 V. The maximum positive excursion of the video signal must not exceed +2 V, and at this voltage the grid current may be expected to be approximately 2 mA.

7Z2 7823

5

EXTERNAL CONDUCTIVE COATING

This tube has an external conductive coating, m, which must be earthed and the capacitance of this to the final electrode is used to provide smoothing for the e.h.t. supply. The tube marking and warning labels are on the side of the cone opposite the final electrode connector and this side should not be used for making contact to the external conductive coating.

WARNING

X-ray shielding is advisable to give protection against danger of personal injury arising from prolonged exposure at close range to this tube,



Α



В



С



D
M36-11W



E



MONITOR TUBE

The M36-13W is a 36 cm diameter rectangular television tube with metal backed screen primarily intedned for use as a monitor tube.

| | 110 ⁰ | |
|------|------------------|---|
| | electro | static |
| min. | 625 | lines |
| max. | 268.5 | mm |
| | | |
| | min. max. | 110 ⁰ electro min. 625 max. 268.5 |

| Colour | white | | |
|------------------------|-------|-------|----|
| Useful screen diagonal | min. | 333.4 | mm |
| Useful screen width | min. | 314.3 | mm |
| Useful screen height | min. | 250.8 | mm |

HEATING

Indirect by A.C. or D.C.; parallel or series supply

| He | eater voltage | V _f 6.3 | V | | |
|--------------------------------|--------------------|--------------------|-------|-----|----|
| Не | eater current | I _f 300 | mA | | |
| CAPACITANCES | | | | | |
| Control grid to all other elem | nents | Cg1 | | 7.0 | pF |
| Cathode to all other elements | 5 | Ck | | 4.0 | pF |
| Final accelerator to external | conductive coating | C_{g_2,g_5} | (ℓ)/m | 800 | pF |

7Z2 7824

11.11.1966

TENTATIVE DATA

MECHANICAL DATA

Dimensions in mm





MECHANICAL DATA (continued)

Dimensions in mm



Mounting position: any, except vertical with the screen downward and the axis of the tube making an angle of less than 20° with the vertical.

Neo eightar (B8H)

Cavity contact

Base

Accessories

Final accelerator contact connector

type 55563

CT8

FOCUSING electrostatic

The range of focus voltage shown under "Typical operating conditions" results in optimum focus at a beam current of 100 μA .

DEFLECTION

double magnetic

diagonal deflection angle 110^o

 $(1)^{2}(3)^{4}(5)$ See page 6.

PICTURE CENTRING MAGNET

Field intensity perpendicular to the tube axis adjustable from 0 to 79.6 A/m (0 to 10 Oerstedt). Adjustment of the centring magnet should not be such that a general reduction in brightness or shading of the raster occurs.

REFERENCE LINE GAUGE

Dimensions in mm



TYPICAL OPERATING CONDITIONS

| Final accelerator voltage | $V_{g_3,g_5}(\ell)$ | 16 | kV |
|---|----------------------|----------|------------------|
| Focusing electrode voltage | Vg4 | 0-400 | V ¹) |
| First accelerator voltage | v_{g_2} | 400 | V |
| Grid No.1 voltage for visual extinction of a focused raster | -v _{g1} | 40 to 85 | V |
| Resolution at screen centre | | min. 625 | lines |
| Measured at | $V_{g_{3},g_{5}}(l)$ | 16 | kV |
| | Vg ₂ | 400 | V |

This tube will resolve 625 lines measured at a brightness of 340 Nits based on a picture height of 237 mm.

The focus voltage is adjusted to obtain the smallest roundest spot. For optimum overall resolution an external centring magnet may be required. 7Z2 7952

| M3 | 6-1 | 3W |
|-----------|-----|----|
|-----------|-----|----|

| LIMITING VALUES | (Absolute | max. | rating | system) |) |
|-----------------|-----------|------|--------|---------|---|
|-----------------|-----------|------|--------|---------|---|

Measured with respect to cathode

| Final accelerator voltage | $v_{g_3,g_5}(\ell)$ | max. min. | 18 13 | kV kV |
|---|---------------------------|--------------|-------------|----------|
| Focusing electrode voltage | v_{g_4} - v_{g_4} | max. max. | 1 500 | kV V |
| First accelerator voltage | vg2 | max. min. | 550 350 | V V |
| Control grid voltage, | | | | |
| negative | -Vg1 | max. | 150 | v |
| positive | Vg1 | max. | 0 | V |
| Focusing electrode current | Ig4 | max. | <u>+</u> 25 | μA |
| Grid No.2 current | Ig2 | max. | <u>+</u> 5 | μA |
| Cathode to heater voltage, | | | | |
| cathode positive | V+k/f- V+k/f-p | max. max. | 250 300 | V V |
| cathode negative | V-k/f+ V-k/f+p | max. max. | 135 180 | V V |
| Resistance between heater and cathode | R _{kf} | max. | 1 | MΩ |
| Resistance between grid No.1 and earth | Rg1 | max. | 1.5 | MΩ |
| Impedance between heater and cathode (f = 50 Hz) | Z _{kf} | max. | 500 | kΩ |
| Impedance between cathode and earth $(f = 50 \text{ Hz})$ | $\mathbf{z}_{\mathbf{k}}$ | max. | 100 | kΩ |

¹) With the small change in focus spot size with variation of focus voltage the limit of 0-400 V is such that an acceptable focus quality is obtained within this range. If it is required to pass through the point of focus, a voltage of at least -100 V to +500 V will be required. 7Z2 6451

WARNING

X-ray shielding is advisable to give protection against possible danger of personal injury arising from prolonged exposure at close range to this tube when operated above 16 kV.

EXTERNAL CONDUCTIVE COATING

This tube has an external conductive coating (m), which must be earthed and capacitance of this to the final electrode is used to provide smoothing for the EHT supply. The tube marking and warning labels are on the side of the cone opposite the final electrode connector and this side should not be used for making contact to the external conductive coating.

NOTES TO OUTLINE DRAWING

- The reference line is determined by the plane of the upper edge of the flange of the reference line gauge, (JEDEC 126) when the gauge is resting on the cone.
- ²) Bulge at splice-line seal may increase the indicated maximum value for envelope width, diagonal and height by not more than 6.4 mm, but at any point around the seal, the bulge will not protrude more than 3.2 mm beyond the envelope surface at the location specified for dimensioning the envelope width, diagonal and height.
- ³) The tube should be supported on both sides of the bulge. The mechanism used should provide clearance for the maximum dimensions of the bulge.
- ⁴) Measured 12 + 1 mm from the centre-line of the screen-cone seal.
- ⁵) The maximum dimension is determined by the reference line gauge.

FLYING SPOT SCANNER TUBE

The M.13-36 is a 13 cm diameter cathode-ray tube intended for flying spot applications.

| | QUICK REFERENCE DATA | |
|---------------------|----------------------|-----------------|
| Accelerator voltage | | 25 kV |
| Deflection angle | | 40 ⁰ |
| Resolution | | 1000 lines |

SCREEN

Metal backed

| | Colour | Persistence |
|---------|---------------|-------------|
| MC13-16 | Purplish blue | Very short |
| MK13-16 | Green | Short |

Useful screen diameter

HEATING

Indirect by A.C. or D.C.; series or parallel supply

| Heater voltage | v_{f} | 6.3 | V |
|----------------|---------|-----|----|
| Heater current | If | 300 | mA |

CAPACITANCES

| Grid No.1 to all other electrodes | C _{g1} | | 6.5 | pF |
|---|-----------------|--------|-----|----|
| Cathode to all other electrodes | Ck | | 6.5 | pF |
| Accelerator to outer conductive coating | $C_{g_2(l)/m}$ | 250 to | 450 | pF |

7Z2 6432

108

mm

min.

MECHANICAL DATA

Dimensions in mm



Mounting position: any, except with screen downwards and the axis of the tube making an angle of less than 50° with the vertical.

Base

Duodecal 7p.

- Reference line, determined by the plane of the upper edge of the reference line gauge when the gauge is resting on the cone.
- ²) Insulating outer coating; should not be in close proximity to any metal part.
- ³) Conductive outer coating; to be grounded.
- 4) Recessed cavity contact.
- 5) Spark trap; to be grounded.
- 6) The distance between the deflection centre and the reference line should not exceed 31 mm.
- 7) Distance between the centre of the magnetic length of the focusing unit and the reference line. 7Z2 6433

Dimensions in mm

FOCUSING

magnetic

Focusing coil

type AT1997

DEFLECTION

magnetic

REFERENCE LINE GAUGE



OPERATING CHARACTERISTICS

| Accelerator voltage | $v_{g_2(\ell)}$ | 25 | kV |
|------------------------------------|------------------------|-----------|----|
| Beam current | Il | 50 to 150 | μA |
| Negative grid No.1 cut-off voltage | $-v_{g_1}(I_{\ell}=0)$ | 50 to 100 | v |
| | 1. | | |

Resolution at centre of screen better than 1000 lines 1)

1) With focusing coil AT1997

LIMITING VALUES (Absolute max. rating system)

| Accelerator voltage | $V_{g_2(\ell)}$ | max. min. | 27 20 | kV kV |
|--|---------------------------|--------------|----------|----------|
| Grid No.1 voltage, | | | | |
| negative value | -Vg1 | max. | 200 | V |
| positive value | $+Vg_1$ | max. | 0 | V |
| peak positive value | $+V_{g_{1p}}$ | max. | 2 | V |
| Cathode current | Ik | max. | 150 | μΑ |
| Voltage between heater and cathode 1) | | | | |
| cathode negative | V _{kf} (k neg.) | max. | 125 | V |
| cathode positive | V _{kf} (k pos.) | max. | 200 | V |
| peak value, cathode positive | V _{kfp} (k pos.) | max. | 410 | V^2 |
| External resistance between heater and cathode | R _{kf} | max. | 1 | MΩ |
| External grid No.1 resistance | Rg1 | max. | 1.5 | MΩ |
| External grid No.l impedance at a frequency of 50 Hz | Z_{g_1} (f = 50 Hz) | max. | 0.5 | MΩ |

REMARKS

Measures should be taken for the beam current to be switched off immediately when one of the time-base circuits becomes defective.

An X-ray radiation shielding with an equivalent lead thickness of 0.5 mm is required to protect the observer.

 2) During a heating-up period not exceeding 45 sec.

¹⁾ In order to avoid excessive hum, the A.C. component of the heater to cathode voltage should be as low as possible and should not exceed 20 $V_{\rm RMS}$.





MG/U/Y6-2

PROJECTION TUBE

SCREEN

Metal backed

| Туре | MG6-2 | MU6-2 | MY6-2 |
|--------------|---------------|---------------|---------------|
| Colour | green | blue | yellow |
| Colour point | x=0.19 y=0.72 | x=0.17 y=0.13 | x=0.54 y=0.46 |

The MY6-2 should be used in conjunction with a suitable filter (e.g. Wratten filter No.25).

Colour points of MY in combination with Wratten No.25 filter x=0.67 y=0.33Useful screen diametermin. 55 mm

HEATING: Indirect by A.C. or D.C.; parallel or series supply



1) Inner radius of curvature of the face plate.

The deviation of the centre of the outer radius of curvature with respect to the centre line of the neck is max. 2 mm.

- Eccentricity of the face plate with respect to the centre line of the neck max. 0.9 mm.
- 3) Reference line, determined by the diameter of 30.28 ± 0.005 mm.
- 4) Spark trap and outer coating. This connection must be earthed.
- 5) The distance from deflection centre to reference line should not exceed 35 mm. 7Z2 7566

OBSOLESCENT TYPE

| a/U/Y6-2 | | | | | |
|---|--|------------------|-------|------|-----|
| FOCUSING | magnetic | | | | |
| DEFLECTION | double magnetic deflection angle 67.5 | 50 | | | |
| TYPICAL OPERAT | ING CONDITIONS | | | | |
| Accelerator voltage | 2 | $V_{g_2(l)}$ | | 25 | kV |
| Negative grid No.1 extinction of a foc | voltage for visual used spot | -Vg ₁ | 40 to | o 90 | V |
| I IMITING VALUES | (Absolute max rating sy | stem) | | | |
| Measured with rest | pect to cathode | occini, | | | |
| Accelerator voltage | e | $v_{g_2(l)}$ | max. | 25 | kV |
| Control grid voltag | e | · | | 200 | * * |
| negative | | -V _{g1} | max. | 200 | V |
| positive | | v _{g1} | max. | 0 | V |
| Cathode to heater v | oltage, | | | | |
| cathode positi | ve | $V_{+k/f}$ - | max. | 125 | V |
| Resistance between | heater and cathode | R _{kf} | max. | 20 | kΩ |
| Resistance between | grid and earth | Rg1 | max. | 1.5 | MΩ |

General observations

Measures should be taken for the anode current to be switched off immediately when one of the time-base circuits becomes defective. An X-ray radiation shielding with an equivalent lead thickness of $0.5 \,\mathrm{mm}$ is required to protect the observer. When the tube is used in an optical box, the screening by the box will in general be sufficient.

MG/U/¥13-38



The M.13-38 are 13 cm diameter projection tubes. The tubes are designed for large screen projection of colour TV displays.

| | QUICK RE | FERENCE DATA | | |
|-------------------|----------------------------|---------------|-----------------|---------------------|
| Final accelerate | or voltage | | 11111 | 50 kV |
| Deflection angle | | | 47 ⁰ | |
| Focusing | | | I | nagnetic |
| SCREEN | | | The state | |
| Туре | MG13-38 | MU13-38 | MY13-38 | |
| Colour | green | blue | yellow | |
| Colour point | x=0.19 y=0.72 | x=0.17 y=0.13 | x=0.661 y=0.331 | |
| Useful diameter | min. 69x92 mm ² | | | |
| Brightress | | | | |
| MG13-38 | | | 2000 | mcd/cm ² |
| MU13-38 | | | 290 | mcd/cm ² |
| MY13-38 | | | 600 | mcd/cm ² |
| measured at V_g | = 50 kV | | | |
| IL | = 500 µA | | | |
| raster size 92x | 69 mm ² | | | |
| HEATING | | | | |

Indirect by A.C. or D.C.; parallel or series supply

| Heater voltage | V_{f} | 6.3 | V |
|----------------|---------|-----|----|
| Heater current | If | 300 | mA |

11.11.1966

TENTATIVE DATA

MG/U/Y13-38

MECHANICAL DATA



Dimensions in mm





- Reference line is determined by position where a gauge 38.1 +0.05 meter and 50 mm long will rest on bulb cone.
- ²) Socket for this base should not be rigidly mounted; it should have flexible leads and be allowed to move freely. Bottom circumference of base shell will fall within circle concentric with cone axis and having a diameter of 50 mm.
- ³) Distance reference line top centre of grid.
- ⁴) This pin must be connected to earth.

MG/U/Y13-38

MECHANICAL DATA (continued)

Mounting position: any, except with screen downwards with the axis at an angle of less than 50° to the vertical.

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

| Base | Duodecal 7 p |
|-------------------------------------|--------------------|
| Dimensions and connections | |
| Overall length | max. 374 mm |
| Face diameter | max. 132.5 mm |
| Net weight | approx. 950 g |
| Accessories | a supervision and |
| Socket | type 5912/20 |
| Final accelerator contact connector | supplied with tube |

CAPACITANCES

| Control grid to all other elements | C_{g_1} | max. | 10 | pF |
|------------------------------------|-----------|------|----|----|
| Cathode to all other elements | Ck | max. | 9 | pF |

magnetic FOCUSING

Distance from the centre of the air gap of the focusing coil to the front of the screen 240 mm

DEFLECTION

double magnetic

deflection angle 47^o

TYPICAL OPERATING CONDITIONS

| Accelerator voltage | $Vg_2(l)$ | , 50 | kV |
|--|------------------|------------|----|
| Negative grid No.1 voltage for visual extinction of focused raster | -Vg ₁ | 100 to 170 | v |
| Peak accelerator current | Igan | min. 2500 | μΑ |

MG/U/Y13-38

| LIMITING VALUES (Absolute max. rating | g system) | | | |
|---|------------------|--------------|----------|-------------------|
| Measured with respect to cathode | | | | |
| Accelerator voltage | $Vg_2(l)$ | max. min. | 55 40 | kV kV |
| Control grid voltage, | | | | |
| negative | -Vg1 | max. | 200 | V |
| positive | v _{g1} | max. | 0 | V |
| positive peak | Vg _{1p} | max. | 0 | V |
| Grid No.2 current | Ig2 | max. | 500 | μA ¹) |
| Cathode to heater voltage, | | | | |
| cathode positive | $V_{+k/f}$ - | max. | 100 | V |
| cathode negative | V-k/f+ | max. | 50 | V ²) |
| Resistance between heater and cathode | R _{kf} | max. | 20 | kΩ |
| Resistance between grid and earth | Rg1 | max. | 1.5 | MΩ |
| Impedance between grid and earth (f = 50 Hz) | z_{g_1} | max. | 0.5 | MΩ |

 1) In order to prevent the possible occurrence of cracked faces, for images with concentrated bright areas (high screen loads) the g2 current should be kept lower than the indicated value. This is especially the case as for as stationary pictures are concerned.

2) In order to avoid excessive hum, the A.C. component of the heater to cath-In order to avoid excessive num, the rest of the second transformed to the second transformation ode voltage should be as low as possible and must not exceed 20 V_RMS. $7Z2\ 7830$

GENERAL OBSERVATIONS

It is essential that means be provided for the instantaneous removal of the beam current in the event of a failure of either one or both of the time bases. Unless such a safety device is incorporated a failure of this type will result in the immediate destruction of the screen of the tube.

Shielding equivalent to a lead thickness of 1 mm is required to protect the observer against X radiation.

The raster dimensions should not come below the minimum of $69x72 \text{ mm}^2$. The screen shall be given adequate cooling by applying a continuous airblast onto the screen of approx. $0.06 \text{ m}^3/\text{sec}$.

In order to prevent damage of the tube caused by a momentary internal arc a resistor of $50 \text{ k}\Omega$ has to be connected between anode contact and the power supply.

Before removing the tube, the screen and the cone should be discharged.

The spark trap and the outer coating of the tube must be connected to earth.

It is necessary to centre the focusing coil to get optimum sharpness.

It is recommended to use the E.H.T. connector, which is delivered with each tube.



MW6-2

PROJECTION TUBE

SCREEN

Metal backed Colour white min. 55 Useful screen diameter mm NAL VINE HEATING: Indirect by A.C. or D.C.; parallel or series supply Heater voltage 6.3 V Heater current If 300 mA 64.8-65.554 MECHANICAL DATA 2.8-55.4 Dimensions in mm 35 Base: V g2.

1) Inner radius of curvature of the face plate.

The deviation of the centre of the outer radius of curvature with respect to the centre line of the neck is max. 2 mm.

- Eccentricity of the face plate with respect to the centre line of the neck max. 0.9 mm.
- 3) Reference line, determined by the diameter of 30.28 ± 0.005 mm.
- 4) Spark trap and outer coating. This connection must be earthed.
- 5) The distance from deflection centre to reference line should not exceed 35 mm. 7Z2 7564

OBSOLESCENT TYPE

| N | 1W6-2 | | | | 4 | |
|---|--|--|------------------|------|-------|----|
| | FOCUSING | magnetic | | | | |
| | DEFLECTION | double magnetic deflection angle 67 | 7.50 | | | |
| | TYPICAL OPERATIN | G CONDITIONS | | | | |
| | Accelerator voltage | | $v_{g_2(l)}$ | | 25 | kV |
| | Negative grid No.1 vo extinction of a focus | oltage for visual ed spot | -V _{g1} | 40 t | :o 90 | v |
| 1 | LIMITING VALUES (A | Absolute max. rating sy | vstem) | | | |
| | Measured with respec | ct to cathode | | | | |
| | Accelerator voltage | | $V_{g_2(\ell)}$ | max. | 25 | kV |
| | Control grid voltage | | -1.50 | | | |
| | negative | | -Vg1 | max. | 200 | v |
| | positive | | Vg1 | max. | 0 | v |
| | Cathode to heater volu | tage, | 48 | | | |
| | cathode positive | | $V_{+k/f}$ – | max. | 125 | V |
| | Resistance between h | eater and cathode | R _{kf} | max. | 20 | kΩ |
| | Resistance between g | rid and earth | Rg1 | max. | 1.5 | MΩ |

General observations

Measures should be taken for the anode current to be switched off immediately when one of the time-base circuits becomes defective. An X-ray radiation shielding with an equivalent lead thickness of $0.5 \,\mathrm{mm}$ is required to protect the observer When the tube is used in an optical box, the screening by the box will in general be sufficient.

MW13_38

PROJECTION TUBE

The MW13-38 is a 13 cm diameter projection tube. The brightness of the tube is such that it can be used for large screen projection of TV displays.

| QUICK REFERENCE DATA | 1 |
|---------------------------|-----------------|
| Final accelerator voltage | 50 kV |
| Deflection angle | 47 ⁰ |
| Focusing | magnetic |

SCREEN

Metal backed

Colour

Useful screen diameter

69 x 92 mm²

white

Brightness

min. 870 mcd/cm²

measured at $V_{g_2} = 50 \text{ kV}$ I₁ = 500 μ A raster size 92 x 69 mm²

HEATING

Indirect by A.C. or D.C.; parallel or series supply

| Heater voltage | Vf | 6.3 | V |
|----------------|----|-----|----|
| Heater current | If | 300 | mA |

CAPACITANCES

| Control grid to all other elements | C_{g_1} | max. | 10 | pF |
|------------------------------------|-----------|------|----|----|
| Cathode to all other elements | Ck | max. | 9 | pF |

MW13-38

MECHANICAL DATA

Dimensions in mm



- ¹) Reference line is determined by position where a gauge $38.1 + \frac{+0.05}{-0.00}$ mm diameter and 50 mm long will rest on bulb cone.
- ²) Socket for this base should not be rigidly mounted; it should have flexible leads and be allowed to move freely. Bottom circumference of base shell will fall within circle concentric with cone axis and having a diameter of 50 mm.
- ³) Distance reference line top centre of grid.
- 4) This pin must be connected to earth.

MW13-38

MECHANICAL DATA (continued)

Mounting position: any, except screen downwards with the axis at an angle of less than 50° to the vertical.

The tube should not be supported by the base alone and under no circumstances should the socket be allowed to support the tube.

Duodecal 7 p

type

5912/20

supplied with tube

Dimensions and connections

| Overall length | | max. 374 | mm |
|----------------|--|-------------|------|
| Face diameter | | max. 132.5 | 5 mm |
| Net weight | | approx. 950 | g |
| | | | |

Accessories

Socket

Base

Final accelerator contact connector

FOCUSING

magnetic

Distance from the centre of the air gap of the focusing coil to the front of the screen 240 mm

DEFLECTION

double magnetic

deflection angle 47⁰

TYPICAL OPERATING CONDITIONS

| Accelerator voltage | $V_{g_2}(\ell)$ | 50 | kV |
|---------------------------------------|-----------------|------------|----|
| Negative grid No.1 voltage for visual | | | |
| extinction of a focused raster | -Vg1 | 100 to 170 | V |
| Peak accelerator current | Ig2- | min. 2500 | μA |

MW13_38

| em) | TAG | | |
|------------------|--|--|---|
| | | | |
| $v_{g_2}(\ell)$ | max. min. | 55 40 | kV kV |
| | | | |
| -Vg1 | max. | 200 | V |
| Vg1 | max. | 0 | V |
| Vg _{1p} | max. | 0 | V |
| Ig2 · | max. | 500 | μA ¹) |
| | | | |
| V+k/f- | max. | 100 | V ²) |
| V-k/f+ | max. | 50 | V |
| | | 40 | Х |
| Rkf | max. | 20 | kΩ |
| Rg1 | max. | 1.5 | MΩ |
| z_{g_1} | max. | 0.5 | MΩ |
| | m) $V_{g_2}(\ell)$ $-V_{g_1}$ $V_{g_{1p}}$ I_{g_2} $V_{+k/f-}$ $V_{-k/f+}$ R_{kf} R_{g_1} Z_{g_1} | m) $V_{g_2}(\ell)$ max. V_{g_1} max. V_{g_1} max. $V_{g_{1p}}$ max. I_{g_2} max. $V_{+k/f-}$ max. $V_{-k/f+}$ max. R_{kf} max. R_{g_1} max. Z_{g_1} max. | m) $V_{g_2}(t)$ max. 55 min. 40 $-V_{g_1}$ max. 200 V_{g_1} max. 0 $V_{g_{1p}}$ max. 0 I_{g_2} max. 500 $V_{+k/f-}$ max. 100 $V_{-k/f+}$ max. 20 R_{g_1} max. 20 R_{g_1} max. 1.5 Z_{g_1} max. 0.5 |

¹) In order to prevent the possible occurrence of cracked faces, for images with concentrated bright areas (high screen loads) the g₂ current should be kept lower than the indicated value. This is especially the case as for as stationary pictures are concerned.

 2) In order to avoid excessive hum, the A.C. component of the heater to cathode voltage should be as low as possible and must not exceed 20 V_{RMS}.

7Z2 6395

GENERAL OBSERVATIONS

It is essential that means be provided for the instantaneous removel of the beam current in the event of a failure of either one or both of the time bases. Unless such a safety device is incorporated a failure of this type will result in the immediate destruction of the screen of the tube.

Shielding equivalent to a lead thickness of 1 mm is required to protect the observer against X radiation.

The raster dimensions should not come below the minimum of $69x72 \text{ mm}^2$. The screen shall be given adequate cooling by applying a continuous airblast onto the screen of approx. $0.06 \text{ m}^3/\text{sec}$.

In order to prevent damage of the tube caused by a momentary internal arca resistor of $50 \text{ k}\Omega$ has to be connected between anode contact and the power supply.

Before removing the tube, the screen and the cone should be discharged.

The spark trap and the outer coating of the tube must be connected to earth.

It is recommended to use the E.H.T. connector, which is delivered with each tube.

It is necessary to centre the focusing coil to get optimum sharpness.



Camera tubes



RATING SYSTEM

ABSOLUTE MAXIMUM RATING SYSTEM

Absolute maximum ratings are limiting values of operating and environmental conditions applicable to any electronic device of a specified type as defined by its published data, which should not be exceeded under the worst probable conditions.

These values are chosen by the device manufacturer to provide acceptable serviceability of the device, taking no responsibility for equipment variations, environmental variations, and the effects of changes in operating conditions due to variations in the characteristics of the device under consideration and of all other electronic devices in the equipment.

The equipment manufacturer should design so that, initially and throughout life, no absolute maximum value for the intended service is exceeded with any device under the worst probable operating conditions with respect to supply voltage variation, equipment component variation, equipment control adjustment, load variations, signal variation, environmental conditions, and variations in characteristics of the device under consideration and of all other electronic devices in the equipment.



55850

CAMERA TUBE

Vidicon with low heater current intended for use in black-and-white or colour TV cameras in industrial, medical and broadcast applications.

| QUICK REFERENCE DATA | | | | |
|----------------------|------------|---------------------------|--|--|
| Resolution | 600 to 900 | TV lines | | |
| Focusing | magnetic | | | |
| Deflection | magnetic | | | |
| Diameter | 25.4 | mm (1 inch) | | |
| Length | 158 | mm ($6\frac{1}{4}$ inch) | | |
| Heater | 6.3 V, 90 | mA | | |

The 55850 has 5 grades:

| 55850 | AM | : low cost tube for experiments, amateur use etc. |
|-------|----|--|
| 55850 | F | : for use in film scanners |
| 55850 | Ν | : for normal industrial applications |
| 55850 | S | : for industrial and broadcast applications in which a higher pic- ture quality is required |
| 55850 | SR | : for use in X-ray medical equipment |

The electrical and mechanical properties of the 5 grades are identical, main differences being found in the degree of uniformity and freedom of blemishes of the photoconductive layers.

OPTICAL

Diagonal of quality rectangle on photoconductive layer (aspect ratio 3 : 4)

max. 16 mm

Orientation of image on photoconductive layer:

horizontal scan should be essentially parallel to the plane passing through tube axis and short index pin. The masking is for orientation only and does not define the proper scanned area of the photoconductive layer.

Spectral response

See page A

55850

HEATING

Indirect by A.C. or D.C., series or parallel supply

| Heater voltage | V_{f} | 6.3 | V +10% |
|----------------|---------|-----|--------|
| Heater current | If | 90 | mA |

Cas

When the tube is used in a series heater chain the heater voltage must not exceed 9.5 $\rm V_{rms}$ when the supply is switched on.

CAPACITANCES

Signal electrode to all

MECHANICAL DATA



NET WEIGHT

approx. 65 g

4.5 pF¹)

¹) This capacitance, which effectively is the output impedance of the 55850, is increased by about 3 pF when the tube is inserted into the deflection and focusing coil-assembly. The resistive component of the output impedance is in the order of 100 M Ω . 7Z2 5675
ACCESSORIES

Socket

Cinch No. 54A18088 or equivalent

Focusing and deflection coil assembly: AT1101, AT1102 or equivalent.

| LIMITING VALUES (Absolute max. rating syst for scanned area of 9.6 mm x 12.8 mm (3/8" | em) x 1/2") ¹) | | | |
|---|-------------------------------|------|------|-------------------|
| Signal electrode voltage | Vas | max. | 100 | V ²) |
| Grid No.4 and grid No.3 voltage | Vg4,g3 | max. | 800 | V |
| Grid No.2 voltage | v _{g2} | max. | 350 | V |
| Grid No.l voltage, negative | -V _{g1} | max. | 125 | V |
| positive | +Vg1 | max. | 0 | V |
| Signal electrode current, peak | I _{asp} | max. | 0.6 | μA ³) |
| | | | | |
| Faceplate illumination | | max. | 5000 | lux |
| Faceplate temperature | t | max. | 80 | °C 4) |
| Cathode to heater voltage, peak | | | | |
| cathode positive | V _{kfp} | max. | 125 | V |
| cathode negative | V _{kfp} | max. | 10 | V |
| Dark current, peak | Idp | max. | 0.25 | μA |

- ²) The signal-electrode voltage should never exceed 100 V, either during heating-up or stand-by, or during operation. An excessive signal-electrode voltage may cause permanent damage to the photoconductive layer.
- 3) Video-amplifiers should be capable of handling signal-electrode currents of this magnitude without amplifier overload or picture distortion.
- 4) Absolute maximum for shelf-life and operation. Under difficult environmental conditions a flow of cooling air directed at the faceplate is recommended. When televising flames and furnaces appropriate infra-red filters should be applied. 7Z2 7683

 [&]quot;Full-size scanning", i.e. scanning of a 9.6 mm x 12.8 mm area of the photoconductive layer should always be applied. The use of a mask having these dimensions is recommended. Underscanning, i.e. scanning of an area less than 9.6 mm x 12.8 mm may cause permanent damage to the specified fullsize area.

OPERATING CONDITIONS AND PERFORMANCE

For scanned area of 9.6 mm x 12.8 mm and faceplate temperature of 25-35 °C

A. PICK-UP FROM LIMITED-MOTION LIVE SCENES

| Conditions | | |
|--|------------|-------------------------|
| Grid No.3 and grid No.4 (beam focus electrode) voltage | 250 - 300 | V ¹) |
| Grid No.2 voltage | 300 | V |
| Grid No.1 voltage adjusted for sufficient beam currents to stabilise highlights | | |
| Minimum peak-to-peak blanking voltage | | |
| when applied to grid No.1 | 75 | V |
| when applied to the cathode | 20 | V ²) |
| Field strength at centre of focusing coil | approx. 40 | Oerstedt ³) |
| Field strength of adjustable alignments coils | 0 - 4 | Oerstedt 4) |
| | | |

 Beam focus is obtained by the combined effect of the grid No.3 voltage, which should be adjustable over the indicated range and a focusing coil having an average field strength of 40 Oerstedt.

Definition, focus uniformity and picture quality decrease with decreasing grid No.3 voltage. In general, grid No.3 should be operated above 250 V.

- ²) In transistorized cameras cathode blanking will be preferable. The cathode impedance is in the order of 30 k Ω .
- ³) The polarity of the focusing coil should be such that a north-seeking pole is attracted to the image end of the focusing coil, with the indicator located outside of and at the image end of the focusing coil.
- ⁴) The alignment coil assembly should be located on the tube so that its centre is at a distance of approx. 94 mm (3 11/16") from the face of the tube and be positioned so that its axis coincides with the axis of the tube, the deflecting yoke and the focusing coil. 7Z2 5677

OPERATING CONDITIONS AND PERFORMANCE (continued)

Performance

| Signal-electrode voltage for dark current | | | |
|--|---------|----------------|-------------------------|
| of 0.02 µA, | range | 20 - 100 | V ¹) |
| | typical | 40 | V |
| Grid No.1 voltage for picture cut-off | - 30 | to -100 | V ²) |
| Signal output current, faceplate illumination 8 lux | typical | 0.150 | μΑ ³) |
| | minimum | 0.075 | μA |
| Resolution capability in picture centre (see page B) | | 600 | TV lines ⁴) |
| Decay: 8 lux on layer, V_{a_S} adjusted for dark current of 0.02 μ A, residual signal after dark pulse of 200 msec | typical | 10 | % |
| Average gamma of transfer characteristic for signal output currents between 0.01 and 0.3 μ A | | 0.6 | |
| Visual equivalent signal-to-noise ratio | approx. | 300 : 1 | 5) |
| | | | |

- ¹) The deflection circuits must provide sufficiently linear scanning for good black-level reproduction. The dark-current signal being proportional to the velocity of scanning, any change in this velocity will produce a black-level error.
- 2) With no blanking voltage on grid No.1.
- Defined as the component of the signal-electrode current after the dark current has been subtracted.
- 4) With a video-amplifier system having 7.5 Mc/s bandwidth (-3 dB points).

⁵) Measured with a peak signal output current of $0.2 \,\mu$ A into a high-gain, cascode-input type of amplifier with an own noise of $0.002 \,\mu$ A r.m.s.and a bandwidth of 5 Mc/s. Because the noise in such a system is predominantly of the high-frequency type, the visual equivalent signal-to-noise ratio is taken as the ratio of the highlight video-signal current to the r.m.s. noise current multiplied by a factor of 3. 7Z2 5678

| | the second se |
|---|---|
| OPERATING CONDITIONS AND PERFORMANCE (continued) | |
| B. PICK-UP FROM FILM (MINIMUM-LAG OPERATION) | |
| Conditions | |
| As under "Pick-up from limited-motion live scenes" with the ex | ception of: |
| Faceplate illumination (highlight) 50 | 00 lux |
| Performance | |
| As under "Pick-up from limited-motion live scenes" with the ex | ception of: |
| Signal-electrode voltage for a dark currentof $0.005 \ \mu A$ 10 - 2 | 20 V |
| Signal output current typical 0. | .3 μA |
| Decay: peak white signal of 0.3 μA, residual signal after dark pulse of 200 msec typical | 3 % |
| | |
| C. OPERATION FOR MAX. RESOLUTION | |
| Conditions | |
| As under "Pick-up from limited-motion live scenes" or "Pick with the exception of: | c-up from film" |
| Grid No.3 and grid No.4 voltage 75 | 50 V |
| Field strength at centre of focusing coil approx. 7 | '0 Oerstedt 1) ²) |
| Performance | |
| As in "Pick-up from limited-mottion live scenes" or "Pick-up the exception of: | from film", with |

Resolution capability in picture centre approx. 900 TV lines

For further details see text and pages B and C

- ¹) The polarity of the focusing coil should be such that a north-seeking pole is attracted to the image end of the focusing coil, with the indicator located outside of and at the image end of the focusing coil.
- 2) With this mode of operation beam-landing errors, resulting in parabolic shading and dark corners, increase. The deflecting and focusing coils should be designed to eliminate these errors.

The increased-power requirements for these coils will increase the tube temperature, adequate provisions for cooling should be made. 7Z2 5679

PRINCIPLE OF OPERATION

SCHEMATIC ARRANGEMENT

The schematic arrangement of the vidicon 55850 with its accessories is shown in Fig.1.

The vidicon may be assumed to consist of three sections, namely the electron gun, the scanning section, and the target section.



Fig. 1 Schematic electrode and coil arrangement

<u>The electron gun</u> contains a thermionic cathode, a grid g_1 controlling the amount of beam, and a limiter anode g_2 which accelerates the electrons and releases them in a fine beam through its diaphragm.

The scanning section. The electron beam released by g_2 enters the space enclosed by the cylindrical anode g_3 . By means of the combined action of the adjustable electrical field of g_3 (beam focus control) and a fixed axial magnetic field produced by the focusing coil, the electrons are focused in one loop on to the target.

The far end of the g_3 cylinder is closed with a fine metal mesh, g_4 , electrically connected to g_3 , which produces a uniform, decelerating field in front of the target. The focused beam is magnetically deflected by two pairs of deflection coils so that it scans the target. Proper alignment of the beam with the axial magnetic field is achieved by either an adjustable magnet, or, as shown in Fig.1, by two sets of alignment coils producing an adjustable transverse magnetic field.

The target section is illustrated in Fig.2. It consists of:

- an optically flat glass faceplate,
- a transparent conductive film on the inner surface of the faceplate, connected electrically to the external signal-electrode ring.
- a thin layer of photoconductive material deposited on the conductive film. In the dark this material has a high specific resistance, which decreases with increasing illumination.

PRINCIPLE OF OPERATION (continued)

The optical image to be televised is focused on the conductive film by means of a lens system.



Fig.2 Target section

OPERATING

The external signal-electrode ring is connected via a load resistor to a positive voltage in the order of 30 V (see Fig.3).

The target may be assumed to consist of a large number of target elements, corresponding to the number of picture elements, each consisting of a small capacitor (C_e), connected on one side to the signal electrode via the transparent conductive film and shunted by a light-dependent resistor (R_{1d} , see Fig.3).

When the target is scanned by the beam its surface will be stabilised at approximately the cathode potential (low-velocity stabilisation) and a potential difference will be established across the photoconductive layer, in other words, each elementary capacitor will be charged to nearly the same potential as applied to the electrode ring.

In the dark, the photoconductive material is a fairly good insulator, so that only a minute fraction of the charge of the elementary ca-



Fig.3

pacitors will leak away between successive scans. This charge will be restored by the beam; the resulting current to the signal electrode is termed "dark current".

When an optical image is focused on to the target, those target elements which are illuminated will become more conductive and will be partly discharged. As a consequence a pattern of positive charges corresponding to the optical image will be produced on the side of target facing the gun section.

OPERATION (continued)

When scanning this charge pattern the electron beam will deposit electrons on the positive elements until the latter are restored to their original cathode potential, causing a capacitive current to the signal electrode and hence avoltage across the load resistor R_L . This voltage, negative going for the highlights, is the video signal and is fed to the pre-amplifier.

A vidicon is called "stabilised" when the magnitude of the beam current applied is just sufficient to restore the scanned surface to cathode potential, so that all elementary capacitors, including those at the highlights in the image, are recharged successively.

During the retrace times the beam electrons should be prevented from landing on the target since otherwise the scan retraces will appear as dark lines in the picture obtained on the monitor. This may be achieved either by cutting off the beam with suitable negative blanking pulses on the control grid or by cutting off the target with adequate positive blanking pulses applied to the cathode.

EQUIPMENT DESIGN AND OPERATING CONSIDERATIONS

The signal-electrode connection is made by a spring contact, which bears against the metal ring at the face end of the tube. The spring contact may be provided as part of the focusing coil design.

The deflection yoke and the focus coil used with the 55850 must be so designed that the beam lands perpendicularly to the target at all points of the scanned area, to ensure high uniformity of sensitivity and focus.

The deflection circuits must provide constant scanning speeds in order to obtain good black-level reproduction. The dark-current signal being proportional to the velocity of scanning, any change in this velocity will produce a black-level error.

The polarity of the focusing coil should be such that a north-seeking pole is attracted to the image end of the focusing coil, with the indicator located outside of and at the image end of the focusing coil.

The alignment coil assembly should be located on the tube so that its centre is at a distance of approx. 94 mm (3 11/16'') from the face of the tube and be positioned so that its axis coincides with the axis of the tube, the deflecting yoke and the focusing coil.

The temperature of the faceplate should never exceed $80 \,^{\circ}$ C, either during operation or storage of the 55850. Operation at a faceplate temperature of 25 to 35° C is recommended.

The effect of the faceplate temperature on sensitivity and dark current of a typical 55850, measured with illumination level and signal-electrode voltage as fixed parameters, is illustrated on page D. 7Z2 5682

EQUIPMENT DESIGN AND OPERATING CONSIDERATIONS (continued)

The temperature of the faceplate is determined by the heating effects of the incident illumination, the associated components, the environmental conditions and to a minor extent by the tube itself.

To reduce these heating effects and to permit operation in the preferred temperature range under conditions of high light levels, respectively high ambient temperatures, the use of an infra-red filter between object and camera lens, or a flow of cooling air directed across the faceplate, is recommended.

As the signal-electrode voltage is increased, the dark current and the sensitivity also increase. See page E.

Signal output and light-transfer characteristics

The typical signal output as a function of a uniform 2870 ^oK tungsten illumination on the photoconductive layer is shown on page F.

The average "gamma" of the light-transfer characteristic is approx. 0.6. This value is relatively constant over a signal output range of 0.01 to 0.3 μ A.

Sufficient uniformity in the value of gamma is maintained to ensure satisfactory performance of colour cameras, in which the signal output currents of three 55850's, with the aud of y-correcting circuitry, must match closely over a wide range of scene illumination.

The spectral response of a typical 55850 is shown on page A.

The resolution capability of the 55850 is illustrated on page B.

In general the resolution decreases with decreasing grid No.3 voltage. The voltage range will depend on the design of the focusing coil, which should be such as to provide a field strength within the range of 36 to 44 Oerstedt. Definition, focus uniformity and picture quality decrease with decreasing grid No.3 and No.4 voltage. In general grid No.3 and grid No.4 should be operated above 250 V.

As shown on pages B and C, a substantial increase in both limiting resolution and amplitude response of the 55850 may be obtained by increasing the operating voltage of grids No.3 and No.4 to 750 V. With this mode of operation, the focusing field strength must be increased to approx. 70 Oerstedt.

Since beam-landing errors increase with increasing grid No.3 and grid No.4 voltage, such operation will show a reduced signal output in the corners of the scanned area. When the 55850 is operated in this manner, the deflecting and focusing coils employed must be designed to eliminate beam-landing errors.

Compensation of beam-landing errors can be obtained by supplying modulating voltages of parabolic shape and of both horizontal and vertical scanning frequencies to the cathode and additionally, in order to prevent beam-modulation, to grid No.1, No.2, No.3 and No.4.

EQUIPMENT DESIGN AND OPERATING CONSIDERATIONS (continued)

A suitable amplitude for this mixed parabolic waveform is approximately 4 V peak-to-peak. The polarity should be chosen such that the potential of the cathode is lowered as the beam approaches the edges of the scanned area. The use of this modulating waveform also improves the centre-to-edge focus of the vidicon.

Care must be taken that identical waveforms are applied to the relevant electrodes of each of the three tubes when using the 55850 in 3-colour vidicon cameras to ensure good registration of all signals over the entire scanned area.

Operation with grid No.3 and grid No.4 voltage at 750 V and a field strength of 70 Oerstedt demands increased-power requirements for the deflecting and focusing coils, which will increase tube temperature unless adequate provisions for cooling are made.

Scanning amplitude

Full-size scanning of the 9.6 mm x 12.8 mm area of the photoconductive layer should always be applied. To obtain this condition, first adjust the deflection circuits to overscan the photoconductive layer sufficiently so that the edges of the sensitive area can just be seen on the monitor, which itself should not be overscanned.

Then, after centring the image on the sensitive area (see Fig.4), reduce the scanning amplitudes in both directions with 15%.

In this way, the maximum signal-to-noise ratio and maximum resolution can be obtained. It should be noted that overscanning of the photoconductive layer produces a picture on the monitor that is smaller than normal.

Underscanning of the photoconductive layer, i.e. scanning of an area of less than 9.6 mm x 12.8 mm or failure of scanning for even the shortest duration should always be avoided, since this may cause permanent damage to the specified full-size area.



Fig.4 Positioning of the image on the sensitive area

7Z2 5684



- A: Spectral sensitivity of 55850 Scanned area = 12.8 mm x 9.6 mm Signal current I_s = 0.02 μ A
- B: Relative spectral sensitivity of the human eye (N).



Horizontal square-wave response in picture centre of a typical 55850.

Highlight signal current = $0.3 \,\mu A$.

Test pattern: transparent square-wave resolution wedge.

| A1: Uncompensated | V_{g_3,g_4} = approx. 285 V, |
|------------------------------|---------------------------------------|
| A ₂ : Compensated | focusing field strength = 40 Oerstedt |
| | |

B: Uncompensated; $V_{g_3,g_4} = 750 \text{ V}$, focusing field strength = approx. 70 Oerstedt



Uncompensated horizontal square-wave response at 400 TV lines as a function of the focusing magnetic field strength of an average 55850.

Curve A: Highlight signal current = $0.1 \,\mu$ A Dark current = $0.02 \,\mu$ A Curve B: Highlight signal current = $0.3 \,\mu$ A Dark current = $0.02 \,\mu$ A



Signal current, dark current and ratio signal current: dark current as a function of the faceplate temperature.

Typical tube

Signal-electrode voltage and illumination level adjusted for a dark current (I_d) of 0.02 μ A and a signal current (I_s) of 0.15 μ A at a faceplate temperature of 30 °C.

D



Signal current and dark current as a function of the signal-electrode voltage.



Average signal current as a function of the illumination on the photoconductive layer.

F



CAMERA TUBE

Vidicon, television camera tube with low heater consumption, magnetic focusing, magnetic deflection and l'' diameter for low-cost industrial cameras, experiments in camera development and for amateur use.

| QUICK | REFERENCE DATA | on concret for |
|------------|----------------|---------------------------|
| Resolution | 600 to 900 | TV lines |
| Focusing | magnetic | |
| Deflection | magnetic | |
| Diameter | 25.4 | mm (1 inch) |
| Length | 158 | mm ($6\frac{1}{4}$ inch) |
| Heater | 6.3 V, 90 | mA |

OPTICAL

Diagonal of quality rectangle on photoconductive layer (aspect ratio 3 : 4)

max. 16 mm

Orientation of image on photoconductive layer:

horizontal scan should be essentially parallel to the straight sides of the masked portions of the faceplate. The masking is for orientation only and does not define the proper scanned area of the photo-conductive layer.

CAPACITANCE

Signal electrode to all

Cas 4.5 pF¹)

¹) This capacitance, which effectively is the output impedance of the tube, is increased by about 3 pF when the tube is inserted into the deflection and focusing coil-assembly. The resistive component of the output impedance is in the order of 100 M Ω . 7Z2 7709

HEATING

Indirect by A.C. or D.C., series or parallel supply

| Heater voltage | V_{f} | 6.3 | V <u>+</u> 10% |
|----------------|---------|-----|----------------|
| Heater current | I_{f} | 90 | mA |

When the tube is used in a series heater chain the heater voltage must not exceed $9.5 V_{rms}$ when the supply is switched on.

MECHANICAL DATA



ACCESSORIES

Socket

Focusing and deflection coil assembly

Cinch No. 54A18088 or equivalent

AT1101, AT1102 or equivalent

7Z2 7710

| LIMITING VALUES (Absolute max. rating syste for scanned area of 9.6 mm x 12.8 mm (3/8" | m) x <u>1</u> '') ¹) | | | |
|---|-------------------------------------|------|------|-------------------|
| Grid No.3 and grid No.4 voltage | Vg3,g4 | max. | 800 | v |
| Grid No.2 voltage | Vg2 | max. | 350 | v |
| Grid No.1 voltage | | | | |
| Negative bias | -v _{g1} | max. | 125 | V |
| Positive bias | +Vg1 | max. | 0 | V |
| Peak heater-cathode voltage | | | | |
| Heater neg. with respect to cathode | V _{kfp} | max. | 125 | V |
| Heater pos. with respect to cathode | Vkfp | max. | 10 | V |
| Signal-electrode voltage | Vas | max. | 100 | V ²) |
| Peak signal-electrode current | Ias p | max. | 0.6 | μA ³) |
| Faceplate illumination | unephy anta | max. | 5000 | lux |
| Faceplate temperature | | max. | 80 | °C ⁴) |
| Dark current, peak | Idp | max. | 0.25 | μA |

 [&]quot;Full-size scanning", i.e. scanning of a 9.6 mm x 12.8 mm area of the photoconductive layer should always be applied. The use of a mask having these dimensions is recommended. Underscanning, i.e. scanning of an area less than 9.6 mm x 12.8 mm may cause permanent damage to the specified fullsize area.

²) The signal-electrode voltage should never exceed 100 V, either during heating-up or stand-by, or during operation. An excessive signal-electrode voltage may cause permanent damage to the photoconductive layer.

³) Video-amplifiers should be capable of handling signal-electrode currents of this magnitude without amplifier overload or picture distortion.

⁴) Absolute maximum for shelf-life and operation. Under difficult environmental conditions a flow of cooling air directed at the faceplate is recommended. When televising flames and furnaces appropriate infra-red filters should be applied. 7Z2 7711

| OPERATING CONDITIONS AND PERFORMAN For scanned area of 9.6mm x 12.8mm and | CE faceplate temperature | of 25-35 ^o C |
|---|--|-------------------------|
| PICK-UP FROM LIMITED-MOTION LIVE SCEI | NES | |
| Conditions | | |
| Grid No.3 and grid No.4 (beam focus electrode) voltage | 250-300 | V ¹) |
| Grid No.2 voltage | 300 | V |
| Grid No.1 voltage adjusted for sufficient beam current to stabilise highlights | e ichode voltage 19. wich responsed to ca | |
| Peak-to-peak blanking voltage | | |
| when applied to grid No.1 | > 75 | Vielange |
| when applied to the cathode | > _ 20 | V ²) |
| Field strength at centre of focusing coil | 40 | Oerstedt ³) |
| Field strength of adjustable alignment coils | 0-4 | Oerstedt ⁴) |
| | | |

 Beam focus is obtained by the combined effect of the grid No.3 voltage, which should be adjustable over the indicated range and a focusing coil having an average field strength of 40 Oerstedt. Definition, focus uniformity and picture quality decrease with decreasing grid No.3 voltage. In general, grid No.3 should be operated above 250 V.

- 2) In transistorized cameras cathode blanking will be preferable. The cathode impedance is in the order of 30 kΩ.
- ³) The polarity of the focusing coil should be such that a north-seeking pole is attracted to the image end of the focusing coil, with the indicator located outside of and at the image end of the focusing coil.
- ⁴) The alignment coil assembly should be located on the tube so that its centre is at a distance of approx. 94 mm (3 11/16") from the face of the tube and be positioned so that its axis coincides with the axis of the tube, the deflecting yoke and the focusing coil. 7Z2 5762

55850AM

OPERATING CONDITIONS AND PERFORMANCE (continued)

Performance

| Signal-electrode voltage for dark current | | | | |
|--|-----------------------------------|------------|------------------|------|
| of 0.02 µA | range | 20 to 100 | V | |
| | typical | 40 | V ¹) | |
| Negative grid No.1 voltage for picture cut-off | | 20-110 | V ²) | |
| Signal output current, faceplate illumination 10 lux | > | 0.075 | μA 3) | |
| Resolution capability in picture centre | > | 600 | lines | 4)5) |
| Decay: 10 lux on layer, V_{as} adjusted for dark current of 0.02 μ A, residual signal after dark pulse of 200 msec | المان ويت المانية إن أنه جا | 20 | % | |
| Average gamma of transfer charac- teristic for signal output currents between 0.01 and 0.3 μ A | (1000) (1000) (≡1007-1 | 0.6 | | |
| Visual equivalent signal-to-noise ratio | | 300:1 | ⁶) | |
| Spurious signals: Shading | | see note 7 | | |
| Spots and blemishes | | see note 8 | | |

- ¹) The deflection circuits must provide sufficiently linear scanning for good black-level reproduction. The dark-current signal being proportional to the velocity of scanning, any change in this velocity will produce a black-level error.
- ²) With no blanking voltage on grid No.1.
- ³) Defined as the component of the signal-electrode current after the dark current has been subtracted.
- 4) With a video-amplifier system having 7.5 Mc/s bandwidth (-3 dB points).
- ⁵) A resolution capability of approx. 900 TV lines can be achieved with the grid No.3 and grid No.4 voltage adjusted to 750 V and a focusing field strength of approx. 70 Oerstedt.

With this mode of operation beam-landing errors, resulting in parabolic shading and dark corners, increase. 7Z2 5761

(Note 5 continued)

The deflecting and focusing coils should be designed to eliminate these errors. Since higher power requirements for these coils will increase the tube temperature, adequate provisions for cooling should be made.

⁶) Measured with a peak signal output current of 0.2μ A into a high-gain,cascodeinput type of amplifier with an own noise of 0.002μ A r.m.s. and a bandwidth of 5 Mc/s. Because the noise in such a system is predominantly of the highfrequency type, the visual equivalent signal-to-noise ratio is taken as the ratio of the highlight video-signal current to the r.m.s. noise current multiplied by a factor of 3.

- ⁷) Target voltage adjusted to obtain a dark current of $0.02 \,\mu$ A. Camera directed towards a uniformly illuminated white background, light level adjusted to produce a signal output current (note 3, page 5) of $0.2 \,\mu$ A. The composite video signal when viewed at horizontal rate on a waveform oscilloscope will fall within an envelope having a width of 50% of the peak signal.
- ⁸) Target voltage adjusted to obtain a dark current of $0.02 \,\mu$ A. Camera focused at a uniformity illuminated two-zone test pattern with the centre zone (1) diameter equal to raster height. Light level adjusted to produce a signal output current of $0.2 \,\mu$ A. Scanning amplitudes of rectangular monitor adjusted to obtain a raster with aspect ratio of 3 : 4. Monitor set-up and contrast control adjusted for faint raster when lens of camera is capped, and for non-blooming bright raster when lens of camera is uncapped.

Under the above conditions number and size of the spots observable in the monitor picture will not exceed the limits stated below:

| Spot size in % | Max. numb | per of spots | To be considered as a black or as a white spot. |
|--|----------------------|----------------------|--|
| of raster height | zone 1 | zone 2 | its contrast ratio must |
| $ > 1 \% \\ 1 - 0.6 \% \\ 0.6 - 0.2 \% \\ < 0.2 \% $ | none 1 4 9) | none 3 6 9) | be greater than 2 to 1. Black spots as well as white ones must be counted as spots. |

9) Do not count spots of this size unless concentration causes a smudgy appearance.

CAMERA TUBE

Vidicon provided with separate mesh intended for industrial, medical and broadcast applications.

| QUI | CK REFERENCE DATA | 0.0 |
|-----------------------------|------------------------------|-----|
| Resolution | up to 1000 TV lines | |
| Focusing | magnetic | |
| Deflection | magnetic | |
| Diameter | 25.4 mm (1 inch) | |
| Length | 158 mm ($6\frac{1}{4}$ inch | 1) |
| Provided with particle trap | | |
| Heater | 55851 6.3 V, 90 mA | |
| | 55852 6.3 V, 300 mA | |

GENERAL

Advantages of vidicons with separate grid No. 4 connection over conventional vidicons like 55850:

- Increased resolution up to 1000 T.V. lines
- Higher amplitude response at 400 T.V. lines
- More uniform resolution over whole picture area
- Stabilisation for peaked highlights possible without appreciable loss in resolution
- 55851 Target properties identical to 55850. Provided with low power heater of 0.6 W, primarily intended for transistorized camera's, in which heat dissipation should be kept at a minimum.
- 55852 Target properties identical to 55850. Provided with 2 W heater.

Both types will be available in 5 grades, namely:

- N for normal industrial applications
- ${\rm S}~$ for industrial and broadcast applications in which a higher picture quality is required
- SR for use in X-ray medical equipment
- F for use in film-scanners
- AM low cost tube for experiments, amateur use etc.

The electrical and mechanical properties of the five grades are essentially identical, main differences being found in the degree of uniformity and freedom of blemishes of the photoconductive layers. 7Z2 7712

TENTATIVE DATA

OPTICAL

Diagonal of quality rectangle on photoconductive layer (aspect ratio 3:4)

max. 16 mm

Orientation of image on photoconductive layer: horizontal scan should be essentially parallel to plane passing through tube axis and short index pin.

Spectral response

See data 55850

HEATING

Indirect by A.C. or D.C.; series or parallel supply

| Heater voltage | | v_{f} | 6.3 | $V \pm 10\%$ |
|----------------|-------|---------|-----|--------------|
| Heater current | 55851 | I_{f} | 90 | mA |
| | 55852 | I_{f} | 300 | mA |

When the tube is used in a series heater chain the heater voltage must not exceed 9.5 $V_{\rm rms}$ when the supply is switched on.

CAPACITANCES

Signal electrode to all

Cas pF 1) 4.5

Dimensions in mm

MECHANICAL DATA



 This capacitance, which effectively is the output impedance, is increased by about 3 pF when the tube is inserted into the deflection and focusing coil assembly. The resistive component of the output impedance is in the order of 100 MΩ.

| | | | 5 | 585 585 | 1 2 |
|------------------------------------|---|--|-----------|------------|-------------------|
| FOCUSING | magnetic | COD PED ORMANES | ion And | 40 JAL | FTT. I |
| DEFLECTION | magnetic | | | | |
| MOUNTING POSI | TION: any | | | | |
| NET WEIGHT | | | app | cox. | 75 g |
| ACCESSORIES | | | | | |
| Socket | | Cinch No. 54A1808 | 8 or equi | valent | |
| Focusing and defl | lection coil assemb | ly: AT1101, AT1102 or | equival | ent | |
| LIMITING VALUE for scanned area | ES (Absolute max. a of 9.6 mm x 12.8 | rating system) 3 mm (³ /8" x ¹ /2") 1) | | | |
| Signal electrode | voltage | v _{as} | max. | 100 | V ²) |
| Grid No.4 voltage | e | vg4 | max. | 1000 | V |
| Grid No.3 voltage | e | Vg3 | max. | 850 | V |
| Grid No.2 voltage | е | Vg2 | max. | 450 | V |
| Grid No.1 voltage | e, negative bias | -Vg1 | max. | 125 | v |
| | positive bias | + V _{g1} | max. | 0 | v |
| Signal electrode o | current, peak | Iasp | max. | 0.6 | μA ³) |
| Faceplate illumin | ation | P - Group | max. | 5000 | lux |
| Faceplate temper | ature | t | max. | 80 | oC 4) |
| Cathode to heater | voltage, peak | | | | |

Dark current, peak

V_{kfp} V_{kfp} cathode positive max. max. cathode negative Idn max. 1) "Full-size scanning", i.e. scanning of a 9.6 mm x 12.8 mm area of the photo-

- conductive layer should always be applied. The use of a mask having these dimensions is recommended. Underscanning, i.e. scanning of an area less than 9.6 mm x 12.8 mm may cause permanent damage to the specified fullsize area.
- 2) The signal electrode voltage should never exceed 100 V, either during heatingup or stand-by, or during operation. An excessive signal electrode voltage may cause permanent damage to the photoconductive layer.
- 3) Video amplifiers should be capable of handling signal-electrode currents of this magnitude without amplifier overload or picture distortion.
- 4) Absolute maximum for shelf-life and operation. Under difficult environmental conditions a flow of cooling air directed at the faceplate is recommended, when televising flames and furnaces appropriate infra-red filters should be applied. 7Z2 7713

125 10 V

0.25 µA

| TYPICAL OPERATION AND | PERFORMANCE | both types | |
|---|---|--|--|
| CONDITIONS | Normal operation | apper in the | Operation for max. resolution |
| Vg4 (mesh) voltage | 265 to 400 V ¹) | 10 A 10 | 575 to 850 V ¹) |
| Vg3 (beam focus) voltage | 250 to 300 V | | 550 to 650 V |
| Vg ₂ voltage | 300 Volts | | 300 Volts |
| V_{g_1} , grid No.1 voltage, adjusted for sufficient beam current to stabilize highlights | en and star and star The contract of the star | ir renilice și | 06.8.3012 68 i amery, and deboot |
| P.t.p. blanking voltage when applied to grid No.1 when applied to cathode | | > 75 Volts > 20 Volts | INTERVE VALUES |
| Field strength at centre of focus-coil | app.40 Oerstedt | 1 | app. 60 Oerstedt ²) |
| Field strength of adjustable alignments coils | 0 - 4 Oerstedt | | 0 - 6 Oerstedt |
| PERFORMANCE | | and see the | |
| Signal-electrode voltage for dark-current of 0.02 µA typical | | 20 - 100 V 45 Volts | |
| Grid No.1 voltage for pic- ture cut-off | | -30 to -100 V | ອີດດີນເຫຼົາ ແລະອອກແກ່ງແລະ. ເ |
| Signal output current, face- plate illumination 8 lux, typical | | 0.15 μΑ | d aprend in the second se |
| Resolution capability in picture centre | 750 T.V. lines ³) | , jagga | 1000 T.V. lines ³) |
| Mod. depth at 400 T.V. lines in picture centre | 50 % ⁴) | | 70 % ⁴) |
| Decay: 8 lux on faceplate, V_{as} adjusted for dark cur- rent of 0.02 μ A, residual signal after dark pulse of | i jalmut o bana internetionalista bana internetionalista | ave, norază 28 daŭ 1729 p. 10. aktore elec | an an a san ann a 11 a mar a Cuiste 11 a mar a san a 11 a mar a san an a |
| 200 msec typical | Research and the second | 10 % | n vo paro do on. |
| Average gamma of transfer characteristics for signal currents between 0.01 and 0.3 μ A | ol, se no na na na Sgriffin e se ska Livij se se slave Independent | 0.6 | anar |
| Visual equivalent S/N ratio | all the restants | app200:1 | wall i mulifinia- |
| | | | 7Z2 7714 |

NOTES

1. Under no circumstances should grid No.4 (field mesh) be allowed to operate at a voltage level below the actual grid No.3, V_{g_3} , level as needed for beam focus, since this may damage the target. Minimum voltage difference between V_{g_4} and V_{g_3} (g4 positive to g3) to produce an attractive gain in resolution: 15 Volts. The optimal voltage of grid No.4 for maximum resolution and optimal uniformity of resolution and white level will depend on the type of coil unit used and will be within the range 1.05 to 1.3 times the actual grid No.3 voltage.

It should be noted that with increasing V_{g_4} voltage also an increase in deflecting power will be needed.

- 2. The higher voltage operation will necessitate an increase in focusing and deflecting power. Provisions should be made for proper cooling of the tube in these increased power conditions.
- 3. With a video amplifier system having flat response to 10 Mc/s.
- 4. Typical values, measured under conditions of peak-signal current $I_s = 0.15 \mu A$ and beam current sufficient to stabilize $0.5 \mu A$ of signal current.



CAMERA TUBE

Plumbicon, sensitive high definition pick-up tube with photoconductive target and low velocity stabilisation.

The 55875 is intended for use in black and white-, the 55875R, G, B for use in colour studio cameras.

| QUIC | CK REFERENCI | E DATA | | |
|--|--------------------|------------|--------|-------------------------------|
| Focusing Deflection Diameter | | | | magnetic magnetic 30 mm |
| OPTICAL | | | | |
| Dimensions of quality rectangle photoconductive layer (aspect | e on ratio 3:4) | 12.0 mm | x 16.0 | mm l |
| Orientation of image on photoco layer | onductive | see note 2 | 2 | |
| Sensitivity at colour temperatu illumination = 2850 °K | re of | | | |
| type: 55875 | | min. | 275 | µA/lumen |
| 55875R | | min. | 60 | μ A/lumen 3 |
| 55875G | | min. | 100 | μ A/lumen ³ |
| 55875B | | min. | 32 | μ A/lumen 3 |
| Gamma of transfercharacterist | ic | 0.95 | ±0.05 | 4 |
| Spectral response; max. response; max. | nse at | approx. | 5000 | A |
| HEATING | | | | |
| Indirect by A.C. or D.C.; para | allel supply | | | |
| Heat | ter voltage | Vf | 6.3 | V ± 5% |
| Heat | ter current | If | 90 | mA |
| 1) ²) ³) ⁴) See page 5 | | | | 7Z2 592 |

12.12.1965

TENTATIVE DATA

1



When indium seal technique is employed, faceplate thickness will be increased to 2.3 mm.

At some date to be indicated by the manufacturer the faceplate thickness maybe increased with a 6 mm glass stud to reduce internal reflections.

MOUNTING POSITION any

WEIGHT

| Net weight | approx. | 100 | g |
|---------------------------------------|---------|---------|-------------------|
| ACCESSORIES | | | |
| Socket | type | 56020 | |
| Focusing and deflection coil assembly | | | |
| for 55875 | type | AT 1132 | |
| for 55875R, G, B | type | AT 1112 | |
| CAPACITANCES | | 1 | |
| Signal electrode to all | Cas | 4 to 6 | pF ⁵) |
| FOCUSING magnetic ⁶) | | | |
| DEFLECTION magnetic by | | | |
| 56 See page 5 | | 7Z | 2 5927 |

| | | | 55875 55875R,G, | | , B |
|--|---|--------------|--------------------|------------------|------------|
| CHAD A CTEDISTICS | seleti solization | | | | |
| | | | | | |
| Grid No.1 voltage for cut-off, at V _{g2} = 300 V | v _{g1} | -30 t | o -100 | v 7) | |
| Blanking voltage, peak to peak on grid No.1 on cathode | Vg _{1p-p} V _{kp-p} | min. min. | 40 15 | v v | |
| Grid No.2 current at normally required beam currents | Ig2 | max. | 1 | mA | |
| Dark current at V_{a_S} = 45 V | I _{as} | max. | 0.003 | μA | |
| LIMITING VALUES (Absolute max. ra | ting system) | | | | |
| Signal electrode voltage | Vas | max. | 50 | V ⁸) | |
| Grid No.4 and No.3 voltage | V_{g_4,g_3} | max. | 750 | V 8) | |
| Grid No.2 voltage | V _{g2} | max. | 450 | V ⁸) | |
| Grid No.1 voltage | | | | | |
| positive | v_{g_1} | max. | 0 | v 8) | |
| negative | -v _{g1} | max. | 125 | V ⁸) | |

Cathode current Ik 3 mA max. Cathode to heater voltage positive peak V+k/f-p 125 max. V negative peak V-k/+fp 10 V max. °C Ambient temperature 50 tamb max. °C -30 (storage and operation) min. Face plate illumination 500 lux 9) max. °C Face plate temperature 50 max. °C (storage and operation) -30 min.

7)8)9) See page 5

7Z2 5928

OPERATING CONDITIONS AND PERFORMANCE

| Cathode voltage | v_k | 0 | V |
|---|-------|---------------------|-------------------|
| Grid No.2 voltage | vg2 | 300 | v |
| Signal electrode voltage | Vas | 15-45 | V ¹⁰) |
| Beam current | Ibeam | See note 11 | |
| Focusing coil current | | See note 12 | |
| Line- resp. frame deflection coil current | | See note 12 | |
| Face-plate illumination | | See notes 13 and 14 | |
| Face plate temperature | t | 20-45 | °C |
| | | | |

Resolution

Modulation depth, i.e. uncompensated horizontal amplitude response at 400 TV lines, in picture centre. See note 15.

| | 55875 | 55875R | 55875G | 55875B | |
|---|-------|--------|--------|--------|----|
| Highlight signal current I _S | 0.3 | 0.15 | 0.3 | 0.15 | μA |
| $V_{g_3}, V_{g_4} = 250 \text{ to } 300 \text{ V}$ See note 16 | 35 | 30 | 35 | 45 | % |
| $V_{g_3}, V_{g_4} = 550 \text{ to } 650 \text{ V}$ See note 16 | 40 | 35 | 40 | 50 | % |

Limiting resolution

Signal to noise ratio 17) at a signal current of 0.15 μ A

TV lines

> 600

approx. 200 : 1

Persistence (or lag)

Low persistence renders tube very suitable

for live studio monochrome and colour applications.

Persistence is basically independent of illumination level.

Decay

Measured with 100% signal current of 0.1 μ A and with a light source with a c.t. of 2850 °K. Appropriate filter inserted in light-path for tubes 55875R, G, B.

Residual signal after dark pulse of 60 msmax.5 %Residual signal after dark pulse of 200 msmax.2 %

10,11,12,13,14,15,16,17) See pages 5 and 6

7Z2 5929

NOTES

 a) Underscanning of the specified useful target-area of 12.0 mm x 16.0 mm or failure of scanning, should be avoided since this may cause damage to the photo-conductive layer.

55875

55875R,G,B

- b) The area beyond the 12.0 mm x 16.0 mm optical image preferably to be covered by a mask to reduce the effects of internal reflections in the faceplate.
- 2. For proper orientation of the image on the photo-conductive layer the vertical scan should be essentially parallel to the plane passing through the tube axis and the mark on the tube base.
- 3. As measured under following conditions:

Tubes are exposed to 5.2 lux illumination of black body colour temperature of 2850 °K. The appropriate filter is inserted in the light path. The signal current obtained in nano-amperes denotes the colour sensitivity expressed in terms of micro-amperes per lumen of white light before the filter. Filters used:

| 55875R | Schott | OG2 | thickness | 3 mm |
|----------|--------|------|-----------|-------|
| 55875G | Schott | VG9 | thickness | 1 mm |
| 55875B | Schott | BG12 | thickness | 3 mm |
| See page | A | | | |

- a) Gamma is, to a certain extent, dependent on the wavelength of the illumination applied.
 - b) The use of gamma-stretching circuitry is recommended.
- 5. Cap. Cas to all, which effectively is the output impedance, increases by approx. 5 pF when the tube is inserted into the deflecting/focusing assembly.
- 6. For focusing/deflection coil assembly, see under "Accessories".
- 7. With no blanking voltage on gl.
- 8. At $V_k = 0 V$.
- 9. For short intervals. During storage and idle periods of camera the tube-face shall be covered with plastic hood provided, respectively lens be capped.
- 10. The signal electrode voltage should be adjusted to 45 V unless otherwise indicated by the tube manufacturer on the test-sheet as delivered with each individual tube.
- 11. The beam current shall be adjusted for correct stabilisation for the highlight signal currents stated in the tabel.

Operation of the tube with beam currents I_b not sufficient to stabilize the brightest highlight picture-elements should be avoided in order to prevent loss of highlight-detail and/or "sticking" effects. Operation at excessively high beam currents will result in loss of resolution. Operation in the high voltage mode will permit the use of beam current of twice the minimum a-mount as needed for stabilisation without appreciable loss of resolution. 7Z2 5930

| 12. Black/white coil assembly AT 113 | 32 focus current | line current mApp | frame current mApp | |
|--------------------------------------|---------------------|-------------------------|--------------------------|--------|
| Vg3,g4 : 300 V | 17 | 160 | 25 | |
| V_{g_3,g_4} : 600 V | 25 | 235 | 35 | |
| Colour coil assembly AT 1112 | | | } | values |
| $V_{g_3,g_4} := 300 V$ | 75 | 160 | 25 | |
| V_{g_3,g_4} : 600 V | 100 | 235 | 35) | |

13. Faceplate illumination level for the 55875 typically needed to produce $0.3 \,\mu\text{A}$ signal current will be approx. 5 lux. The signal currents stated for the colour tubes 55875R, G and B respectively will be obtained with an incident white light-level (2850 °K) on the filter of approx. 12 lux.

These figures are based on the use of the filters described in note 3, for filter BG12 however a thickness of 1 mm is chosen.

14. Illumination on the photo-conductive layer, B_{ph} , in the case of a black/white camera is related to scene-illumination, B_{SC} , by the formula:

$$B_{ph} = B_{sc} \frac{R.T.}{4F^2 (m+1)^2}$$

in which R represents the scene-reflexivity (average or the object under consideration, whichever is relevant), T the lens transmission factor, F the lens aperture and m the linear magnification from scene to target.

A similar formula may be derived for the illumination level on the photoconductive layers of the respective R, G, and B tubes in which the effects of the various components of the complete optical system have been taken into account.

- 15. The figures shown represent the typical horizontal amplitude responses of the tubes proper after correction for faults introduced by the optical system. Horizontal amplitude response can be raised by the application of suitable correction circuits. Such compensation, however, does not affect vertical resolution, nor does it influence the limiting resolution.
- 16. Grid No.3 and No.4 voltage adjusted for optimum focus. See also note 12.
- 17. The stated ratio represents the "visual equivalent signal-to-noise ratio", which is taken as the ratio of highlight vidio-signal current to R.M.S. noise-current, multiplied by a factor of 3. (Assuming an R.M.S. noise-current of the video pre-amplifier of 2.10^{-9} A, bandwidth 5 Mc/s).

GENERAL RECOMMENDATIONS AND INSTRUCTIONS FOR USE

TRANSPORT, HANDLING, STORAGE

During transport, handling or storage the longitudinal axis must either be in a horizontal position or be kept vertically with the face-plate of the tube up.

GENERAL

- 1. Signal-electrode connection is made by a suitable spring-contact, executed as part of the focusing coil, against the metallic coating at the face end of the tube.
- 2. Electrostatic shielding of the signal-electrode is required in order to avoid interference effects in the picture. Effective shielding is provided by ground-ing shields on the inside of the face-plate end of the focusing coil and on the inside of the deflecting yoke.
- 3. The Plumbicon as described in these data has been provided with tungsten base pins. It is recommended to avoid mechanical force and shocks to these pins and to insert the tube into its socket, type 56020, with care.
- 4. In some cases the properties of the photo-conductive layer as used in the Plumbicon maybe found to have slightly deteriorated during long idle periods, such as encountered between the last test in our works and actual delivery to the user.

It is therefore recommended to operate the tube directly after receipt under normal voltage settings, in overscanned position with evenly illuminated target and a signal current of $0.15 \,\mu\text{A}$ for some hours after which the initial properties will have been fully restored.

5. The light-transfer characteristic of the Plumbicon being characterized by a gamma near unity, it may be desirable for broadcast applications to incorporate a gamma correcting circuitry in the video-amplifier system with an adjustable gamma of 0.5 to 1.

It is suggested to design this gamma correcting circuitry such that an extra compression can be introduced by manual control in the video signal range of 75 to 100% of normal peak white level.

This provision will prevent the video amplifier system from becoming overloaded when the Plumbicon with its near unity gamma transfer-characteristic is exposed to scenes containing small peaked highlights as caused by reflections of shiny objects.

6. The Plumbicon not generating own noise to any noticeable extent, the signal to noise ratio will mainly be determined by the entrance noise of the video amplifier system.

The high sensitivity of the Plumbicon warrants pictures with excellent signal-to-noise ratio under normal studio lighting conditions provided its output is fed into a well-designed input stage of the video-amplifier system. In such a system an aperture correction may be incorporated to ensure an attractive gain in resolving power without visually impairing the signal-to-noise ratio. 7Z2 5932

INSTRUCTIONS FOR USE

- 1. Insert the tube in the deflection unit in such a way that the mark at the base of the tube is uppermost.
- 2. Clean the face-plate of the tube and press the socket gently onto the basepins.
- 3. Cap lens and close iris.
- 4. Set: a) Grid No.1 basis-control at max. negative bias (beam cut-off)
 - b) Signal electrode voltage to the value as indicated on the tube's test sheet.
 - c) Scanning amplitudes to max. scan.
- 5. Switch on camera equipment and monitor, allow a few minutes for heatingup.
- 6. Adjust monitor to produce a faint non overscanned raster.
- 7. Direct camera to the scene to be televised and uncap lens.
- 8. Turn grid No.1 bias-control slowly till a picture is produced on the monitor. If the picture is too faint, increase lens aperture.
- 9. Adjust grid No.3 and grid No.4 voltage control (beam focus) and optical focus alternately for max. focus.
- 10. Align the beam of the Plumbicon by either of the two following methods:
 - a) Adjust the alignment fields in such a way that the centre of the picture on the monitor does not move when grid No.3 and No.4 voltage (beam focus) is varied.
 - b) Reduce signal-electrode potential to a few tenths of a volt only. Adjust alignment fields till most uniform picture is obtained as observed on monitor or waveform oscilloscope.
- 11. Adjust scanning amplitudes:
 - a) By means of a mask of 12.0 mm x 16.0 mm, which is in contact with and centred at the face-plate. Decrease horizontal and vertical deflecting currents till the periphery of this mask is just outside the raster on the monitor. This procedure may be facilitated by small adjustments of the centring controls.
11. b) If no mask available direct the camera to a test chart having correct aspect ratio of 3 : 4 and adjust the centring controls in such a way that the target ring is just visible in the corners of the picture.



Adjust distance from camera to test chart and optical focus alternately till the picture of the test chart positioned on the faceplate as indicated on the adjoining figure.

55875

55875R,G,B

Decrease both scanning amplitudes till the picture of the test chart completely fills the scanned raster on the monitor.

- 12. Adjust iris for a picture of sufficient contrast and adjust the beam current to such a value that all highlights are stabilized.
- 13. Check alignment, beam focus and optical focus.

ALWAYS:

- use full size (12.0 x 16.0 mm) scanning of the target and avoid underscanning.
- adjust sufficient beam current to stabilize the picture highlights.
- make sure that the deflection circuits are operative before adjusting beam current.
- avoid focusing camera directly to the sun.
- keep lens capped when transporting camera.

7Z2 5934

55875 55875R,G,B

7Z04209-eehge 1 Transmission 80 OG 2 0.6 BG 12-VG 9 0.4 0.2 0 600 700 Wavelength (nm) 400 500 700

A

CAMERA TUBE

Plumbicon, pick-up tube with photoconductive target and low velocity stabilisation exclusively intended for use with X-ray image intensifier in medical equipment.

| QUICK REFERENCE DATA | | | | |
|----------------------|-------|--|----------|--|
| Focusing | * | | magnetic | |
| Deflection | | | magnetic | |
| Diameter | | | 30 mm | |

OPTICAL

Image dimensions on photoconductive layercircle of 17.0 mm diameter 1)²)Sensitivity, measured with a fluorescent
light source having P20 distributionmin.175 μ A/lumenGamma of transfer characteristic0.9 \pm 0.13)Spectral response, region of max. response4300 to 5200 A

HEATING

Indirect by A.C. or D.C.; parallel supply

| Heater voltage | Vf | 6.3 | $V \pm 10\%$ |
|----------------|---------|-----|--------------|
| Heater current | I_{f} | 90 | mA |

- 1) All underscanning of the specified useful target-area of 17.0 mm diameter or failure of scanning, for even the shortest duration, should be carefully avoided, since this may cause permanent damage to the photoconductive layer.
- 2) The area beyond the 17.0 mm circular optical image preferably to be covered by a mask.
- 3) The near unity gamma of the 55876 ensures good contrast when televising low contrast X-ray image-intensifier pictures as encountered in radiology. Further contrast improvement may be obtained when an adjustable gamma expansion circuitry is incorporated in the video amplifier system.

7Z2 5666

TENTATIVE DATA

CAPACITANCES

Signal electrode to all

MECHANICAL DATA

Cas 4 to 6 pF 1)

Dimensions in mm



When Indium seal technique is used, face plate thickness will be increased to 2.3 mm

| FOCUSING | magnetic | | |
|----------------------------|--------------|---|---------|
| DEFLECTION | magnetic | × | |
| MOUNTING POSITION | any | | |
| ACCESSORIES | | | |
| Socket | | | type |
| Focusing and deflection co | oil assembly | | type |
| NET WEIGHT | | | approx. |

1) Cap. as-rest, which effectively is the output impedance, increases by approx. 5 pF when the tube is inserted into the deflection/focusing coilassembly. 7Z2 5667

56020 AT1122

100 g

TOOLIGING

CHARACTERISTICS

| Grid No. | 1 voltage for cut-off | | | | |
|--------------|----------------------------|--------------------|-------|----------|------------------|
| at V_{g_2} | = 300 V | v _{g1} | -30 t | o -100 | V 1) |
| Blanking | voltage, peak to peak | | | -a 1 - 4 | 1 in |
| on grid | No.1 | Vg _{1p-p} | min. | 40 | V |
| on cathe | ode | V _{kp-p} | min. | 15 | V |
| Grid No. | 2 current at normally | | | | |
| require | d beam current | Ig ₂ | max. | 1 | mA |
| Dark cur | rent | I _{as} | max. | 0.003 | μA 2) |
| IIMITIN | C VALUES (Absolute max ra | ting system) | | | |
| | S VALUES (IDSolute max. 14 | tring system; | | 50 | |
| Signal ele | ectrode voltage | v _{as} | max. | 50 | V -) |
| Grid No. | 4 and grid No.3 voltage | v_{g_4}, v_{g_3} | max. | 750 | V 3) |
| Grid No. | 2 voltage | v_{g_2} | max. | 450 | v ³) |
| Grid No. | 1 voltage | | | | 1.1.1 |
| | positive | Vg ₁ | max. | 0 | V ³) |
| | negative | $-v_{g_1}$ | max. | . 125 | v ³) |
| Cathode | current | Ik | max. | 3 | mA |
| Cathode t | to heater voltage | | | | |
| | positive peak | V _{kfp} | max. | 125 | V |
| | negative peak | V _{kfp} | max. | 10 | v |
| Ambient | temperature | | max | 50 | °C |
| • (storag | e and operation) | tamb | min. | -30 | oC |
| Face-pla | te illumination | | max. | 100 | lux |
| Face-pla | te temperature | | mar | 50 | 00 |
| (storag | e and operation) | • t | min | -30 | °C |
| | | | min. | 00 | - |

 1) With no blanking voltage on g $_{1}$

2) The target voltage should be adjusted to the value indicated by the tube manufacturer on the test sheet as delivered with each individual tube.

3) At $V_k = 0$ V

7Z2 5668

OPERATING CONDITIONS AND PERFORMANCE

| Cathode voltage | Vk | 0 V |
|------------------------------------|------------------------------|---------------------|
| Grid No.2 voltage | Vg ₂ 30 | 0 V |
| Grid No.4 and grid No.3 voltage | V_{g_4}, V_{g_3} 250 to 30 | 0 V ¹) |
| Signal electrode voltage | V _{as} 15 to 4 | 5 V ²) |
| Beam current | I _{beam} See note | 3 |
| Focusing coil current | 17 mA (AT1122 |) |
| Highlight signal electrode current | I _{as} 0.1 to 0. | 6 μA ⁴) |
| Average signal output | approx. 0.0 | 6 μA ⁴) |
| Face-plate temperature | t 25 to 4 | .0 ^o C |
| Face-plate illumination | approx. | 2 lux 5) |
| | | |

- I) Grid No.4 and No.3 voltage adjusted for optimum picture focus. Preferred focus-coil current approx. 17 mA.
- 2) The target voltage should be adjusted to the value indicated by the tube manufacturer on the test sheet as delivered with each individual tube.
- 3) Operation of the tube with beam currents I_b not sufficient to stabilize the brightest highlight picture elements must be carefully avoided in order to prevent loss of highlight-detail and/or "sticking" effects.
 - Operation at excessively high beam currents will result in loss of resolution.
- Substraction of dark current is unnecessary because of the extremely small value.
- 5) Illumination on the photoconductive layer, B_{ph}, is related to scene-illumination, B_{sc}, by the formula:

$$B_{ph} = B_{sc} \frac{R.T.}{4.F^2.(m+1)^2}$$

in which R represents the scene-reflexivity (average or of the object under consideration, whichever is relevant), T the lens transmissionfactor, F the lens aperture and m the linear magnification from scene to target. 7Z2 5669

%²)

10 %

30

OPERATING CONDITIONS AND PERFORMANCE (continued)

Resolution

Modulation depth, i.e. uncompensated horizontal amplitude response (see note 1) at 5 Mc/s in picture centre (625 lines, 50 fields system)

Signal to noise ratio at a signal current of $0.15 \,\mu A$

Persistence (or lag)

Low persistence renders tube very suitable for medical X-ray applications in combination with X-ray image intensifier Persistence is basically independent of illu-

mination level

Decay

Measured with 100% video signal current of $0.1\,\mu\text{A}$ to zero signal after 5 s peak video signal. Fluorescent light source having P20 distribution.

Residual signal after dark pulse of 100 ms Residual signal after dark pulse of 500 ms approx. 200 : 1

max. 1 %

max.

¹) With a signal current of 0.10 μ A and a beam current of 0.20 μ A.

- 2) Horizontal amplitude response can be raised by the application of suitable phase-and-aperture correction circuits. Such compensation, however, does not affect vertical resolution, nor does.it influence the limiting resolution.
- 3) The specified ratio represents the "visual equivalent signal-to-noise ratio", which is taken as the ratio of highlight video-signal current to R.M.S. noise-current, multiplied by a factor of 3. (Assuming an R.M.S. noise-current of the video pre-amplifier of 2.10⁻⁹ A, bandwidth 5 Mc/s.)

GENERAL RECOMMENDATIONS AND INSTRUCTIONS FOR USE

MOUNTING, WORKING POSITION:

1. Any

2. During transport, handling or storage the longitudinal axis must either be in a horizontal position or be kept vertically with the face-plate of the tube up.

GENERAL

- 1. Signal-electrode connection is made by a suitable spring-contact which is executed as part of the focusing coil.
- 2. Electrostatic shielding of the signal-electrode is required in order to avoid interference effects in the picture. Effective shielding is provided by grounding shields on the inside of the face-plate end of the focusing coil and on the inside of the deflecting yoke.
- 3. The Plumbicon as described in these data has been provided with tungsten base pins. It is recommended to avoid mechanical force and shocks to these pins and to insert the tube into its socket with care.
- 4. In some cases the properties of the photoconductive layer as used in the Plumbicon may be found to have slightly deteriorated during long idle periods, such as encountered between the last test in our works and actual delivery to the user.

It is therefore recommended to operate the tube directly after receipt under normal voltage settings, in overscanned position with evenly illuminated target and a signal current of $0.15 \,\mu\text{A}$ for some hours after which the initial properties will have been fully restored.

5. The Plumbicon not generating own noise to any noticeable extent, the signal to noise ratio will mainly be determined by the entrance noise of the video amplifier system.

The high sensitivity of the Plumbicon warrants pictures with excellent signalto-noise ratio, provided its output is fed into a well-designed input stage of the video-amplifier system. In such a system an aperture correction may be incorporated to ensure an attractive gain in resolving power without impairing the visual signal-to-noise ratio.

INSTRUCTIONS FOR USE

- 1. Clean face-plate.
- 2. Insert tube into deflection unit.
- 3. Place mask with 17.0 mm diameter aperture in front of and in close contact with face-plate.
- 4. Press socket gently onto the base pins.
- 5. Set a) grid No.1 bias control at max. neg. bias (beam cut-off)
 - b) signal electrode voltage at zero volts
 - c) scanning amplitudes to max. scan.
- 6. Switch on camera equipment and monitor and allow to heat up for a minimum of 30 seconds.
- 7. Adjust monitor to produce a faint non overscanned raster.
- 8. Remove camerahead from image-intensifier unit.
- 9. Direct camera to lightbox or place suitable lightbox on objective holder. Switch on light and adjust illumination level to correspond to appr. 0.3 ft.cdl for the whites of the testchart on the face-plate.
- 10. Adjust signal-electrode voltage to the value as indicated on the tube's test-sheet.
- 11. Turn grid No.1 control slowly till a picture is produced on the monitor, increase beam-current in order to fully discharge the picture highlights.
- 12. Adjust grid No.3 and grid No.4 voltage control (beam focus) and optical focus for best picture detail.
- 13. Align the beam of the plumbicon by either of the two following methods:
 - A) Adjust the alignment fields in such a way that the centre of the picture on the monitor does not move when grid No.3 and No.4 voltage (beam focus) is varied.
 - B) Reduce signal-electrode potential to a few tenths of a volt only. Adjust alignment field till most uniform picture is obtained as observed on monitor or waveform oscilloscope. Restore signal-electrode voltage to value as indicated on the tube's testsheet.
- 14. Decrease scanning amplitudes till perfect circular picture is produced on monitor, with diameter equal to height of monitor raster. This procedure may be facilitated by small adjustment of the vertical centring control. Adjust horizontal centring control till circular picture is properly centred at centre of monitor raster.
- 15. Remove lightbox and attach camera head to image intensifier unit.
- Place suitable image-intensifier testchart in front of image-intensifier. Switch on image-intensifier and X-ray source.
- 17. Adjust optical focus and beam focus for max. picture detail.

7Z2 5672

ALWAYS:

- keep face-plate capped during transport and shelf-life
- avoid underscanning
- apply sufficient beam current to stabilize picture whites
- make certain that the deflection circuits are operative before applying beam current
- avoid focusing camera head directly to the sun or to reflecting objects
- keep lens capped when transporting camera head

Photo tubes



PHOTOTUBES APPLICATION DIRECTIONS

1. GENERAL

1.1 <u>Photo tubes</u> are photo-electric devices of the emissive type, as distinct from the barrier-layer and photo-conductive cells. They may be divided into two groups:

1. High-vacuum photo tubes,

2. Gas-filled photo tubes

Each of these groups can be subdivided into red sensitive and blue sensitive photo tubes; the spectral response depending upon the photocathode material. For the blue sensitive photo tubes the "A" type of cathode is used (caesium-antimony).

For the red sensitive photo tubes the "C" type of cathode is used (caesium-oxidised silver).

Spectral response curves for each type of cathode are given at the end of these recommendations.

2. OPERATING CHARACTERISTICS

For a vacuum photo tube, the anode current for a fixed quantity of light, is reasonably constant at anode voltages above a certain low value known as the "saturation voltage".

The gas-filled photo tube contains a quantity of inert gas, the ionising potential of which is generally somewhat higher than the saturation voltage of an equivalent vacuum photo tube so that the anode current is substantially constant between the saturation voltage and the voltage at which ionisation commences. Above this voltage range, ionisation increases, resulting in a progressive increase in anode current.

Since a gas-filled photo tube operates at a higher voltage than the ionising potential it will have a greater sensitivity than a similar vacuum photo tube. Within the operating ranges of both groups of photo tubes the anode current is directly proportional to the quantity of light incident on the cathode surface.

2.1 <u>Luminous sensitivity</u>. The response of a photo tube to light falling on its cathode is termed its <u>luminous sensitivity</u>; this is expressed in micro-amperes per lumen.

The sensitivity of all types is dependent upon the colour temperature of the light source and in some cases upon the portion of the cathode that is illuminated.

The sensitivity of gas-filled photo tubes moreover is dependent upon the anode voltage; the sensitivity of vacuum photo tubes in the "saturation region" in which region the tube mainly operates, is practically independent of the anode voltage.

Unless otherwise stated, the values given in the data sheets have been obtained by illuminating the total useful cathode area with an incandescent la_{inp} having a colour temperature of 2700 ^oK.

The values given for sensitivity on the data sheets are the initial values for average photo tubes. The ratio between the maximum and minimum initial sensitivity of photo tubes of a given type will not exceed 3 to 1.

- 2.2 Dark current. This is the current which flows between photocathode and anode when the photo tube is in total darkness. The tube is in total darkness when no radiation within the spectral sensitivity curve of the photocathode is present. This current is caused mainly by electrical leakage and thermionic emission from the photocathode and will therefore increase with temperature and voltage.
- 2.3 <u>Frequency response</u>. The sensitivity of a vacuum photo tube is constant for frequencies of light modulation up to those generally met in practice. Only at very high frequencies, at which transit time limitations occur, the sensitivity becomes dependent upon the frequency.

The sensitivity of gas-filled photo tubes, however, decreases with the frequency. At a frequency of 15000 Hz this decrease is about 3 dB, as is shown in the accompanying curve.

3. THERMAL DATA

Ambient temperature. The temperature of the photocathode may not be too high otherwise evaporation of the emissive cathode layer may result, with consequent reduction in sensitivity and life. As it is difficult to measure this temperature a limiting value for the ambient temperature is given on the published data sheets.

It must be considered, however, that even in case the ambient temperature in the immediate vicinity of the photo tube is not beyond the limit, an excessive temperature rise of the photocathode can be caused e.g. by infrared heat radiation. If the possibility of this radiation exists, a suitable filter should be inserted in the optical path to minimize this effect.

4. OPERATIONAL NOTES

<u>Stability during life</u>. Where a gas-filled photo tube is continuously operated at its maximum rated voltage its sensitivity may fall by as much as 50%, during 500 hours.

Vacuum photo tubes on the other hand are inherently more stable.

The stability of both types of photo tubes will be improved if the current density of the photocathode is reduced (e.g. by reducing the incident light or enlarging the illuminated area of the photocathode).

Particularly in the case of gas-filled photo tubes reduction of the anode voltage will improve the stability.

Also in the inoperative periods photo tubes must not be exposed to strong radiation such as direct sunlight.

A loss of sensitivity of both vacuum and gas-filled photo tubes during operation will be wholly or partially restored during the inoperative periods.

Prevention of glow discharge. Gas-filled photo tubes must not be operated above the published maximum voltage since a glow discharge, indicated by a faint blue glow in the bulb, may occur which adversely affects the good operation of the photo tube and even can result in rapid destruction of the photo-cathode. If accidental over-running can be expected the anode resistance should have a value of at least 0.1 M Ω .

Where it is necessary to use the maximum operating voltage a stabilized supply is recommended.

5. MOUNTING

If no restrictions are made on the individual published data sheets photo tubes may be mounted in any position.

6. STORAGE

It is necessary that phototubes be always stored in the dark.

7. LIMITING VALUES

The limiting values of photo tubes are given in the absolute max. rating system.

8. OUTLINE DIMENSIONS

The outline dimensions are given in mm.

7Z2 5203



Relative spectral response curve type C



Frequency response curve



LIST OF SYMBOLS

| Supply voltage | V _b |
|-------------------------------|----------------|
| Cathode current | Ik |
| Anode series resistance | R _a |
| Sensitivity | N |
| Capacitance, anode to cathode | Cak |
| Ambient temperature | tamb |
| Envelope temperature | tenv |
| | |



58CG

GAS FILLED PHOTOTUBE

Gas-filled phototube particularly sensitive to incandescent light sources, and to near infra-red radiation.

| QUICK REFERENCE DATA | | | | | |
|-------------------------|----------------|------------|--------|----------|--|
| Anode supply voltage | v _b | max. | 90 | v | |
| Luminous sensitivity | N | | 100 | µA/lumen | |
| Spectral response curve | | type C | | | |
| Outline dimensions | | max. 16 di | a.x 30 | mm | |

MECHANICAL DATA



The arrows show the direction of the incident radiation

Photocathode

Surface

Projected sensitive area

Caesium on oxidised silver 1.1 cm^2

Dimensions in mm



2) Black

³) Sensitive cathode area shown shaded

7Z2 5205

OBSOLESCENT TYPE

58CG

ELECTRICAL DATA

| Operating characteristics | | | | |
|--|-------------------|------|-----|----------|
| Anode supply voltage | Vb | | 85 | V |
| Anode series resistor | Ra | | 1 | MΩ |
| Luminous sensitivity measured with the whole cathode area illuminated by a lamp of colour temperature 2700 ^o K | N | | 100 | µA/lumen |
| Dark current | I _{dark} | max. | 0.1 | μA |
| Capacitance | | | | |
| Anode to cathode | Cak | | 3.0 | pF |
| LIMITING VALUES (Absolute max. rating syste | em) | | | |
| Anode supply voltage | Vb | max. | 90 | V |
| Cathode current | Ik | max. | 1.5 | μA |
| Ambient temperature | tamb | max. | 100 | °C |
| | | | | |

58CV

VACUUM PHOTOTUBE

Vacuum phototube particularly sensitive to incandescent light sources, and to near infra-red radiation

| OUTON DEFEDENCE DATA | | | | | |
|-------------------------|----|--------------|------|----------|--|
| Anode supply voltage | Vb | max. | 250 | V | |
| Luminous sensitivity | Ν | | 20 | µA/lumen | |
| Spectral response curve | | type C | | | |
| Outline dimensions | | max. 16 dia. | x 30 | mm | |

MECHANICAL DATA





The arrows show the direction of the incident radiation

Photocathode

Surface

Projected sensitive area

Ceasium on oxidised silver

Dimensions in mm

1.1 cm²

1) Red

²) Black

 3) Sensitive cathode area shown shaded

7Z2 5207

1.1.1967

OBSOLESCENT TYPE

58CV

ELECTRICAL DATA

| Operating characteristics | | | | |
|---|-------------------|------|------|----------|
| Anode supply voltage | Vb | | 50 | V |
| Anode series resistor | Ra | | 1 | MΩ |
| Luminous sensitivity measured with the whole cathode illuminated by a lamp of | | | | |
| colour temperature 2700 ^o K | Ν | | 20 | µA/lumen |
| Dark current (at $V_a = 100 V$) | I _{dark} | max. | 0.05 | μA |
| Capacitance | | | | |
| Anode to cathode | C_{ak} | | 3.0 | pF |
| | | | | |
| LIMITING VALUES (Absolute max. rating syst | em) | | | |
| Anode supply voltage | Vb | max. | 250 | V |
| Cathode current | Ik | max. | 3 | μΑ |
| Ambient temperature | tamb | max. | 100 | °C |

90AV

VACUUM PHOTOTUBE

Vacuum phototube, particularly sensitive to daylight and to light radiation with a blue predominance.

| OUICK REFERENCE DATA | | | | | | |
|-------------------------|----------------|------|--------------|----------|--|--|
| Anode supply voltage | V _b | max. | 100 | v | | |
| Luminous sensitivity | N | | 45 | µA/lumen | | |
| Spectral response curve | | type | A | | | |
| Outline dimensions | | max. | 19 dia. x 54 | mm | | |

MECHANICAL DATA

Dimensions in mm

Base: Miniature



The arrows show the direction of the incident radiation

The cathode connection should be made to pins 1, 2, 6 and 7 connected together and the anode connection to pins 3, 4 and 5 together

Photo cathode

Surface

caesium antimony

Projected sensitive area

 4 cm^2

7Z2 5209

MAINTENANCE TYPE

90AV

ELECTRICAL DATA

| Operating characteristics | | | |
|--|-------------------|-----------|----------------|
| Anode supply voltage | v _b | 100 | V |
| Anode series resistor | Ra | 1 | MΩ |
| Luminous sensitivity measured with the whole cathode area illuminated by a lamp of colour temperature 2700 ^o K | N | 45 | µA/lumen |
| Dark current | I _{dark} | max. 0.05 | μA |
| Capacitance | | | |
| Anode to cathode | Cak | 0.7 | pF |
| LIMITING VALUES (Absolute max. rating sys | tem) | | a Ana |
| Anode supply voltage | Vb | max. 100 | V |
| Cathode current | Ik | max. 5 | μA |
| Ambient temperature | tamb | max. 70 | °C |
| 5 <i>I₀ (µA) 4 3</i> | | 0.051 | 7203522-ij.122 |

7Z2 8020

120 Vg (V) 140

90CG

Dimensions in mm

GAS FILLED PHOTOTUBE

Gas filled phototube particularly sensitive to incandescent light sources, and to near infra-red radiation.

| QUICK REFERENCE DATA | | | | | |
|-------------------------|----|----------------|-----|----------|--|
| Anode supply voltage | Vb | max. | 90 | v | |
| Luminous sensitivity | Ν |] | 125 | µA/lumen | |
| Spectral response curve | | type C | | | |
| Outline dimensions | | max. 19 dia. x | 54 | mm | |

MECHANICAL DATA

Base: Miniature



The arrows show the direction of the incident radiation

The cathode connection should be made to pins 1, 2, 6 and 7 connected together and the anode connection to pins 3, 4 and 5 connected together.

Photocathode

Surface

Projected sensitive area

Caesium on oxidized silver 3.1 cm^2

7Z2 5211

90CG

ELECTRICAL DATA

| Operating characteristics | | | | |
|---|-------|------|-----|----------|
| Anode supply voltage | Vb | | 90 | V |
| Anode series resistor | Ra | | 1 | MΩ |
| Luminous sensitivity measured with the whole cathode area illuminated by a lamp of colour temperature 2700 ^o K | N | | 125 | µA/lumen |
| Dark current | Idark | max. | 0.1 | μA |
| Capacitance | | | | |
| Anode to cathode | Cak | | 1.1 | pF |
| LIMITING VALUES (Absolute max. rating sys | tem) | | | |
| Anode supply voltage | v_b | max. | 90 | V |
| Cathode current | Ik | max. | 2.0 | μA |
| Ambient temperature | tamb | max. | 100 | °C |
| | | | | |



90CV

VACUUM PHOTOTUBE

Vacuum phototube, particularly sensitive to incandescent light sources, and to near infra-red radiation.

| QUICK REFERENCE DATA | | | | | |
|-------------------------|----|------------|----------|----------|--|
| Anode supply voltage | Vb | max. | 250 | V | |
| Luminous sensitivity | Ν | | 20 | µA/lumen | |
| Spectral response curve | | type C | | | |
| Outline dimensions | | max. 19 di | ia. x 54 | mm | |

MECHANICAL DATA

Dimensions in mm

Base: Miniature



The arrows show the direction of the incident radiation.

The cathode connection should be made to pins 1, 2, 6 and 7 connected together and the anode connection to pins 3, 4 and 5 connected together.

 3.0 cm^2

Photo cathode

Surface

Ceasium on oxidised silver

Projected sensitive area

7Z2 5213

90CV

ELECTRICAL DATA

| Operating characteristics | | | | |
|--|------------------|------|------|----------------|
| Anode supply voltage | Vb | | 50 | V |
| Anode series resistor | Ra | | 1 | MΩ |
| Luminous sensitivity measured with the whole cathode area illuminated by a lamp of colour temperature 2700 ^O K | N | | 20 | µA/lumen |
| Dark current (at V _a = 100 V) | Idark | max. | 0.05 | μΑ |
| Capacitance | | | | |
| Anode to cathode | Cak | | 0.8 | pF |
| LIMITING VALUES (Absolute max. rating syst | em) | | | |
| Anode supply voltage | v _b | max. | 250 | v |
| Cathode current | Ik | max. | 10 | μA |
| Ambient temperature | t _{amb} | max. | 100 | °C |
| $I_{a} $ (μA) | | | | 720352 |
| 15 | | | | <i>S-ij 3.</i> |
| | | | | 32 |
| | | | | |
| 10 | | | | |
| | | | | 0.4 7 |
| | | | | |
| 5 | | | | |
| | | | | 0.21 |
| | | | | 0.11 |
| | | | | 0.057 |
| | | | | 0.051 |

92AG

Dimensions in mm

GAS FILLED PHOTOTUBE

Gas-filled phototube particularly sensitive to daylight and to radiation having a blue predominance.

| QUICK | REFERENC | E DATA | | tor con And |
|-------------------------|----------|-----------|----------|-------------|
| Anode supply voltage | Vb | max. | 90 | V |
| Luminous sensitivity | N | | 130 | µA/lumen |
| Spectral response curve | | type A | | |
| Outline dimensions | | max. 19 d | ia. x 54 | mm |

MECHANICAL DATA

Base: Miniature



The arrows show the direction of the incident radiation

The cathode connection should be made to pins 1, 2, 6 and 7 connected together and the anode connection to pins 3, 4 and 5 connected together.

Photocathode

Surface

Caesium antimony

Projected sensitive area

2.1 cm²

92AG

ELECTRICAL DATA

| Operating characteristics | | | |
|--|---|-----------------------|--|
| Anode supply voltage | v _b | 85 | V |
| Anode series resistor | Ra | 1 | MΩ |
| Luminous sensitivity measured with the whole cathode area illuminated by a lamp of colour temperature 2700 $^{\rm O}{\rm K}$ | N | 130 | µA/lumen |
| Dark current | Idark | max. 0.1 | μΑ |
| Capacitance | | | |
| Anode to cathode | Cak | 0.9 | pF |
| LIMITING VALUES (Absolute max. rating sys Anode supply voltage Cathode current | stem) V _b I _k | max. 90 max. 0.012 | V 5 μA/mm ² |
| Ambient temperature | tamb | | 2025 lm 2025 lm 2022 lm 2022 lm 2022 lm 2021 lm 2015 lm 2011 lm |

0.005lm

Va (V)

80

20

40

92AV

VACUUM PHOTOTUBE

Vacuum phototube particularly sensitive to daylight and to light radiation with a blue predominance.

| QUICK REFERENCE DATA | | | | | |
|-------------------------|------|-------------------|----------|--|--|
| Anode supply voltage | Vb | max. 100 | V | | |
| Luminous sensitivity | Ν | 45 | µA/lumen | | |
| Spectral response curve | | type A | | | |
| Outline dimensions | 1111 | max. 19 dia. x 54 | mm | | |

MECHANICAL DATA

a

k.s(2

k.s

Base: Miniature



7Z03531

max 8.5-

The arrows show the direction of the incident radiation.

7203530

The cathode connection should be made to pins 1, 2, 6 and 7 connected together and the anode connection to pins 3, 4 and 5 connected together.

a

6) k.s

5

Photocathode

Surface

Projected sensitive area

caesium antimony 2.1 cm²

Dimensions in mm

7Z2 5217

ELECTRICAL DATA

| Operating | characteristics |
|-----------|-----------------|
|-----------|-----------------|

| Anode supply voltage | V _b | 85 | V |
|---|---------------------|----------|-----------------------|
| Anode series resistor | R _a | 1 | MΩ |
| Luminous sensitivity measured with the whole cathode area illuminated | | | |
| by a lamp of colour temperature 2700 ^O K | Ν | 45 | µA/lumen |
| Dark current | I _{dark} m | ax. 0.05 | μA |
| Capacitance | | | |
| Anode to cathode | Cak | 0.9 | pF |
| LIMITING VALUES (Absolute max. ratin | g system) | | |
| Anode supply voltage | V _b m | ax. 100 | v |
| Cathode current | I _k m | ax. 0.01 | 25 µA/mm ² |
| Ambient temperature | t _{amb} m | ax. 70 | oC |



150AV

PHOTO TUBE

Vacuum phototube with high stability and linearity intended for use in high precision photometry (maximum intensity 1 lux) and for measurements of quickly changing light phenomena (maximum light intensity approx. 1000 lux).

| QUICK REFERENCE DATA | | | | | |
|----------------------|-----------------|----------------------------|-------------------|--|--|
| Anode voltage | va | 6 to 90 | v _{D.C.} | | |
| Average current | Ι _a | max. 50 x 10^{-9} | А | | |
| Peak current | I _{ap} | max. 35 x 10 ⁻⁶ | А | | |
| Sensitivity | N | 60 x 10 ⁻⁶ | A/lumen | | |
| Rise time | | 14 | ns | | |
| Spectral response | | type A | | | |
| Outline, dimensions | | max. 52 x 82 | mm | | |

MECHANICAL DATA

Dimensions in mm



Mounting position: any

7Z2 8040

TENTATIVE DATA

150AV

Photocathode

Cathode material

Caesium-antimony

type A

The cathode material has been deposed on the inner surface of the window. This window is optically plane and polished.

It therefore allows the luminous source to be at close and narrowly reproducable distance from the cathode.

| Useful cathode area | dia. | 30 | mn |
|---------------------|------|----|----|
| | | | |

Spectral response

The spectral response curve shown is a nominal curve and considerable variation between individual tubes may be expected.

| Sensitivity measured with a tungsten ribbon | typical | 60 x 10 ⁻⁶ | A/lumen |
|---|---------|-----------------------|---------|
| lamp having a c.t. of 2850 ^O C | min. | $35 \ge 10^{-6}$ | A/lumen |

Each tube is marked with its sensitivity

An angle of 15° between the axis of the tube and the direction of the incident light decreases the sensitivity not more than 5%.

CAPACITANCE

| Anode to cathode | Cak | 13 pF |
|------------------|-----|-------|
|------------------|-----|-------|

TYPICAL CHARACTERISTICS

| Saturation voltage, | luminous flux (luminous flux | 1 lumen | | | < 6 < 70 | VD VD | .с. с. |
|--------------------------|----------------------------------|---------|-----------------|------|-------------|----------|-----------|
| Anode voltage | | | Va | | 6 to 90 | VD | с. |
| Dark current | | | I _{ao} | max. | 10-12 | А | |
| Linearity ¹) | | | | | 0.1 | % | |
| Insulation resistand | ce | | rins | min. | 10^{15} | Ω | |
| Rise time | | | Tr | | 14 | ns | |
| | | | | | | | |

The relation between the incident luminous flux and the tube current is linear within measuring errors, provided the anode voltage is higher than the saturation voltage.
LIMITING VALUES (Absolute max. rating system)

| Anode voltage | | | Va | max. | 100 | VD.C. |
|------------------|--------------------------|--------|-------------------|------|------------------------|-------------------|
| Cathode current | per mm ² of | | | | | |
| cathode area, | peak | | Ikn | max. | $50 \ge 10^{-9}$ | A/mm ² |
| | average (T _{av} | = 1 s) | Ik | max. | 70 x 10 ⁻¹² | A/mm ² |
| Cathode current, | peak ¹) | | Ikn | max. | 35 x 10-6 | А |
| | average (T_{av} | = 1 s) | Ik | max. | 50 x 10 ⁻⁹ | A |
| Envolopo tompor | aturo | | t _{bulb} | min. | -90 | °C |
| Envelope tempera | ature | | t _{bulb} | max. | +60 | °С |

LIFE EXPECTANCY

With an average cathode current of $50 \ge 10^{-9}$ A, the sensitivity will not decrease more than 10% of its initial value between zero and 500 operating hours.

At lower cathode currents a higher stability may be expected.

REMARKS

- The cathode should not be exposed to direct sunlight.
- In cases where low frequency noise influences the measuring results, this source of noise may be reduced by cooling the tube to -90 °C.

APPLICATION

The currents allowed through 150AV are so low that amplification will always be necessary. To maintain the precision of the signal coming from the photo-tube is often the main problem.

This problem may be divided into four parts:

1. Distortion due to capacitive shunting:

The signal on the input of the amplifier is

$$v = \sqrt{\frac{1}{R^2 + \omega^2 C^2}}$$

in which v = signal in V

i = current through phototube in A

- R = part of series-resistance (in Ω) from which the signal is taken
 = frequency of the signal in Hz
- C = total capacitance of cathode of phototube + input-capacitance of amplifier + stray capacitance of wiring in F. The value of C will not easily be kept below 20 pF.

1) With the cathode uniformly illuminated.

If a certain distortion only is accepted the maximum frequency of the signal to be transferred will limit the value of the resistance from which the signal will be taken and by this limit the value of the signal on the input of the amplifier.

2. Noise:

The level of the signal on the input of the amplifier shall be above the noise level.

The 3 main sources of noise are:

a. Shot noise in the phototube which follows the formula:

 $I_{noise} = \sqrt{2ei \times B'in A_{R.M.S.}}$ $V_{noise} = RxI_{noise}$

· noise

in which $e = 1.6 \times 10^{-19}$ in As

i = the current through the phototube in A

B = the bandwidth in Hz

- R = value of resistor from which signal is taken in Ω
- b. Resistance noise of that part of the series-resistor from which the input signal for the amplifier is taken.

This part of the noise follows the formula:

noise =
$$\sqrt{4 \text{ k T R B}}$$

in which k = 1.35×10^{-23}

 $T = temperature in {}^{O}K$

R = value of resistor in Ω

B = bandwidth in Hz

c. Input-noise of the amplifier

In such cases where an electron tube is used in the input of the amplifier, the noise-voltage follows the formula

$$V_{\text{noise}} = \sqrt{\sum V_{eq}^2 \Delta B}$$

The value of $\rm V_{eq}$ as a function of frequency is different for each type of tube, but for frequencies above 1000 Hz $\rm V_{eq}$ does not change much with the frequency allowing the formula to be reduced to

$$V_{noise} = V_{eq} \sqrt{B}$$

In that case V_{eq} can be approximated within a factor 2 to 3 by

$$V_{eq} = \frac{3 \times 10^{-9} \sqrt{I_a}}{S}$$

in which ${\rm I}_a$ is the anode current of the tube in A and S is the transconductance in A/V.

Bringing the formulas shown in items 1 and 2 together gives: The square of the signal to noise ratio on the input of the amplifier will be:

$$\left\{\frac{\text{signal}}{\text{noise}}\right\}^{2} = \frac{i}{2 \text{ e i } B + 4 \text{ T} \frac{1}{R} B + V_{eq}^{2} B \left(\frac{1}{R^{2}} + \omega^{2} C^{2}\right)}$$

in which i is the current through the phototube in Amperes

3. Input current of the amplifier

- The input-current of the amplifier should be low compared with the signal
 - current through the phototube.

4. Linearity of the amplifier

The amplifier should have a feedback so that the stability and the distortion of the signal is not impaired.

If the circumstances are such that the signal to noise ratio cannot be kept within acceptable limits - usually there where low incident illumination levels combine with high frequencies - use of this type of phototube should be abandoned in preference to photomultipliers where the distortion due to capacitive shunting and noise sources other than shot noise are of smaller relative importance.

Examples:

An example for a simple circuit which is useful for many purposes of static light measurements is shown in fig.1.



In this circuit the μ A meter with 50 μ A f.s.d. may be calibrated in milli-lumen or - if the whole of the cathode is illuminated - in lux. Assuming that the pointer of the μ A meter will not move with frequencies above 20 Hz, for calculation of the noise level frequencies below 20 Hz are of interest only.

For currents of 5×10^{-9} A through the phototube the signal on the input of the amplifier is of a level of 5 V, the shot noise on a level of 10^{-4} V, the resistance noise on a level of 10^{-5} V, the equivalent noise voltage on the input of EC1000 on a level of 10^{-6} V.

The feedback of this system is about 1000 times, so the accuracy is solely determined by the accuracy of the μ A meter, all other sources being small.

Mains voltage variations of +10% and -15% are of no influence on the measuring result.

The circuit of Fig.1 is calibrated as follows: Adjust P₂ so that the total cathode resistance of the EC1000 is $\frac{A \times R_1}{50 \times 1000} \Omega$

in which R_1 is the value of the series resistance of the 150AV and A is the actual sensitivity in $\mu A/lumen$ of the 150AV as marked on the tube.

Disconnect the connection between the phototube and the grid of the EC1000 and connect the grid of EC1000 to earth. Connect the circuit to the mains and adjust P_1 so that the μ A meter indicates zero.

The circuit is now restored and has been calibrated for 0.02 mlumen per μA deflection of the μA meter.

For measurements of rapidly changing phenomena the series-resistor in Fig.1 of 150AV should be adapted for an acceptable signal to noise ratio and acceptable distortion while the μ A meter should be replaced by a resistor shunted by the input of an oscilloscope.

Depending on the frequency further adaptations of the circuit may be necessary, e.g. further smoothing of the D.C. voltages and a D.C. heater supply for the EC1000.

Remark P1 and P2 should be wirewound resistors.

7Z2 6814

For extremely rapid changes when all time constants of the circuit have to be reduced as far as possible a circuit as shown in fig.2 may be used on which laser light flashes can be recorded with a rise time of the signal on the oscilloscope of 20 ns.



fig.2



150CV

PHOTO TUBE

Vacuum phototube with high stability and linearity intended for use in high precision/photometry (maximum intensity 1 lux) and for measurements of quickly changing light phenomena (maximum light intensity approx. 1000 lux).

| QUICK REFERENCE DATA | | | | |
|----------------------|-----------------|-------------------------|----------------------|--------------------|
| Anode voltage | Va | aur e div | 6 to 90 | V _{D.C} . |
| Average current | Ia | max. 3 | 5 x 10-9 | A |
| Peak current | I _{ap} | max. 2 | 5 x 10 ⁻⁶ | A |
| Sensitivity | N N | 200 000 v 10 0 000 v | 0 x 10 ⁻⁶ | A/lumen |
| Rise time | | | 14 | ns |
| Spectral response | | | type C | SAPACITAN |
| Outline dimensions | | max. | 52 x 85 | mm |

MECHANICAL DATA

Dimensions in mm



Mounting position: any

7Z2 8041

TENTATIVE DATA

150CV

Photocathode

Cathode material

Caesium on oxidized silver

The cathode material has been deposed on the inner surface of the window. This window is optically plane and polished.

It therefore allows the luminous source to be at close and narrowly reproducable distance from the cathode.

| Useful cathode area | dia. | 26 | mm |
|---------------------|--------|----|----|
| | | | |
| Spectral response | type C | | |

The spectral response curve shown is a nominal curve and considerable variation between individual tubes may be expected.

| Sensitivity measured with a tungsten ribbon | typical | 20 x 10 ⁻⁶ | A/lumen |
|---|---------|-----------------------|---------|
| lamp having a c.t. of 2850 ^O K | min. | 14 x 10 ⁻⁶ | A/lumen |

Each tube is marked with its sensitivity.

An angle of 15^{0} between the axis of the tube and the direction of the incident light decreases the sensitivity not more than 5%.

CAPACITANCE

| Anode to cathode | Cak | 13 pF |
|------------------|-----|-------|
| | an | |

TYPICAL CHARACTERISTICS

| Saturation voltage, luminous flux 0.05 lumen luminous flux 1 lumen | | | < 6 < 70 | V _{D.C.} V _{D.C.} |
|---|-----------------|------|-------------|--|
| Anode voltage | Va | (| 5 to 90 | V _{D.C} . |
| Dark current | I _{ao} | max. | 10-9 | А |
| Linearity ¹) | | | 0.1 | %o |
| Insulation resistance | rins | min. | 1015 | Ω |
| Rise time | Tr | | 14 | ns |
| | | | | |

¹) The relation between the incident luminous flux and the tube current is linear within measuring errors, provided the anode voltage is higher than the saturation voltage. 7Z2 7182

150CV

LIMITING VALUES (Absolute max. rating system)

| Anode voltage | | Va | max. | 100 | V _{D.C} . |
|------------------------------------|---|--|--------------|---|--|
| Cathode current p cathode area, | per mm ² of peak average (T _{av} = 1 s) | I _k p I _k | max. max. | 50 x 10 ⁻⁹ 70 x 10 ⁻¹² | A/mm ² A/mm ² |
| Cathode current, | peak ¹) average (T _{av} = 1 s) | I _{kp} Ik | max. max. | 25 x 10 ⁻⁶ 35 x 10 ⁻⁹ | A A |
| Envelope tempera | ature | t _{bulb} t _{bulb} | min. max. | -90 +60 | °Ç °Č |

LIFE EXPECTANCY

With an average cathode current of 35×10^{-9} A, the sensitivity will not decrease more than 10% of its initial value between zero and 500 operating hours.

At lower cathode currents a higher stability may be expected.

REMARKS

- The cathode should not be exposed to direct sunlight.
- In cases where low frequency noise influences the measuring results, this source of noise may be reduced by cooling the tube to -90 ^OC.

APPLICATION

Please refer to data of 150AV.



PHOTO TUBE

Vacuum phototube with high stability and linearity intended for use in high precision photometry (maximum intensity 1 lux) and for measurements of quickly changing light phenomena (maximum light intensity approx. 1000 lux).

| QUICK REFERENCE DATA | | | | |
|----------------------|-----------------|----------------------------|-----------------------|--------------------|
| Anode voltage | Va | 144 B. 14 14 4 (15 - 14 | 6 to 90 | V _{D.C} . |
| Average current | Ι _a | max. | $50 \ge 10^{-9}$ | А |
| Peak current | I _{ap} | max. | 35 x 10 ⁻⁶ | A |
| Sensitivity | N | | $35 \ge 10^{-6}$ | A/lumen |
| Rise time | | | 14 | ns |
| Spectral response | | | type U | |
| Outline dimensions | | max. | 53 x 110 | mm |

MECHANICAL DATA

Dimensions in mm



Mounting position: any

7Z2 8042

TENTATIVE DATA

Photocathode

Cathode material

Caesium-antimony

The cathode material has been deposed on the inner surface of the quartz window. This window is optically plane and polished.

It therefore allows the luminous source to be at close and narrowly reproducable distance from the cathode.

Useful cathode area

Spectral response

The spectral response curve shown is a nominal curve and considerable variation between individual tubes may be expected.

| Sensitivity measured with a tungsten ribbon | typical | 60 x 10 ⁻⁶ | A/lumen |
|---|---------|-----------------------|---------|
| lamp having a c.t. of 2850 ^O K | min. | 35 x 10-6 | A/lumen |

Each tube is marked with its sensitivity.

An angle of 15° between the axis of the tube and the direction of the incident light decreases the sensitivity not more than 5 %.

CAPACITANCE

Anode to cathode

Cak

dia. type U

13 pF

30 mm

TYPICAL CHARACTERISTICS

| Saturation voltage, | luminous flux 0.05 lumen luminous flux 1 lumen | | < 6 < 70 | VD.C. |
|----------------------|---|-----------------|------------------------|-------|
| Anode voltage | | va | 6 to 90 | VD.C. |
| Dark current | | I _{ao} | max. 10 ⁻¹² | 2 A |
| Linearity 1) | | | 0.1 | %0 |
| Insulation resistand | ce | rins | min. 10 ¹⁵ | Ω |
| Rise time | | Tr | 14 | ns |
| | | | | |

 The relation between the incident luminous flux and the tube current is linear within measuring errors, provided the anode voltage is higher than the saturation voltage.
 7Z2 7183

LIMITING VALUES (Absolute max. rating system)

| Anode voltage | | Va | max. | 100 | V _{D.C} . |
|-------------------------------|---|--|--------------|--|--|
| Cathode current cathode area, | per mm ² of peak average (T _{av} = 1 s) | I _{kp} I _k | max. max. | $50 \ge 10^{-9}$ 70 \times 10^{-12} | A/mm ² A/mm ² |
| Cathode current, | peak ¹) average (T _{av} = 1 s) | ${\scriptstyle I_{k} \atop I_{k}}$ | max. max. | 35 x 10 ⁻⁶ 50 x 10 ⁻⁹ | A A |
| Envelope temper | ature | ^t bulb t _{bulb} | min. max. | -90 +60 | °C 0°C |

LIFE EXPECTANCY

With an average cathode current of 50×10^{-9} A, the sensitivity will not decrease more than 10% of its initial value between zero and 500 operating hours.

At lower cathode currents a higher stability may be expected.

REMARKS

- The cathode should not be exposed to direct sunlight.
- In cases where low frequency noise influences the measuring results, this source of noise may be reduced by cooling the tube to -90 ^OC.

APPLICATION

Please refer to data of 150AV.



A

PHOTOCELL

Top sensitive gas-filled phototube, sensitive to ultra-violet radiation, intended for use as an on-off device in flame failure circuits.

| | QUICK REFERENCE DATA | ragaa | n daa | auntern |
|----------------|----------------------|-------|-------|---------|
| Supply voltage | | Vb | 220 | VRMS |

OPERATING PRINCIPLE

When photons of sufficient energy strike the cathode of the device electrons may be released. Provided the tube voltage is sufficiently high, these electrons may initiate a discharge. The probability that this will occur is dependent amongst other things on the value of the supply voltage and the ultra-violet radiation intensity.

The discharge will extinguish as soon as the instantaneous value of the tube voltage falls below the maintaining voltage.

It should be noted that most sources of visible light (e.g. the sun, fluorescent lamps) are at the same time sources of U.V. radiation.

Where the level of such radiation affects the reliable operation of the circuit, adequate shielding or filtering should be provided.

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: Noval 4 pins





The arrows show the required direction of incident radiation for highest sensitivity.

Mounting position: any

MOUNTING

A noval socket with a centre hole diameter of at least 5.4 mm should be used. Pins 1 and 6 should be connected to pins 9 and 4 respectively on the socket.

Vm

CHARACTERISTICS

Spectral response

Maintaining voltage

0.2 to 0.29 μm (2000 to 2900 Å) See also page A 180 to 220 V

RECOMMENDED CIRCUITS

I. DIRECT RELAY CIRCUIT (t_{amb} = max. 70 °C)



Notes

- 1. The filter $R_1 C_1$ reduces the effects of high voltage transients on the mains.
- 2. Incidental discharges of the tube will not activate the relay for any value of the mains voltage within the range 220 V +10 % to -15 %.

Sensitivity

Under the worst probable conditions of supply voltage (190 V) component variation and characteristic variation of the tube during 10.000 hours, the tube will activate the relay when a "standard radiation source" (candle, see fig.4) is at a distance < 50 mm from the tube.

RECOMMENDED CIRCUITS (continued)

II. INDIRECT RELAY CIRCUITS (t_{amb} = max. 100 °C)



Fig.2

| R_1 | $100 \ \Omega \pm 10\%$ | C ₁ | $12 \text{ nF} \pm 15\%$ |
|----------------|--------------------------------|---------------------------------|--------------------------|
| R_2 | $100 \Omega \pm 10\%$ | C ₂ | 12 nF ±15% |
| R ₃ | $120 \text{ k}\Omega \pm 10\%$ | C_3^{-} | 2.2 $\mu F \pm 15\%$ |
| R_4 | 120 kΩ <u>+</u> 10% | D ₁ , D ₂ | diodes |
| R_5 | 470 k $\Omega \pm 10\%$ | | |

Note

IIa

The filter $R_1 C_1$ reduces the effects of high voltage transients on the mains.

Sensitivity

The curve on page B shows the relationship between the output voltage V_0 and the distance between the tube and the "standard radiation source" (see fig.4) under the worst probable conditions of supply voltage (198 V) and component variation for the least sensitive new tube.

After the first 10000 hours of operation the sensitivity will have decreased, but will in all cases be better than indicated by the curve on page B provided the radiation source is doubled (two candles according to fig.4).

7Z2 8045

IIb

RECOMMENDED CIRCUITS (continued)



Fig.3

| R ₁ | $100 \Omega \pm 10\%$ | C_1 | 12 nF ±15% |
|----------------|--------------------------------|---------|-------------|
| R ₂ | $100 \ \Omega \ \pm 10\%$ | C_2 | 12 nF ±15% |
| R_3^2 | $330 \text{ k}\Omega \pm 10\%$ | C_3^2 | 2.2 μF ±15% |
| R ₄ | 150 k $\Omega \pm 10\%$ | D_1 | diode |
| R5 | 470 k $\Omega \pm 10\%$ | | |

Note

The filter $R_1 C_1$ reduces the effects of high voltage transients on the mains.

Sensitivity

The curve on page B shows the relationship between the output voltage V_o and the distance between the tube and the "standard radiation source" (see fig.4) under the worst probable conditions of supply voltage (198 V) and component variation for the least sensitive new tube.

After the first 10 000 hours of operation the sensitivity will have decreased, but will in all cases be better than indicated by the curve on page B provided the radiation source is doubled (two candles according to fig.4).

LIMITING VALUES

| Ambient temperature, operation | ng t _{amb} | min25 max. 70 | °C °C | when used in cir- cuit fig.1 |
|--------------------------------|---------------------|------------------|----------------|--|
| | | max. 100 | ^o C | when used in cir- cuits fig.2 and 3 |
| storage | e t _{stg} | min50 max.+50 | °C °C | |
| | | | | 770 0044 |

7Z2 8046

Warning

Designers of flame failure detectors are strongly advised not to depart from the recommended circuits. Any such departure may result in an unsafe operating mode which is likely to cause an internal short in the tube before its rated useful life has expired.

Application notes

To ensure that the intensity of radiation incident on the built-in tube will be sufficient throughout its service life (10000 hours in the case of a new tube) the following procedure should be observed:

For circuit fig.1

Place a "standard radiation source" at a distance of 50 mm from the tube and measure the average voltage across the relay.

In actual operation the same tube should be mounted at a distance from the flame such that the average voltage across the relay is <u>at least</u> equal to that obtained under irradiation from the "standard radiation source" at 50 mm.

Care should be taken that the value of the mains voltage is the same during both measurements.

The flame used during this measurement should be the minimum flame which has to be detected. No further readjustment of the distance between tube and flame will be necessary when the tube has to be replaced.

For circuits fig.2 and fig.3

The output power from the circuits in fig.2 and 3 is too low for direct tripping of a relay. For effective discrimination, the voltage on the input of the added amplifier must attain a certain threshold value when the U.V. energy emitted by the flame attains a certain critical intensity.

The implication is that steps must be taken to ensure that the output voltage $\rm V_O$ from the recommended circuit will remain above this threshold value throughout the life of the tube. This is done in the following way.

Read from the dotted curve on page B the distance d corresponding to the required minimum output voltage V_{Ω} .

Place two "standard radiation sources" at the distance d from the tube and connect the circuit output to a d.c. voltmeter with a high input resistance; observe the average output voltage V_0 . (The mean value around which the needle swings.)

In actual operation the same tube should be mounted at a distance from the flame such that the average output voltage V_0 is at least equal to that obtained under irradiation from the two "standard irradiation sources" at the distance d.

Care should be taken that the value of the mains voltage is the same during both measurements.

The flame used during this measurement should be the minimum flame which has to be detected.

No further readjustment of the distance between tube and flame is necessary when the tube has to be replaced.

Above procedures do of course not include allowance for dirt deposited on the tube during life.





"Standard radiation source"



A



The output voltage as a function of the distance between radiation source and the least sensitive tube in the circuit of fig.3.

The curve is valid at 0 hours when the tube is irradiated by one "standard radiation source" and at 10 000 hours when irradiated by two "standard radiation sources".



The output voltage as a function of the distance between radiation source and the least sensitive tube in the circuit of fig.2.

The curve is valid at 0 hours when the tube is irradiated by one "standard radiation source" and at 10 000 hours when irradiated by two "standard radiation sources".

Photoconductive devices



PHOTOCONDUCTIVE DEVICES APPLICATION DIRECTIONS

1. GENERAL

- 1.1 These application directions are valid for all types of photoconductive cells, unless otherwise stated on the individual technical data sheets.
- 1.2 A photoconductive device is a light-sensitive device whose resistance varies with the illumination on the device.
- 1.3 Where the term <u>illumination</u> is used in the following sections it shall be taken to mean the radiant energy which is normally used to excite the device.
- 1.4 Also in the following sections, <u>history</u> is taken to mean the duration of the specified conditions plus a sufficient description of previous conditions.

2. OPERATING CHARACTERISTICS

- 2.1 The data given on the individual technical data sheets are based on the devices being uniformly illuminated.
- 2.2 The illumination resistance is the ratio of the voltage across the device to the current through the device when illumination is applied to the device.
- 2.2.1 For a particular set of conditions the <u>equilibrium illumination resistance</u> is the illumination resistance after such a time under these conditions that the rate of change of the illumination resistance is less than 1% per 5 minutes.
- 2.2.2 For a particular set of conditions the <u>initial illumination resistance</u> is the first virtually constant value of the illumination resistance after a period of storage or other operating conditions. The initial illumination resistance usually occurs after a few seconds under the specified conditions.
- 2.3 The <u>illumination current</u> is the current which passes when a voltage and illumination are applied to the device.
- 2.3.1 For a particular set of conditions the equilibrium illumination current is the illumination current after such a time under these conditions that the rate of change of the illumination current is less than 1% per 5 minutes.

7Z2 5146

2.3.2 For a particular set of conditions the <u>initial illumination current</u> is the first virtually constant value of the illumination current after a period of storage or other operating conditions.

The initial illumination current usually occurs after a few seconds under the specified conditions.



- 2.4 The <u>dark resistance</u> is the resistance of the device in the absence of illumination.
- 2.4.1 For a particular set of conditions the equilibrium dark resistance is the dark resistance after such a time under these conditions that the rate of change of the dark resistance is less than 2% per 5 minutes.
- 2.4.2 For a particular set of conditions the <u>initial dark resistance</u> is the dark resistance after a specified time under these conditions following a specified history.
- 2.5 The <u>dark current</u> is the current which passes when a voltage is applied to the device in the absence of illumination.
- 2.5.1 For a particular set of conditions the <u>equilibrium dark current</u> is the dark current after such a time under these conditions that the rate of change of the dark current is less than 2% per 5 minutes.
- 2.5.2 For a particular set of conditions the <u>initial dark current</u> is the dark current after a specified time under these conditions immediately following a specified history.
- 2.6.1 For a particular set of conditions and history the <u>resistance decay time</u> is the time taken for the resistance of the device to fall to a specified value measured from the instant of starting the illumination.
- 2.6.2 For a particular set of conditions and history the <u>resistance rise time</u> is the time taken for the resistance of the device to rise to a specified value measured from the instant of stopping the illumination.

2.7.1 For a particular set of conditions and history the <u>current rise time</u> is the time taken for the current through the device to rise to 90% ot its initial illumination current measured from the instant of starting the illumination.



2.7.2 For a particular set of conditions and history the current decay time is the time taken for the current through the device to fall to 10% of its value at the instant of stopping the illumination, measured from that instant.



- 2.8 The <u>illumination sensitivity</u> is the quotient of illumination current by the incident illumination.
- 2.9 The <u>illumination resistance</u> (current) <u>temperature response</u> is the relationship between the illumination resistance (current) and the ambient temperature of the device under constant illumination and voltage conditions.
- 2.10 For a particular set of conditions the initial drift is the difference between the equilibrium and initial illumination current, expressed as a percentage of the initial illumination current.
- 2.11 The illumination response is the relationship between the initial illumination resistance and the illumination, defined as $\frac{\Delta \log r_{10}}{\Delta \log E}$

3. THERMAL DATA

3.1 Ambient temperature. The ambient temperature of a device is the temperature of the surrounding air of that device in its practical situation, which means that other elements in the same space or apparatus must have their normal maximum dissipation and that the same apparatus envelope must be used. This ambient temperature can normally be measured by using a mercury thermometer the mercury container of which has been blackened, placed at a distance of 5 mm from the envelope in the horizontal plane through the centre of the effective area of the CdS tablet.

It shall be exposed to substantially the same radiant energy as that incident on the CdS tablet.

3.2 The thermal resistance of a device is defined as the temperature difference between the hottest point of the device and the dissipating medium, divided by the power dissipated in the device.

4. OPERATIONAL NOTES

4.1 When a photoconductive device is subjected to a change of operating conditions there may be a transient change of current in excess of that due to the difference between the equilibrium illumination currents. This transient change is called overshoot.



4.2 Direct sunlight irradiation should be avoided.

5. MOUNTING

- 5.1 If no restrictions are made on the individual published data sheets, the device may be mounted in any position.
- 5.2 Most of the photoconductive devices may be soldered directly into the circuit, which is indicated on the individual published data sheets. However, the heat conducted to the seal of the device should be kept to a minimum by the use of a thermal shunt. If not otherwise indicated, the device may be dip-soldered at a solder temperature of 240 °C for a maximum of 10 seconds up to a point 5 mm from the seals.

6. STORAGE

It is recommended that the devices be stored in the dark. At any rate direct sunlight irradiation should be avoided.

7. LIMITING VALUES

The limiting values of photoconductive devices are given in the absolute maximum rating system.

8. OUTLINE DIMENSIONS

The outline dimensions are given in mm.

9. SHOCK AND VIBRATION

The conditions for shock and vibration given on the individual data sheets are intended only to give an indication of the mechanical quality of the device. It is not advisable to subject the device to such conditions.



TYPE D

CADMIUM SULPHIDE PHOTOCONDUCTIVE DEVICES

LIST OF SYMBOLS

| Cell voltage | v |
|-------------------------------------|------------------|
| | |
| Cell current | 1 |
| Illumination current | I |
| Initial illumination current | Ilo |
| Equilibrium illumination current | Ile |
| Dark current | Id |
| Initial dark current | Ido |
| Equilibrium dark current | I _{de} |
| Illumination resistance | rl |
| Initial illumination resistance | rlo |
| Equilibrium illumination resistance | rle |
| Dark resistance | r _d |
| Initial dark resistance | rdo |
| Equilibrium dark resistance | rde |
| Current rise time | tri |
| Current decay time | t _{fi} |
| Resistance rise time | trr |
| Resistance decay time | tfr |
| Pulse time | t _{imp} |
| Averaging time | tav |
| Pulse repetition rate | p _{rr} |

| Illumination sensitivity | Ν |
|---------------------------|------------------|
| Illumination response | γ |
| Voltage response | α |
| Ambient temperature | T _{amb} |
| Thermal resistance | К |
| Temperature of CdS tablet | Ttablet |
| Colour temperature | T_{K} |
| Dissipation | Р |
| Illumination | Е |
| Initial drift | Do |
| | |

RATING SYSTEM

ABSOLUTE MAXIMUM RATING SYSTEM

Absolute maximum ratings are limiting values of operating and environmental conditions applicable to any electronic device of a specified type as defined by its published data, which should not be exceeded under the worst probable conditions.

These values are chosen by the device manufacturer to provide acceptable serviceability of the device, taking no responsibility for equipment variations, environmental variations, and the effects of changes in operating conditions due to variations in the characteristics of the device under consideration and of all other electronic devices in the equipment.

The equipment manufacturer should design so that, initially and throughout life, no absolute maximum value for the intended service is exceeded with any device under the worst probable operating conditions with respect to supply voltage variation, equipment component variation, equipment control adjustment, load variations, signal variation, environmental conditions, and variations in characteristics of the device under consideration and of all other electronic devices in the equipment.



ORP 11

CADMIUM SULPHIDE PHOTOCONDUCTIVE CELL

Cadmium sulphide photoconductive cell with top sensitivity intended for use in flame failure, smoke detection circuits and general industrial applications.

| QUICK REFERENCE DATA | | | | | | |
|--|--------|-------------|--------|----|--|--|
| Power dissipation at T_{amb} = 25 ^{O}C | Р | max. | 400 | mW | | |
| Cell voltage, d.c. and repetitive peak | V | max. | 300 | V | | |
| Cell resistance at 50 lux, 2700 ^o K colour temperature | r | | 1700 | Ω | | |
| Spectral response curve | | type D | | 1 | | |
| Outline dimensions | Brist! | max. 17 dia | . x 58 | mm | | |

MECHANICAL DATA

Dimensions in mm



2

7203543

Sensitive area 1.25 cm^2 .

7Z2 5153

1

MAINTENANCE TYPE

ORP 11

ELECTRICAL DATA

General

The electrical properties of CdS cells are dependent on many factors such as illumination, colour temperature of the light source, voltage, current, temperature, total time of operation in the circuit and time of operation during the last 24 hours prior to the measurement. The following basic characteristics are therefore only checkpoints of the electrical properties of these devices measured with defined values of the various conditions and at delivery.

| 2700 °K and at delivery. 1) | | | | | |
|---|-----------------|--------|---------|------|------|
| | symbol | min. | typical | max. | unit |
| Equilibrium dark resistance measured with 300 V d.c. applied via 1 M Ω , 30 minutes after switch- ing off the illumination | r _{de} | 8 | | | MΩ |
| Initial illumination resistance measured at 10 V d.c. and illumi- nation = 50 lux, after 16 hrs in darkness. 2) ³) | rlo | 750 | 1500 | 3000 | Ω |
| Equilibrium illumination resistance measured at 10 V d.c. and illumi- nation = 50 lux, after 15 minutes under the measuring conditions. ³) | r _{le} | | 1700 | | Ω |
| Resistance decay time | t _{fr} | see sl | heet C | | |
| Resistance rise time | t _{rr} | see sl | heet B | | |

Basic characteristics at $T_{amb} = 25$ °C, illumination with colour temperature of 2700 9K and at delivery 1)

LIMITING VALUES (Absolute max. rating system)

| Cell voltage, d.c. and repetitive peak | | V | max. | 300 | V |
|--|----------|------------------|------|-----|------|
| Power dissipation at $T_{amb} = 25 \ ^{\circ}C$) | see also | Р | max. | 400 | mW |
| Power dissipation at T_{amb} = 70 °C \int | sheet A | Р | max. | 100 | mW |
| Ambient temperature, storage and operating operating (< 1 lux) operating (≥ 1 lux) | | T _{amb} | min. | -40 | οС |
| | | Tamb | max. | +50 | °C |
| | | Tamb | max. | +70 | °C 4 |
¹) For sources of illumination other than a lamp of colour temperature 2700 ^oK, the cell resistance should be multiplied by the following approximate factors.

| | Source of illumination | Factor |
|------|---|--------|
| Inca | indescent radiation at colour temperature | e of: |
| | 1500 ^o K | 1/2 |
| | 2000 ^o K | 2/3 |
| | Sunlight | 4/3 |
| | White fluorescent | 2 |

- 2) After 16 hours in darkness changes in the CdS material are still occurring, but have only insignificant effect on the illumination resistance and on the resistance decay time.
- ³) For a.c. conditions, the nominal and limit resistance values are approximately 1.1 times those for d.c. The a.c. values are taken to be r.m.s.
- ⁴) The cell should not be subjected to high relative humidity levels above an ambient temperature of 50 °C. 7Z2 5155











CADMIUM SULPHIDE PHOTOCONDUCTIVE CELL

Cadmium sulphide photoconductive cell with top sensitivity intended for use in flame control, smoke detection and industrial on-off switching applications.

| QUICK REFERENCE DATA | | | | | | |
|--|---|---|------------|---------|----|--|
| Power dissipation at T _{amb} = 25 ^o C | P | | max. | 1.2 | W | |
| Cell voltage, d.c. and repetitive peak | V | 7 | max. | 350 | v | |
| Cell resistance at 50 lux, 2700 ^o K colour temperature | r | | | 330 | Ω | |
| Spectral response curve | | | type D | | | |
| Outline dimensions | | | max. 38 di | a. x 75 | mm | |

MECHANICAL DATA

Dimensions in mm





Total area to be illuminated Sensitive part of this area



111

Base: Octal 7.5 cm² 4.5 cm²

ELECTRICAL DATA

General

The electrical properties of CdS cells are dependent on many factors such as illumination, colour temperature of the light source, voltage, current, temperature, total time of operation in the circuit and time of operation during the last 24 hours prior to the measurement. The following basic characteristics are therefore only checkpoints of the electrical properties of these devices measured with defined values of the various conditions and at delivery. 7Z2 5156

MAINTENANCE TYPE

1

| 2700 ^O K and at delivery | | 1 1 | | 1 | 1 |
|--|-----------------|------|-----------|------|---------|
| And Arnoudwoord | symbol | min. | typical | max. | unit |
| Equilibrium dark current measured with 300 V d.c. applied via 1 MΩ, 15 minutes after switching off the illumination | I _{de} | | | 5 | μΑ |
| <pre>Initial illumination current measured at 10 V d.c. and illu- mination = 50 lux, after 16 hrs in darkness ¹)</pre> | Ilo | 11 | 30 | 47 | mA |
| Initial illumination current measured at 10 V d.c., illumi- nation = 50 lux and colour temper- ature = 1500 ^o K, after 16 hrs in darkness | Ilo | 24 | 60 | 96 | mA |
| Current rise time | t _{ri} | s | see sheet | B | |
| Current decay time | t _{fi} | s | see sheet | В | N RO IN |
| Sensitivity at 50 lux, with 10 Vd.c. applied. | N | | 0.6 | | mA/lux |

LIMITING VALUES (Absolute max. rating system)

| Cell voltage, d.c. and repetitive peak | V | max. 350 | V |
|--|------------------|-----------|-------------------|
| Power dissipation at $T_{amb} = 25 \ ^{OC}$) See also | Р | max. 1.2 | W |
| Power dissipation at T_{amb} = 70 °C \int sheet C | Р | max. 0.35 | W |
| Ambient temperature, storage and operating | Tamb | min40 | ^o C |
| storage | T _{amb} | max. +50 | °C ²) |
| operating | T _{amb} | max. +70 | ^o C |

²) Operation of the cell counteracts the deteriorating effect of long periods at high temperature. The maximum operating temperature is therefore higher than the maximum storage temperature. 7Z2 5157

2

After 16 hours in darkness changes in the CdS material are still occurring, but have only insignificant effect on the illumination resistance and on the resistance decay time.







С



CADMIUM SULPHIDE PHOTOCONDUCTIVE CELL

Cadmium sulphide photoconductive cell with top and side sensitivity.

| QUICK REFEREN | NCE DA | TA | - | Sec. |
|--|--------|-------------------------------|-------|------|
| Power dissipation at T_{amb} = 25 ^{o}C | Р | max. | 0.4 | W |
| Cell voltage, d.c. and repetitive peak | V | max. | 300 | v |
| Cell resistance at 50 lux, 2700 ^o K colour temperature | r | in du con Sinteriorial ann | 2700 | Ω |
| Spectral response curve | | type D | | |
| Outline dimensions | | max. 16 dia | x 44 | mm |

MECHANICAL DATA

Dimensions in mm



Soldering

The cell may be soldered directly into the circuit but heat conducted to the seal should be kept to a minimum by the use of a thermal shunt. The cell may be dip-soldered at a solder temperature of 240 $^{\rm O}{\rm C}$ for a maximum of 10 s up to a point 10 mm from the seals.

1) Not tin plated

7Z2 5158

1

ELECTRICAL DATA

General

The electrical properties of CdS cells are dependent on many factors such as illumination, colour temperature of the light source, voltage, current, temperature, total time of operation in the circuit and time of operation during the last 24 hours prior to the measurement. The following basic characteristics are therefore only checkpoints of the electrical properties of these devices measured with defined values of the various conditions and at delivery.

| 2700 °K and at delivery. | symbol | min. | typical | max. | unit |
|--|-----------------|--------|----------|------------|------|
| Equilibrium dark resistance measured with 300 V d.c. applied via 1 MΩ, 30 minutes after switch- ing off the illumination | rde | 8 | | | MΩ |
| Initial illumination resistance measured at 20 V d.c. and illumi- | | | 6 Gry 12 | | -0 |
| nation = 50 lux, after 16 hrs in darkness 1) | rlo | 1300 | 2700 | 6200 | Ω |
| Equilibrium illumination resistance measured at 20 V d.c. and illumi- nation = 50 lux, after 15 minutes under the measuring conditions | rle | | 3400 | | Ω |
| Resistance decay time Time to reach $7 k\Omega$ measured from the instant of starting the illumi- nation of 50 lux, after 16 hrs in darkness | t _{fr} | | 350 | | ms |
| Resistance rise time Time to reach $25 \text{ k}\Omega$ measured from the instant of stopping the il- lumination, after 15 minutes or | | 1 | | | |
| longer illumination of 50 lux | t _{rr} | an ben | 75 | 1. 11 19 1 | ms |

Basic characteristics at $T_{amb} = 25$ °C, illumination with colour temperature of

 After 16 hours in darkness changes in the CdS material are still occurring, but have only insignificant effect on the illumination resistance and on the resistance decay time.
7Z2 5159

DESIGN CONSIDERATIONS

Apparatus with CdS devices should be designed so that changes in resistance values of the CdS cells during life from -30% to +70% do not impair the circuit performance. Direct sunlight irradiation should be avoided.

LIMITING VALUES (Absolute max. rating system)

| Cell voltage, d.c. and repetitive peak | | V | max. | 300 | V |
|---|----------|------------------|------|-----|----|
| Power dissipation at T_{amb} = 25 °C | See also | Р | max. | 0.4 | W |
| Power dissipation at T_{amb} = 70 ^{o}C | sheet A | Р | max. | 0.1 | W |
| Ambient temperature, storage and o | perating | T _{amb} | min. | -40 | °C |
| storage | | Tamb | max. | +50 | °C |
| operating (< | 1 lux) | Tamb | max. | +50 | °C |
| operating (\geq | l lux) | Tamb | max. | +70 | oC |

7Z2 8028







В



CADMIUM SULPHIDE PHOTOCONDUCTIVE CELL

Cadmium sulphide photoconductive cell with top sensitivity intended for use in flame control and other industrial applications as well as for automatic brightness and contrast control in TV receivers.

The cell is shock and vibration resistant.

| QUICK REFERENCE DATA | | | | | | | |
|--|---|------------|----------|----|--|--|--|
| Power dissipation at T_{amb} = 25 ^{o}C | Р | max. | 70 | mW | | | |
| Cell voltage, d.c. and repetitive peak | V | max. | 350 | V | | | |
| Cell resistance at 50 lux, 2700 ^O K colour temperature | r | | 60 | kΩ | | | |
| Spectral response curve | | type D | | | | | |
| Outline dimensions | | max. 6 dia | . x 16.5 | mm | | | |





 mm^2 0.25

Soldering

Sensitive area

The cell may be soldered directly into the circuit but heat conducted to the seal should be kept to a minimum by the use of a thermal shunt. The cell may be dip-soldered at a solder temperature of 240 °C for a maximum of 10 s up to a point 5 mm from the seals.

- 1) Not tin plated
- ²) Centre of sensitive area

7Z2 5161

Dimensions in mm

2.1

max 5

12±2

max 16.5

ELECTRICAL DATA

General

The electrical properties of CdS cells are dependent on many factors such as illumination, colour temperature of the light source, voltage, current, temperature, total time of operation in the circuit and time of operation during the last 24 hours prior to the measurement. The following basic characteristics are therefore only checkpoints of the electrical properties of these devices measured with defined values of the various conditions and at delivery.

| 2700 ^o K and at delivery | | | | | |
|--|--------|----------------|--|-------------|--|
| and the second | symbol | min. | typical | max. | unit |
| Initial dark current measured at 300 V d.c. applied | | | i | | - marina Salari |
| via 1 M Ω , 20 s after switching off | | a di seria | 1 | a - 13 | Clines I. |
| the illumination | Ido | | | 1.5 | μA |
| Initial illumination current measured at 30 Vd.c. and illumi- nation = 50 lux. after 16 hrs in | | 10-12-14 14 | the state of the s | | an a |
| darkness ¹) | Ilo | 200 | 500 | 800 | μA |
| Sensitivity at 50 lux, with 30 V d.c. | | frank i se | and the second | and some of | and the first of |
| applied | N | | 10 | da. S | $\mu A/lux$ |
| | | | 1 | | |

Basic characteristics at T_{amb} = 25 °C, illumination with colour temperature of 2700 °K and at delivery

End of life characteristics at $T_{amb} = 25$ °C

Life test conditions: Illumination 50 to 100 lux, colour temperature about 2500 $^{\rm O}{\rm K},~{\rm P}$ = 60 mW, ${\rm T}_{\rm amb}$ = 35 $^{\rm O}{\rm C}$

None of the end of life values stated under this heading are expected to be reached before 2500 operating hours under the following conditions:

Initial dark current measured at 300 V d.c., 20 s after switching off the illumination I_{do} max. 3 μ A Change of initial illumination current during life measured at 30 V d.c., illumination = 50 lux and colour temperature = 2700 °K,

after 16 hrs in darkness

 ΔI_{10} max. 60 %

¹) After 16 hours in darkness changes in the CdS material are still occurring, but have only insignificant effect on the illumination resistance and on the resistance decay time.

SHOCK AND VIBRATION

An indication for the ruggedness of the device is the following: Samples taken from normal production are submitted to shock and vibration tests mentioned below. More than 95% of the devices pass these tests without perceptible damage.

Shock

25 gpeak, 3000 shock in one of the three positions of the cell.

Vibration

2.5 gpeak, 50 Hz during 32 hours in each of the three positions of the cell.

LIMITING VALUES (Absolute max. rating system)

| Cell voltage, d.c. and repetitive p | beak | V | max. 350 | V |
|---|-------------|------------------|----------|-------------------------------|
| Power dissipation at T _{amb} = 25 °C | C) See also | Р | max. 70 | mW |
| Power dissipation at T_{amb} = 70 °C | c } sheet B | Р | max. 20 | mW |
| Cell current, d.c. and repetitive | peak | 1 | max. 7.5 | mA |
| Ambient temperature, storage and | l operating | T _{amb} | min40 | °C |
| storage | | T _{amb} | max. +50 | ^o C ¹) |
| operating | | Tamb | max, +70 | °C |

Tamb

operating

7Z2 5163

¹⁾ Operation of the cell counteracts the deteriorating effect of long periods at high temperature. The maximum operating temperature is therefore higher than the maximum storage temperature.





В



Dimensions in mm

CADMIUM SULPHIDE PHOTOCONDUCTIVE CELL

Cadmium sulphide photoconductive cell with side sensitivity intended for use in flame control and other industrial applications as well as for automatic brightness and contrast control in TV receivers.

The cell is shock and vibration resistant.

| QUICK REFERENCE DATA | | | | | | |
|--|---|---------------|------|----|--|--|
| Power dissipation at T_{amb} = 25 ^{o}C | Р | max. | 70 | mW | | |
| Cell voltage, d.c. and repetitive peak | v | max. | 350 | v | | |
| Cell resistance at 50 lux, 2700 ^o K colour temperature | r | | 60 | kΩ | | |
| Spectral response curve | | type D | | | | |
| Outline dimensions | | max. 6 dia. x | 16.5 | mm | | |

MECHANICAL DATA





Sensitive area

 0.25 mm^2

Soldering

The cell may be soldered directly into the circuit but heat conducted to the seal should be kept to a minimum by the use of a thermal shunt. The cell may be dip-soldered at a solder temperature of 240 $^{\rm O}C$ for a maximum of 10 s up to a point 5 mm from the seals.

- 1) Not tin plated
- ²) Centre of sensitive area
- ³) Brown dot

7Z2 5164

1

ELECTRICAL DATA

General

The electrical properties of CdS cells are dependent on many factors such as illumination, colour temperature of the light source, voltage, current, temperature, total time of operation in the circuit and time of operation during the last 24 hours prior to the measurement. The following basic characteristics are therefore only checkpoints of the electrical properties of these devices measured with defined values of the various conditions and at delivery.

| Basic characteristics at T_{amb} = 25 | ^о С, | illumination | with colour | temperature of |
|---|-----------------|-----------------------------|-------------|----------------|
| 2700 ^O K and at delivery | | a construction of the state | | |

| | symbol | min. | typical | max. | unit |
|--|--|--------------------------|------------|--------|--------|
| Initial dark current measured at 300 V d.c. applied | | Richard I. Richard I. | † 17 – m | | 714187 |
| via 1 M Ω , 20 s after switching off | 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1 | | nga, vovia | A CORD | |
| the illumination | Ido | | e na se la | 1.5 | μA |
| Initial illumination current measured at 30 Vd.c. and illumi- | | | | | |
| nation = 50 lux, after 16 hrs in | | | | 1 | |
| darkness ¹) | Ilo | 200 | 500 | 800 | μA |
| Sensitivity at 50 lux, with 30 V d.c. applied | N | | 10 | | µA/lux |
| | | | | | |

End of life characteristics at $T_{amb} = 25 \ ^{O}C$

Life test conditions: Illumination 50 to 100 lux, colour temperature about 2500 $^{\rm o}$ K, P = 60 mW, T_{amb} = 35 $^{\rm o}$ C

None of the end of life values stated under this heading are expected to be reached before 2500 operating hours under the following conditions:

| Initial dark current measured at 300 V d.c., | | | | |
|---|-----------------|------|----|----|
| 20 s after switching off the illumination | Ido | max. | 3 | μA |
| Change of initial illumination current during | | | | |
| life measured at 30 V d.c., illumination = 50 lux and colour temperature = $2700 {}^{\circ}$ K, | | | | |
| after 16 hrs in darkness | ΔI_{lo} | max. | 60 | % |
| | | | | |

 After 16 hours in darkness changes in the CdS material are still occurring, but have only insignificant effect on the illumination resistance and on the resistance decay time.
7Z2 5165

SHOCK AND VIBRATION

An indication for the ruggedness of the device is the following: Samples taken from normal production are submitted to shock and vibration tests mentioned below. More than 95% of the devices pass these tests without perceptible damage.

Shock

25 gpeak, 3000 shocks in one of the three positions of the cell.

Vibration

2.5 g_{peak}, 50 Hz during 32 hours in each of the three positions of the cell.

LIMITING VALUES (Absolute max. rating system)

| Cell voltage, d.c. and repetitive peak | V | max. 350 | V |
|--|------------------|----------|-------------------------------|
| Power dissipation at T_{amb} = 25 ^{O}C See also | Р | max. 70 | mW |
| Power dissipation at $T_{amb} = 70 \text{ °C}^{\circ}$ sheet B | Р | max. 20 | mW |
| Cell current, d.c. and repetitive peak | 1 | max. 7.5 | mA |
| Ambient temperature, storage and operating | T _{amb} | min40 | °C |
| storage | Tamb | max. +50 | ^o C ¹) |
| operating | Tamb | max. +70 | °C |

Tamb

operating

¹⁾ Operation of the cell counteracts the deteriorating effect of long periods at high temperature. The maximum operating temperature is therefore higher than the maximum storage temperature. 7Z2 5166





В



CADMIUM SULPHIDE PHOTOCONDUCTIVE CELL

Cadmium sulphide photoconductive cell with side sensitivity intended for use in flame control and other industrial on off applications. The cell is shock and vibration resistant.

| QUICK REFERENCE DATA | | | | | | |
|--|---|---|----------|------------|----|--|
| Power dissipation at T_{amb} = 25 ^{o}C | 1 | Р | max. | 100 | mW | |
| Cell voltage, d.c. and repetitive peak | | V | max. | 350 | V | |
| Cell resistance at 50 lux, 2700 ^o K colour temperature | | r | | 46 | kΩ | |
| Spectral response curve | | | type D | | | |
| Outline dimensions | | | max. 6 d | ia. x 16.5 | mm | |

MECHANICAL DATA



Sensitive part of this area 1.5 mm^2

Soldering

The cell may be soldered directly into the circuit but heat conducted to the seal should be kept to a minimum by the use of a thermal shunt. The cell may be dip-soldered at a solder temperature of 240 °C for a maximum of 10 s up to a point 5 mm from the seals.

1) Not tin plated

2) Centre of sensitive are

3) Red dot

7Z2 5167

ELECTRICAL DATA

General

The electrical properties of CdS cells are dependent on many factors such as illumination, colour temperature of the light source, voltage, current, temperature, total time of operation in the circuit and time of operation during the last 24 hours prior to the measurement. The following basic characteristics are therefore only checkpoints of the electrical properties of these devices measured with defined values of the various conditions and at delivery.

| AGAO DEL | symbol | min. | typical | max. | unit |
|--|-----------------|-------------|------------|--|----------|
| Initial dark current | | 1. dartes | 1-15 milio | la e forde a series de la series En la series de la se | 1.201112 |
| measured with 300 V d.c. applied via 1 M Ω , 20 s after switching off | 1.00 4.1 | a while | ane es p | in Panjer ku | e Pessie |
| the illumination | Ido | 1.1.1.1.1. | (05-) | 2 | μA |
| Initial illumination current | Strategie Con | | dest afted | | |
| measured at 30 V d.c. and illu- | a nya nya | | navije ka | ter - Ini | Theory R |
| mination = 50 lux, after 16 hrs in darkness. ¹) | Ilo | 300 | 650 | 1000 | μA |
| Current rise time | t _{ri} | see sheet D | | | AHDAM |
| Current decay time | t _{fi} | see sheet D | | | |
| Sensitivity at 50 lux, with 30 V d.c. applied | N | | 13 | | µA/lux |
| | Start H | 1.5 | | - 5,6 - 500 | 12 |

Basic characteristics at $T_{amb} = 25 \text{ }^{\circ}\text{C}$, illumination with colour temperature of

End of life characteristics at $T_{amb} = 25 \ ^{\circ}C$

Life test conditions: Illumination 50 to 100 lux, colour temperature about 2500 $^{\rm O}$ K, P = 85 mW, T_{amb} = 35 $^{\rm O}$ C

None of the end of life values stated under this heading are expected to be reached before 2500 operating hours under the following conditions:

| Initial dark current measured with 300 V d.c. applied | | | | |
|--|-----|------|----|----|
| via 1 M Ω , 20 s after switching off the illumination | Ido | max. | 5 | μA |
| Change of initial illumination current during life | | | | |
| measured at 30 V d.c., illumination = 50 lux and colour | | | | |
| temperature = 2700 °K, after 16 hrs in darkness | Ilo | max. | 50 | % |

 After 16 hours in darkness changes in the CdS material are still occurring, but have only insignificant effect on the illumination resistance and on the resistance decay time.
7Z2 5168

SHOCK AND VIBRATION

An indication for the ruggedness of the cell is the following: Samples taken from normal production are submitted to shock and vibration tests mentioned below. More than 95% of the devices pass these tests without perceptible damage.

Shock

 $25 g_{peak}$, 3000 shocks in one of the three positions of the cell.

Vibration

 $2,5 g_{\text{peak}}$, 50 Hz, during 32 hours in each of the three positions of the cell.

LIMITING VALUES (Absolute max. rating system)

| Cell voltage, d.c. and repetitive peak | | V | max. | 350 | V |
|---|----------|----------------|------|------|-------------------|
| Cell voltage, pulse, t _{imp} = max. 1 ms prr = a few times per 24 hrs | 5 | v _p | max. | 1000 | v |
| Power dissipation at $T_{amb} = 25 \text{ °C}$ | See also | Р | max. | 100 | mW |
| Power dissipation at $T_{amb} = 70 \circ_C \int$ | sheet B | Р | max. | 30 | mW |
| Ambient temperature, storage and ope | erating | Tamb | min. | -40 | oC |
| storage | | Tamb | max. | +50 | °C ¹) |
| operating | HANNE - | Tamb | max. | +70 | °C |

Operation of the cell counteracts the deteriorating effect of long periods a high temperature. The maximum operating temperature is therefore higher than the maximum storage temperature. 7Z2 5169





В



С



D


CADMIUM SULPHIDE PHOTOCONDUCTIVE CELL

Cadmium sulphide photoconductive cell with side sensitivity. The cell is tropic proof, shock- and vibration resistant.

| QUICK REFERENCE DATA | | | | | | | | |
|--|---|--------|--------|----|--|--|--|--|
| Power dissipation | Р | max. | 75 | mW | | | | |
| Cell voltage, d.c. and repetitive peak | V | max. | 100 | v | | | | |
| Cell resistance at 50 lux, 2700 ^o K colour temperature | r | | 1600 | Ω | | | | |
| Spectral response | | type D | | | | | | |
| Outline dimensions | | 6 di | a.x 26 | mm | | | | |



Dimensions in mm



Soldering

The cell may be soldered directly into the circuit but heat conducted to the seal should be kept to a minimum by the use of a thermal shunt. The cell may be dipsoldered at a solder temperature of 240 $^{\rm O}$ C for a maximum of 10 s up to a point 5 mm from the seal.

1) Centre of sensitive area.

²) Not tin plated.

Care should be taken not to bend the leads nearer than 1.5 mm to the seal.

7Z2 8029

MAINTENANCE TYPE

ELECTRICAL DATA

General

The electrical properties of CdS cells are dependent on many factors such as illumination, colour temperature of the light source, voltage, current, temperature, total time of operation in the circuit and time of operation during the last 24 hours prior to the measurement. The following basic characteristics are therefore only checkpoints of the electrical properties of these devices measured with defined values of the various conditions and at delivery.

| = 2700 ^o K and at delivery | | 10.165 | | | |
|---|-----------------|---------|------------------------|------------------|---------------|
| | Symbol | min. | typical | max. | unit |
| Initial dark resistance measured with 100 V d.c. applied via 1 MΩ 20 s after switching | | n qui i | 06.15 K.M | 1. | |
| off the illumination | rdo | 9 | | (1) | ΜΩ |
| Equilibrium dark resistance measured with 100 V d.c. applied via 1 MΩ. 30 min. after switching | | | 0145° | st st katysut | 1165 31962 |
| off the illumination | rde | 250 | 2 | 1) | MΩ |
| Initial illumination resistance measured at $V = 10 V$, illumination | | 750 | 1600 | 2500 | 10316 |
| 50 lux, after 16 nours in darkness ") | rlo | /50 | 1000 | 2500 | 22 |
| Equilibrium illumination resistance measured at V = 10 V, illumination 50 lux, after 15 minutes under the | | .45 | | 5 | |
| measuring conditions | rle | 750 | 1920 | 3250 | Ω |
| Current rise time | | - Park | ा लगा । जिल | To per Mi | |
| Time to reach 90% of its initial illumination current, measured from the instant of starting the illumination | | | ا ڈرۇند <u>ا 8</u> (19 | (instruction) | |
| of 50 lux, at V = 10 V, after 16 hours in darkness | t _{ri} | 112 | 1000 | alio ekir jije | ms |

Basic characteristics at $T_{amb} = 25 \ ^{\circ}C$, illumination with colour temperature

²) After 16 hours in darkness changes in the CdS material are still occurring, but have only insignificant effect on the illumination resistance and on the 7Z2 8030 resistance decay time.

¹) The spread of the dark resistance is large and values higher than 30 M Ω and 2000 M Ω are possible for the initial dark resistance and the equilibrium dark resistance respectively.

| ELECTRICAL DATA (continued) | | | | 47334(s.): | i sand |
|---|-----------------|------------|------------------|------------|------------|
| | Symbol | min. | typical | max. | unit |
| Current decay time | District for | 8 L 1 1 1 | the state of the | 6 | and the |
| Time to reach 10% of its initial | | 17 Section | 11.1 | Note II. | ¥ |
| illumination current, measured fr | om | fi e com | 14 16 19 | | 10.5 |
| the instant of stopping the illumi- | | | 15 17.4 | 149, 35 | e, la cube |
| nation of 50 lux, at V = 10 V, after | c | | | | 10.12 |
| 16 hours in darkness | t _{fi} | | 75 | in as | ms |
| Sensitivity at 50 lux, with $V = 10 V c$ | l.c. | 1.11 | A. Car | | |
| applied | N | | 0.15 | and and | mA/lux |
| Negative temperature response of t | he | | | e teleno | |
| illumination resistance | | | 0.2 | 0.5 | %/°C |
| Voltage response $\frac{r \text{ at } 0.5 \text{ V}}{r \text{ at } 10 \text{ V}}$ | α | | 1.5 | | |

DESIGN CONSIDERATIONS

It should be noted that this cell is designed for very high typical sensitivity with respect to its sensitive area, but that it may be expected that a high sensitivity will only be maintained if the dissipation averaged over 2 s is kept below 20 mW at 25 $^{\circ}$ C. Higher dissipations will accelerate the aging process which lowers sensitivity.

SHOCK AND VIBRATION

An indication for the ruggedness of the cell is the following: Samples taken from normal production are submitted to shock and vibration tests mentioned below: More than 95% of the devices pass these tests without perceptible damage.

Shock

 $25g_{peak}$, 10000 shocks in one of the three positions of the cell.

Vibration

2.5 g_{peak} , 50 Hz, during 32 hours in each of the three positions of the cell.

LIMITING VALUES (Absolute max. rating system)

| Cell voltage, d.c. and repetitive peak | V | max. | 100 | V |
|--|------|--------|--------|-------|
| Power dissipation, $t_{av} = 2 s$ | Р | see sl | neet A | |
| Ambient temperature, storage and operating | Tamb | min. | -40 | °C |
| Storage | Tamb | max. | +40 | °C 1) |
| Operating | Tamb | max. | +70 | °С |

4

Operation of the cell counteracts the deteriorating effect of long periods at the high temperature. The maximum operating temperature is therefore higher than the maximum storage temperature. 7Z2 8032





1.1.1967

A



CADMIUM SULPHIDE PHOTOCONDUCTIVE CELL

Cadmium sulphide photoconductive cell with side sensitivity intended for use in flame control, smoke detector or industrial on-off switching applications. The cell is shock and vibration resistant.

| QUICK REFER | ENCE | DATA | | |
|--|------|-------------|--------|----|
| Power dissipation at T_{amb} = 25 °C | Р | max. | s 1 | W |
| Cell voltage, d.c. and repetitive peak | V | max. | 350 | V |
| Cell resistance at 50 lux, 2700 ^o K colour temperature | r | | 1000 | Ω |
| Spectral response curve | | type D | | |
| Outline dimensions | | max. 19 dia | x 60.3 | mm |

MECHANICAL DATA

Dimensions in mm



Base: 7 p. miniature

Total area to be illuminated $1.1 \times 2.9 \text{ cm}^2$

ELECTRICAL DATA

General

The electrical properties of CdS cells are dependent on many factors such as illumination, colour temperature of the light source, voltage current, temperature, total time of operation in the circuit and time of operation during the last 24 hours prior to the measurement. The following basic characteristics are therefore only checkpoints of the electrical properties of these devices measured with defined values of the various conditions and at delivery.

| 2700 ^o K and at delivery. | symbol | min. | typical | max. | unit |
|--|-----------------|------|---------|------|--------|
| Initial dark current measured with 300 V d.c. applied via 1 MΩ, 20 s after switching off the illumination | I _{do} | | | 70 | μΑ |
| Equilibrium dark current measured with 300 V d.c. applied via 1 MΩ, 15 minutes after switching off the illumination | I _{do} | | -830 | 2.5 | μA |
| <pre>Initial illumination current measured at 10 V d.c. and illu- mination = 50 lux, after 16 hrs in darkness ¹)</pre> | Ilo | 3 | 10 | 15 | mA |
| Initial illumination current measured at 10 V d.c., illumina- tion = 50 lux and colour tempera- ture = 1500 ^o K, after 16 hrs in darkness | Ilo | 6 | 20 | 31 | mA |
| Sensitivity at 50 lux, with 10 V d.c. applied | Ν | | 0.2 | | mA/lux |
| Current rise time | t _{ri} | | see she | et B | |
| Current decay time | t _{fi} | | see she | et B | 29 P |

Basic characteristics at $T_{amb} = 25$ °C, illumination with colour temperature of 2700 °K and at delivery.

¹) After 16 hours in darkness changes in the CdS material are still occurring, but have only insignificant effect on the illumination resistance and on the resistance decay time. 7Z2 5174

LIMITING VALUES (Absolute max. rating system)

| Cell voltage, d.c. and repetitive peak | | V | max. | 350 | V |
|--|----------|------|------|-----|-------|
| Power dissipation at T_{amb} = 25 °C (| See also | Р | max. | 1.0 | W |
| Power dissipation at $T_{amb} = 70 \text{ °C}$ | sheet C | Р | max. | 0.3 | W |
| Ambient temperature, storage and ope | erating | Tamb | min. | -40 | °C |
| storage | | Tamb | max. | +50 | °C 1) |
| operating | | Tamb | max. | +70 | °C |

 Operation of the cell counteracts the deteriorating effect of long periods at high temperature. The maximum operating temperature is therefore higher than the maximum storage temperature. 7Z2 5175





1.1.1967

В



С

CdS CELLS-LAMP COMBINATION

Combination of four cadmium sulphide photoconductive cells and a small incandescent lamp in a Noval envelope for use in relais circuits with low output resistance, control circuits and logic circuits.

| QUICK REFERENCE DATA | | | | | | |
|---|---|------------|-----------|----|--|--|
| Power dissipation, each cell, at T_{amb} = 25 ^{o}C | Р | max. | 150 | mW | | |
| Cell voltage, d.c. and repetitive peak | v | max. | 200 | v | | |
| Cell resistance | r | | 15 | Ω | | |
| Outline dimensions | | max. 22 di | a. x 55.6 | mm | | |

MECHANICAL DATA

Dimensions in mm

Base: Noval





ELECTRICAL DATA

Basic characteristics at $T_{amb} = 25$ ^oC, and at delivery

| | symbol | min. | typical | max. | unit |
|--|--------|------|---------|------|------|
| Lamp filament voltage | Vf | | 24 | | v |
| Lamp filament current at V_f = 24 V | If | 54 | 60 | 66 | mA |
| Initial dark current measured in the circuit of fig.1 | Ido | | | 15 | μΑ |

| Basic characteristics at $T_{amb} = 25$ °C, ar | nd at deli | very (c | ontinued |) | |
|---|---------------------|----------------------------------|-----------------|------------|----------------------------------|
| | symbol | min. | typical | max. | unit |
| Initial illumination resistance measured in the circuit of fig.1 after 16 hrs in darkness ¹) | rlo | 3.307.2 | 15 | 25 | Ω |
| Resistance decay time Time to reach 400 Ω in circuit of fig.2, measured from the in- stant of starting the illumination ofter 16 brs in dorkness | | i bulak ka tibak kahi ili | | 30 | dic aŭ desolo secolo me |
| | ur | | | 50 | 1115 |
| Resistance rise time Time to reach 300 k Ω in circuit of fig.2, measured from the in- stant of stopping the illumination after 5 minutes or longer illu- mingtion | | | | 1.7 | 6 |
| | urr | | | 1.7 | |
| Insulation resistance between two cells or between cell and fila- ment measured at 300 V d.c. | r _{ins} | 200 | | | MΩ |
| CAPACITANCES measured at filament vol | tage V _f | = 0 V | | | |
| Between the terminals of each cell | | | Cr | 9 | .5 pF |
| Between any cell terminal and the filament (except pins 4 and 6) | | | C _{rf} | max. | 1 pF |
| REMARK | | | | | |
| Shock and vibration should be avoided. | | | | | |
| LIMITING VALUES (Absolute max. rating | system) |) | | | |
| Filament voltage (d.c. or r.m.s.) | 1-12-1 | Vf | max. | 25.2 | V ²) |
| Cell voltage, d.c. and repetitive peak | | V | max. | 200 | V. |
| Power dissipation of each cell at T _{amb} = 2 | 5 °C | Р | max. | 150 | mW ³) |
| Power dissipation of each cell at T _{amb} = 5 | 5 °C | Р | max. | 85 | mW ³) |
| Voltage between any pair of cells | 6.85 | V _{ri} -V _{ri} | max. | 350 | v |
| Ambient temperature, operating | | T _{amb} | min. max. | -40 +55 | °C °C 3) |
| | | | | 77 | 22 5177 |

Measuring circuit for rlo and Ido



Fig.1

Measuring circuit tfr and trr



- 1) After 16 hours in darkness changes in the CdS material are still occurring, but have only insignificant effect on the illumination resistance and on the resistance decay time.
- 2) It is recommended to ensure that during operation the filament voltage V_f exceeds as little as possible the nominal value of 24 V. The life expectancy is considerably longer with lower values of V_f.
- ³) For $V_f = 24$ V.





A

CADMIUM SULPHIDE PHOTOCONDUCTIVE CELL

Cadmium sulphide photoconductive cell with side sensitivity intended for use in general control circuits. The cell is tropic proof, shock and vibration resistant.

| QUICK REFERENCE DATA | | | | | | | |
|---|---|---------------|--------|----|--|--|--|
| Power dissipation at T_{amb} = 25 ^{o}C | Р | max. | 0.5 | W | | | |
| Power dissipation, with a heatsink with K = 5 $^{\rm o}$ C/W and T _{amb} = 25 $^{\rm o}$ C | Р | max. | 2 | W | | | |
| Cell voltage, d.c. and repetitive peak | V | max. | 100 | V | | | |
| Cell resistance at 5000 lux, 2700 ^O K colour temperature | r | | 25 | Ω | | | |
| Spectral response curve | | type D | | | | | |
| Outline dimensions | | max. 27 x 16. | .3 x 6 | mm | | | |

MECHANICAL DATA

Dimensions in mm





The centre distance of the leads is compatible with the IEC standard raster for printed wiring (0.1 inch).

Soldering

The cell may be soldered directly into the circuit but heat conducted to the seal should be kept to a minimum by the use of a thermal shunt. The cell may be dipsoldered at a solder temperature of 240 $^{\rm O}$ C for a maximum of 10 s up to a point 5 mm from the seals.

ELECTRICAL DATA

General

The electrical properties of CdS cells are dependent on many factors such as illumination, colour temperature of the light source, voltage, current, temperature, total time of operation in the circuit and time of operation during the last 24 hours prior to the measurement. The following basic characteristics are therefore only checkpoints of the electrical properties of these devices measured with defined values of the various conditions and at delivery.

| 2700 ^O K and at delivery. | 1 | 12. 369. | ins alomeo | pigen y | |
|--|---------------------|----------|----------------------|---------|------|
| | symbol | min. | typical | max. | unit |
| Initial dark resistance measured with 100 V d.c. applied via 1 MΩ, 20 s after switching off | | 12.74 | oenaare en ligiod | di siri | |
| the illumination | rdo | 5.6 | la de la | (1) | MΩ |
| Equilibrium dark resistance measured with 100 V d.c. applied via 1 M Ω , 30 minutes after switching off the illumination | rde | 50 | n 1 Mai 1 | 1) | MΩ |
| <pre>Initial illumination resistance (1) measured at 10 V d.c., illumina- tion = 50 lux, after 16 hrs in darkness. 2)</pre> | r _{lo} (1) | 235 | 400 | 1200 | Ω |
| <pre>Initial illumination resistance (2) measured at 1 V d.c., illumina- tion = 5000 lux, after 16 hrs in darkness 2)3)</pre> | r _{lo} (2) | | 25 | 35 | Ω |

¹) The spread of the dark resistance is large and values higher than 15 M Ω and 2000 M Ω are possible for the initial dark resistance and the equilibrium dark resistance respectively.

- ²) After 16 hours in darkness changes in the CdS material are still occurring, but have only insignificant effect on the illumination resistance and on the resistance decay time.
- 3) Maximum during life 40 Ω .

| nin. 235 | typical 480 | max. | unit |
|-------------|----------------|---|---|
| 35 | 480 | 1560 | 0 |
| | | | 36 |
| | | | |
| | | 35 | Ω |
| | | | |
| | 5 | 25 | ms |
| | 40 | 200 | |
| | 40 | 200 | 1115 |
| | 0.5 | | mA/lux |
| | 0.2 | 0.5 | %/°C |
| | 1.1 | | |
| | | | |
| Тt | ablet | max. +8 | 85 ^o C |
| K | | 1: | 20 ⁰ C/W |
| | | | |
| | T _t | 40 0.5 0.2 1.1 Ttablet K | 40 200 0.5 0.5 1.1 0.5 T _{tablet} max. +4 K 1: |

¹) After 16 hours in darkness changes in the CdS material are still occurring, but have only insignificant effect on the illumination resistance and on the resistance decay time.

²) Maximum during life 40 Ω .

DESIGN CONSIDERATIONS

Apparatus with CdS cells should be designed so that changes in resistance values of the cells during life from -30% to +70% do not impair the circuit performance. Direct sunlight irradiation should be avoided.

SHOCK AND VIBRATION

An indication for the ruggedness of the cell is the following:

Samples taken from normal production are submitted to shock and vibration tests mentioned below. More than 95% of the devices pass these tests without perceptible damage.

Shock

 $25 \text{ g}_{\text{peak}}$, $10\,000 \text{ shocks}$ in one of the three positions of the cell.

Vibration

2,5 g_{peak}, 50 Hz, during 32 hours in each of the three positions of the cell.

N.B. These conditions are used solely to assess the mechanical quality of the cell. It is not advisable to subject the cell to such conditions.

LIMITING VALUES (Absolute max. rating system)

| Cell voltage, d.c. and repetitive peak | V | max. | 100 | V |
|---|---------------------|--------|-------|-------------------------------|
| Cell voltage, pulse, t _{imp} = max. 5 ms prr = max. once per minute | Vp | max. | 250 | V |
| Power dissipation, $t_{av} = 2 s$ | Р | see sh | eet C | |
| Power dissipation, pulse | Pp | max. | 5 x P | |
| Cell current, d.c. and repetitive peak | 1 | max. | 250 | mA |
| Illumination | Е | max. | 50000 | lux |
| Temperature CdS tablet, operating | T _{tablet} | max. | +85 | ^o C ¹) |
| Ambient temperature, storage and operating | T _{amb} | min. | -40 | °C |
| storage | T _{amb} | max. | +50 | °C 2) |
| operating | Tamb | max. | +70 | °C |

¹) If no forced air cooling is used, the envelope temperature opposite the centre of the sensitive area is about 83 °C when the CdS tablet temperature is 85 °C. This temperature can be determined e.g. with a thermocouple fastened on the envelope.

²) Operation of the cell counteracts the deteriorating effect of long periods at high temperature. The maximum operating temperature is therefore higher than the maximum storage temperature. 77.2 7966

Dimensions in mm

MECHANICAL DATA (continued)

RPY18 MOUNTED ON HEATSINK





Detail: Clamping strip tombac 0.3 mm

| With a | a | = | 50 | mm | Κ | = | 19 | °C/W |
|--------|---|---|-----|----|---|---|-----|------|
| With a | a | = | 100 | mm | Κ | = | 7.5 | °C/W |

Mounting instructions

- 1. Mount one clamp on the heatsink, using the side with round holes.
- 2. Push the RPY18 under than clamp.
- 3. Press the second clamp firmly against the RPY18, using the slot holes.



A



B



С

CADMIUM SULPHIDE PHOTOCONDUCTIVE CELL

Cadmium sulphide photoconductive cell with side sensitivity intended for use in general control circuits.

The cell is tropic proof, shock and vibration resistant.

| QUICK REFEREN | CE DA | TA | | |
|--|-------|-----------|----------|----|
| Power dissipation at T _{amb} = 25 ^o C | Р | max. | 0.5 | W |
| Power dissipation, with a heatsink with K = 5 ^o C/W and T _{amb} = 25 ^o C | Р | max. | 2 | w |
| Cell voltage, d.c. and repetitive peak | v | max. | 400 | v |
| Cell resistance at 50 lux, 2700 ^o K colour temperature | r | | 3000 | Ω |
| Spectral response curve | | type D | | |
| Outline dimensions | | max. 27 x | 16.3 x 6 | mm |

MECHANICAL DATA

Dimensions in mm





Soldering

The cell may be soldered directly into the circuit but heat conducted to the seal should be kept to a minimum by the use of a thermal shunt. The cell may be dip-soldered at a solder temperature of 240 $^{\circ}$ C for a maximum of 10 s up to a point 5 mm from the seals.

ELECTRICAL DATA

General

The electrical properties of CdS cells are dependent on many factors such as illumination, colour temperature of the light source, voltage, current, temperature, total time of operation in the circuit and time of operation during the last 24 hours prior to the measurement. The following basic characteristics are therefore only checkpoints of the electrical properties of these devices measured with defined values of the various conditions and at delivery.

| 2700 °K and at delivery | | F dima 3 | 18 18 117 | pter di si | 17000 |
|---|-----------------|--|------------------------------------|------------|-----------------|
| | symbol | min. | typical | max. | unit |
| Initial dark resistance measured with 300 V d.c. applied via 1 MΩ, 20 s after switching off | | | | | |
| the illumination | rdo | 10 | SE S GI | 1) | MΩ |
| Equilibrium dark resistance measured with 300 V d.c. applied | | iour 16 ree | es X ^a (00 La sériér | | National States |
| ing off the illumination | rde | 200 | , por cien | 1) | MΩ |
| Initial illumination resistance measured at 10 V d.c. illumination = 50 lux, after 16 hrs | | | 67.60 | | |
| in darkness ²) | rlo | 1400 | 3000 | 6600 | 52 |
| Equilibrium illumination resistance measured at 10 V d.c. illumination = 50 lux, after 15 min- utes under the measuring condi- | | and and a second se | | | |
| tions | rle | 1400 | 3800 | 9000 | Ω |
| Resistance decay time Time to reach 20 k Ω , measured from the instant of starting the illumination of 50 lux, at 10 V d.c. | | | | | |
| after 16 hours in darkness | t _{fr} | | | 0.2 | S |

Basic characteristics at Tamb = 25 °C, illumination with colour temperature of

¹) The spread of the dark resistance is large and values higher than 100 M Ω and 10000 M\Omega are possible for the initial dark resistance and the equilibrium dark resistance respectively.

²⁾ After 16 hours in darkness changes in the CdS material are still occurring, but have only insignificant effect on the illumination resistance and on the resistance decay time.

| Basic characteristics at $T_{amb} = 25 \ ^{\circ}C$ 2700 $^{\circ}K$ and at delivery (continued) | , illumin | ation v | with colou | r temp | erature of |
|---|-----------------|------------------|------------|--------|---------------------|
| , (, | symbol | min. | typical | max. | unit |
| Resistance rise time Time to reach $1 M\Omega$, measured from the instant of stopping the illumina- tion often 5 minutes on heaven illu |) 19 1) | 1998. 1998. S | | | |
| mination of 50 lux, at 10 V d.c. | t _{rr} | | 0.6 | 1.25 | Ş |
| Sensitivity | N | | 0.07 | | mA/lux |
| Negative temperature response of illumination resistance | | | 0.2 | 0.5 | %/°С |
| Voltage response $\frac{r \text{ at } 0.5 \text{ V d.c.}}{r \text{ at } 10 \text{ V d.c.}}$ | α | han. | 1.1 | | araan Taridah |
| THERMAL DATA | | | | | |
| Continuous temperature of CdS tablet | | Tt | ablet | max. + | 85 ^o C |
| Thermal resistance from CdS tablet to ambient, device free in air | ранота. | K | | 1 | 20 ⁰ C/W |
| Thermal resistance from CdS tablet to heatsink (temperature of heatsink measurednear the centre of the cell), when the cell is properly clamped or |) , 1 | V | | | 25 00 m |
| a neatsink as described on sheet 5 | | K | | | 25 °C/W |

DESIGN CONSIDERATIONS

Apparatus with CdS cells should be designed so that changes in resistance values of the cells during life from -30% to +70% do not impair the circuit performance. Direct sunlight irradiation should be avoided.

SHOCK AND VIBRATION

An indication for the ruggedness of the cell is the following: Samples taken from normal production are submitted to shock and vibration tests mentioned below. More than 95% of the devices pass these tests without perceptible damage.

Shock

25 gpeak, 10000 shocks in one of the three positions of the cell.

Vibration

2.5 gpeak, 50 Hz, during 32 hours in each of the three positions of the cell.

| LIMITING VALUES (Absolute max. rating syst | em) | | |
|---|------------------|-------------|-------|
| Cell voltage, d.c. and repetitive peak | V | max. 400 | V |
| Cell voltage, pulse, T _{imp} = max. 5 ms p _{rr} = max. once per minute | Vp | max. 1000 | V |
| Power dissipation, $t_{av} = 1 s$ | Р | See sheet C | |
| Power dissipation, pulse | Pp | max. 5xP | 2.17 |
| Cell current, d.c. and repetitive peak | 1 | max. 250 | mA |
| Illumination | E | max. 50000 | lux |
| Temperature CdS tablet, operating | Ttablet | max. +85 | °C 1) |
| Ambient temperature, storage and operating | Tamb | min40 | °C |
| storage | T _{amb} | max. +50 | °C 2) |
| operating | Tamb | max. +70 | °C |

7Z2 7970

4

¹⁾ If no forced air cooling is used, the envelope temperature opposite the centre of the sensitive area is about 83 °C when the CdS tablet temperature is 85 °C. This temperature can be determined e.g. with a thermocouple fastened on the envelope.

²) Operation of the cell counteracts the deteriorating effect of long periods at high temperature. The maximum operating temperature is therefore higher than the maximum storage temperature.

RPY19 MOUNTED ON HEATSINK





Detail: Clamping strip tombac 0.3 mm

The heat resistance K of the heatsink is defined as the temperature difference between the point Q at the backside of the heatsink, and ambient at point P, per Watt dissipation in the device, the heatsink being placed in an enclosure as given below.

Enclosure: cubical with internal edges $5 \times a \mod 3$.

Place : point Q in the centre of the cubic, plane of heatsink vertical, top upside.

Determined according to the above rules a heatsink as given in the drawing has a heat resistance K = 19 $^{\circ}C/W$ when a = 50 mm and a K = 7.5 $^{\circ}C/W$ when a = 100 mm.

With smaller enclosure dimensions a higher value for K may be expected.

Mounting instructions

To reach the above mentioned K values it is essential that the RPY19 be installed in the following manner:

1. Mount one clamp on the heatsink, using the side with round holes.

2. Push the RPY19 under that clamp.

3. Press the second clamp firmly against the RPY19, using the slot holes.



A





CADMIUM SULPHIDE PHOTOCONDUCTIVE CELL

Cadmium sulphide photoconductive cell with side sensitivity intended for use in general control circuits such as twilight switches and flame failure equipment. The cell is tropic proof, shock and vibration resistant.

| QUICK REFERENCE DATA | | | | | | | |
|--|-----------------------------|-----------|----------|----|--|--|--|
| Power dissipation at T_{amb} = 25 °C | Р | max. | | W | | | |
| Power dissipation, with a heatsink with K = 5 °C/W and T _{amb} = 25 °C | Р | max. | 3 | Ŵ | | | |
| Cell voltage, d.c. and repetitive peak | v | max. | 400 | v | | | |
| Cell resistance at 50 lux, 2700 ^o K colour temperature | r | | 1500 | Ω | | | |
| Spectral response curve | | type D | | | | | |
| Outline dimensions | ्वयद्य प्रमुख १४ च जनसंब | max. 43 x | 16.3 x 6 | mm | | | |

MECHANICAL DATA



The centre distance of the leads is compatible with the standard raster for printed wiring (0.1 inch)

7Z2 7916

Dimensions in mm

Soldering

The cell may be soldered directly into the circuit but heat conducted to the tablet should be kept to a minimum by the use of a thermal shunt. The cell may be dip-soldered at a solder temperature of 240 $^{\rm O}C$ for a maximum of 10 s up to a point 5 mm from the seals.

ELECTRICAL DATA

General

The electrical properties of CdS cells are dependent on many factors such as illumination, colour temperature of the light source, voltage, current, temperature, total time of operation in the circuit and time of operation during the last 24 hours prior to the measurement. The following basic characteristics are therefore only checkpoints of the electrical properties of these devices measured with defined values of the various conditions and at delivery.

| Basic characteristics at | $T_{amb} = 25 {}^{o}C,$ | illumination | with colour | temperature | of |
|-------------------------------------|-------------------------|--------------|-------------|-------------|----|
| 2700 ^o K and at delivery | | | | | |

| | | | La Contractor | | - 1 Kim |
|--|-----------------|------|---------------|----------------|------------|
| | symbol | min. | typical | max. | unit |
| Initial dark resistance measured with 300 V d.c. applied | | | www.co.com | denorí i | inse (|
| via 1 M Ω , 20 s after switching off | | | enters. | aliments | or ang Q. |
| the illumination | r _{do} | 6.5 | | 1) | MΩ |
| Equilibrium dark resistance | | | ATA | ų tenni | el Antonio |
| measured with 300 V d.c. applied via 1 M Ω , 30 minutes after switch- | | | | | |
| ing off the illumination | r _{de} | 120 | 1 | ¹) | MΩ |
| Initial illumination resistance measured at 10 V, d.c. illumination = 50 lux, after 16 hrs | | | | | |
| in darkness ²) | rlo | 700 | 1500 | 3300 | Ω |
| Equilibrium illumination resistance measured at 10 V, d.c. | n and a second | | | | |
| illumination = 50 lux, after 15 min- utes under the measuring condi- | | | | | |
| tions | r _{le} | 700 | 1900 | 4500 | Ω |
| | | | | | |

1) The spread of the dark resistance is large and values higher than 100 M Ω and 10000 M Ω are possible for the initial dark resistance and the equilibrium dark resistance respectively.

2) After 16 hours in darkness changes in the CdS material are still occurring, but have only insignificant effect on the illumination resistance and on the resistance decay time. 7Z2 7917

| 2700 °K and at delivery (continued) | 18.10.20 | | | | |
|--|---------------------------|---|---|--------------------|---------|
| | symbol | min. | typical | max. | unit |
| Resistance decay time Time to reach 10 k Ω , measured from the instant of starting the il- lumination of 50 lux, at 10 V d.c. after 16 hours in darkness 2) | tfr | | ing and the second s | 0.2 | S |
| Resistance rise time Time to reach 1 M Ω , measured from the instant of stopping the illumination after 5 minutes or longer illumination of 50 lux, at | | | | alen Lien | |
| 10 V d.c. | trr | | 0.9 | 1.5 | S |
| Sensitivity at 50 lux, with 10 V d.c. applied | N | | 0.15 | noile né Motiva | mA/lux |
| Negative temperature response of illumination resistance | | | 0.2 | 0.5 | %/°C |
| Voltage response $\frac{r \text{ at } 0.5 \text{ V } \text{ d.c.}}{r \text{ at } 10 \text{ V } \text{ d.c.}}$ | α | | 1.05 | adiew | NOV C |
| THERMAL DATA | angi sety a 1975 april | | a sila si 1 sila si | BS Agiv Interna | |
| Continuous temperature of CdS table | t d s literi | Tt | ablet ¹ | max. + | 85 °C |
| Thermal resistance from CdS tablet to ambient, device free in air | 0 | K | HOITA. | | 60 °C/W |
| Thermal resistance from CdS tablet to heatsink (temperature of heatsink measured near the centre of the cell) when the cell is properly clamped of | o), n | анара 2. араан 2. араан 2. араан | | | |

D.

7Z2 7918

Shoper

OPERATING CONDITIONS in a typical twilight switching circuit.



- C = CdS cell RPY20
- R = D.C. Relay 20 k Ω with $I_e < 2.7$ e.g. energizing current I_e of 2 mA and release current I_r of 0.8 mA.

VDR = voltage dependent resistor 10 mA at 180 V, 2 W e.g. type E299DG/P248

- F = Absorption filter to be used to correct spread of the circuit and to adjust the switching level (10 to 70 lux). Light transmission 5 to 20 %.
- D = Diode $V_{inv_D} > 500 V$

DESIGN CONSIDERATIONS

Apparatus with CdS cells should be designed so that changes in resistance values of the cells during life from -30 % to +70 % do not impair the circuit performance. Direct sunlight irradiation should be avoided.

SHOCK AND VIBRATION

An indication for the ruggedness of the cell is the following:

Samples taken from normal production are submitted to shock and vibration tests mentioned below. More than 95% of the devices pass these tests without perceptible damage.

Shock

25 gpeak, 10000 shocks in one of the three positions of the cell.

Vibration

2.5 gpeak, 50 Hz, during 32 hours in each of the three positions of the cell.
| LIMITING VALUES (Absolute max. rating system) | | | | | | | | | |
|---|---|---------------------|---------|---------|-------------------|--|--|--|--|
| Cell voltage, | d.c. and repetitive peak | V | max. | 400 | V | | | | |
| Cell voltage, | pulse, t _{imp} = max. 5 ms p _{rr} = max. once per minute | Vp | max. | 1000 | v | | | | |
| Power dissip | ation, t _{av} = 2 s | Р | See she | eet B | | | | | |
| Power dissip | Pp | max. | 5xP | | | | | | |
| Cell current, | d.c. and repetitive peak | Í | max. | 500 | mA | | | | |
| Illumination | | Е | max.5 | 0 0 0 0 | lux | | | | |
| Temperature | CdS tablet, operating | T _{tablet} | max. | +85 | °C 1) | | | | |
| Ambient temperature, storage and operating | | T _{amb} | min. | -40 | °C | | | | |
| | storage | T _{amb} | max. | +50 | °C ²) | | | | |
| | operating | T _{amb} | max. | +70 | °C | | | | |

¹) If no forced air cooling is used, the envelope temperature opposite the centre of the sensitive area is about 83 °C when the CdS tablet temperature is 85 °C. This temperature can be determined e.g. with a thermocouple fastened on the envelope.

²) Operation of the cell counteracts the deteriorating effect of long periods at high temperature. The maximum operating temperature is therefore higher than the maximum storage temperature. 7Z2 7919

RPY20 MOUNTED ON HEATSINK







The heat resistance K of the heatsink is defined as the temperature difference between the point Q at the backside of the heatsink, and ambient at point P, per Watt dissipation in the device, the heatsink being placed in an enclosure as given below.

Enclosure: cubical with internal edges 5 x a mm

Place : point Q in the centre of the enclosure, plane of heatsink vertical, "top" up

Determined according to the above rules a heatsink as given in the drawing has a heat resistance K = 19 $^{O}C/W$ when a = 50 mm and K = 7.5 $^{O}C/W$ when a = 100 mm.

With smaller enclosure dimensions a higher value for K may be expected.

Mounting instructions

To reach the above mentioned K values it is essential that the RPY20 be installed in the following manner:

1. Mount one clamp on the heatsink, using the side with round holes.

2. Push the RPY20 under that clamp.

3. Press the second clamp firmly against the RPY20, using the slot holes.



A



В





CADMIUM SULPHIDE PHOTOCONDUCTIVE CELL

Cadmium sulphide photoconductive cell with top sensitivity intended for use in general control circuits such as twilight switches and flame failure equipment. The cell is tropic proof, shock and vibration resistant.

| QUICK REFERENCE DATA | | | | | | | | |
|--|---|--------------|----------|----|--|--|--|--|
| Power dissipation at T_{amb} = 25 °C | Р | max. | 1 | W | | | | |
| Cell voltage, d.c. and repetitive peak | v | max. | 400 | v | | | | |
| Cell resistance at 50 lux, 2700 ^o K colour temperature | r | | 650 | Ω | | | | |
| Spectral response curve | | type D | | | | | | |
| Outline dimensions | | max. 31.5 di | a.x 7.25 | mm | | | | |

MECHANICAL DATA



Soldering

The cell may be soldered directly into the circuit but heat conducted to the seal should be kept to a minimum by the use of a thermal shunt. The cell may be dip-soldered at a solder temperature of 240 $^{\rm O}C$ for a maximum of 10 s up to a point 5 mm from the seals.

ELECTRICAL DATA

General

The electrical properties of CdS cells are dependent on many factors such as illumination, colour temperature of the light source, voltage, current, temperature, total time of operation in the circuit and time of operation during the last 24 hours prior to the measurement. The following basic characteristics are therefore only checkpoints of the electrical properties of these devices measured with defined values of the various conditions and at delivery.

| -CS/DATA_ | symbol | min. | typical | max. | unit |
|--|-----------------|----------------|----------------------|--------------------------|----------------------|
| Initial dark resistance measured with 400 V d.c. applied via 1 MΩ, 20 s after switching off | | nd. repetit | F 16 don Bris | an an State Biologian | 19999 1990 - 1990 |
| the illumination | rdo | 6.0 | N 08 11 1 | 1) | MΩ |
| Equilibrium dark resistance measured with 400 V d.c. applied via 1 MΩ, 30 minutes after switch- | - 110 - | erteqina 9 | bolour i nac curv | 45-11 | Specie |
| ing of the illumination | r _{de} | 100 | SUCCESSION STREET | 1) | MΩ |
| Initial illumination resistance measured at 10 V d.c. after 16 hrs in darkness ²) illumination 50 lux | r _{lo} | 380 | 650 | 1900 | n ABORI , Ω |
| Equilibrium illumination resistance measured at 10 V d.c. after 15 minutes under the meas- uring conditions | | 1 | P | | |
| illumination 50 lux | r _{le} | 380 | 820 | 2600 | Ω |

Basic characteristics at T_{amb} = 25 °C, illumination with colour temperature of 2700 °K and at delivery

¹) The spread of the dark resistance is large and values higher than 100 M Ω and 10 000 M Ω are possible for the initial dark resistance and the equilibrium dark resistance respectively.

²) After 16 hours in darkness changes in the CdS material are still occurring, but have only insignificant effect on the illumination resistance and on the resistance decay time. 7Z2 7914

| 2700 ^o K and at delivery (continued) | of the te | aconthe | est i offi | sol in | |
|---|-------------------|-----------------|----------------------------------|--------------------|---------------------|
| | symbol | min. | typical | max. | unit |
| Resistance decay time Time to reach 10 kΩ, measured from the instant of starting the il- lumination of 50 lux, at 10 V d.c. after 16 hours in darkness ²) | t _{fr} | | antor sig si si actes u | 0.2 | S |
| Resistance rise time | | | | | |
| Time to reach 1 M Ω , measured from the instant of stopping the il- lumination after 5 minutes or | | 6d 58 . | egcalah ja | H-08 | |
| longer illumination with 50 lux, at 10 V d.c. | t _{rr} | m shi | 1.0 | 1.5 | s |
| Sensitivity at 50 lux, with 10 V d.c. applied | N | ana na ann - | 0.3 | ove jou Nigicai | mA/lux |
| Negative temperature response of illumination resistance | | r piq s e | 0.2 | 0.5 | %/°C |
| Voltage response $\frac{r \text{ at } 0.5 \text{ V d.c.}}{r \text{ at } 10 \text{ V d.c.}}$ | α | rina. | 1.05 | allugit T | att, tavu Att ta |
| THERMAL DATA | | | | | |
| Continuous temperature of CdS tablet | | Tt | ablet ¹ | max. + | -85 °C |
| Thermal resistance from CdS tablet to ambient, device free in air | o arono bi | K | | | 60 °C/1 |

DESIGN CONSIDERATIONS

Apparatus with CdS cells should be designed so that changes in resistance values of the cells during life from -30 % to +70 % do not impair the circuit performance. Direct sunlight irradiation should be avoided.

SHOCK AND VIBRATION

An indication for the ruggedness of the cell is the following: Samples taken from normal production are submitted to shock and vibration tests mentioned below. More than 95 % of the devices pass these tests without perceptible damage.

Shock

 $25 \text{ g}_{\text{peak}}$, 10000 shocks in one of the three positions of the cell.

Vibration

2.5 g_{Deak} , 50 Hz, during 32 hours in each of the three positions of the cell.

LIMITING VALUES (Absolute max. rating system)

| Cell voltage, d.c. and repetitive peak | V | max. 40 | 00 V |
|---|---------------------|-----------|----------------------|
| Cell voltage, pulse, t _{imp} = max. 5 ms p _{rr} = max. once per minute | Vp | max. 100 | 00 V |
| Power dissipation, $t_{av} = 2 s$ | Р | See sheet | В |
| Power dissipation, pulse | Pp | max. 5x | хP |
| Cell current, d.c. and repetitive peak | I | max. 25 | 50 mA |
| Illumination - | E | max.5000 | 00 lux |
| Temperature CdS tablet, operating | T _{tablet} | max. +8 | 35 °C |
| Ambient temperature, storage and operating | Tamb | min4 | 40 °C |
| storage | T _{amb} | max. +5 | 60 °C ¹) |
| operating | Tamb | max. +7 | 70 °C |

 ¹) Operation of the cell counteracts the deteriorating effect of long periods at high temperature. The maximum operating temperature is therefore higher than the maximum storage temperature. 7Z2 5199

4



A



В

CADMIUM SULPHIDE PHOTOCONDUCTIVE CELL

Cadmium sulphide photoconductive cell with side sensitivity intended for use in general control circuits.

The cell is tropic proof, shock and vibration resistant.

| QUICK REFERENCE DATA | | | | | | | | | |
|--|-----|----------|---------|----|--|--|--|--|--|
| Power dissipation at T_{amb} = 25 °C | Р | max. | 225 | mW | | | | | |
| Cell voltage, d.c. and repetitive peak | V | max. | 100 | V | | | | | |
| Cell resistance at 50 lux, 2700 ºK colour temperature | r | | 1.6 | kΩ | | | | | |
| Spectral response curve | | type D | | | | | | | |
| Outline dimensions | · . | max. 22x | 9.8x4.3 | mm | | | | | |

MECHANICAL DATA

Dimensions in mm



Soldering

The cell may be soldered directly into the circuit but heat conducted to the seal should be kept to a minimum by the use of a thermal shunt. The cell maybe dip-soldered at a solder temperature of 240 $^{\rm O}$ C for a maximum of 10 s up to a point 5 mm from the seals.

7Z2 7971

TENTATIVE DATA

ELECTRICAL DATA

General

The electrical properties of CdS cells are dependent on many factors such as illumination, colour temperature of the light source, voltage current, temperature, total time of operation in the circuit and time of operation during the last 24 hours prior to the measurement. The following basic characteristics are therefore only checkpoints of the electrical properties of these devices measured with defined values of the various conditions and at delivery.

| 2700 ^o K and at delivery | | | - | | |
|---|-----------------|------------------|------------------------------------|---------------|--------|
| (1.4.1.4.1.4.1.4.1.4.1.4.1.4.1.4.1.4.1.4 | symbol | Imin. | typical | max. | unit |
| Initial dark resistance measured with 100 V d.c. applied via 1 M Ω , 20 s after switching off the illumination | r _{do} | 9 | int of the | 1) | MΩ |
| Equilibrium dark resistance measured with 100 V d.c. applied via 1 M Ω , 30 minutes after switch- ing off the illumination | r _{de} | 100 | ua o a su ugé o ure minée | 1) | MΩ |
| <pre>Initial illumination resistance measured at V = 10 V d.c., illumination 50 lux, after 16 hours in darkness ²)</pre> | rlo | 950 | 1600 | 4800 | Ω |
| Equilibrium illumination resistance measured at V = 10 V d.c., illumination 50 lux, after 15 minutes under the measuring conditions | r _{le} | 950 | 1900 | 6200 | Ω |
| Resistance decay time Time to reach 20 k Ω at V = 10 V d.c. measured from the instant of starting the illumination of 50 lux, after 16 hours in darkness. 2) | ter | | | 0.2 | S |
| Resistance rise time Time to reach 1 M Ω at V = 10 V d.c. measured after 5 minutes or longer illumination of 50 lux | trr | | 1.0 | 1.5 | S |
| Sensitivity, at V = 10 V d.c. and 50 lux | 'N | a ta ta Tanàn | 0.12 | litay († 1 | mA/lux |
| Negative temperature response of illumination resistance | | i rin Alie | 0.2 | 0.5 | %/°C |
| Voltage response $\frac{r \text{ at } 0.5 \text{ V d.c.}}{r \text{ at } 10 \text{ V d.c.}}$ | α | | 1.1 | | |

7Z2 7972

1)2) See page 4

THERMAL DATA

| Continuous temperature of CdS tablet | T _{tablet} | +85 | oC |
|--|---------------------|-----|------|
| Thermal resistance from CdS tablet to ambient, | | | |
| device free in air | K | 265 | °C/W |
| | | | |

DESIGN CONSIDERATIONS

Apparatus with CdS cells should be designed so that changes in resistance values of the CdS cells during life from -30% to +70% do not impair the circuit performance. Direct sunlight irradiation should be avoided.

SHOCK AND VIBRATION

An indication for the ruggedness of the cell is the following: Samples taken from normal production are submitted to shock and vibration tests mentioned below. More than 95% of the devices pass these tests without perceptible damage.

Shock

 $25 \text{ g}_{\text{peak}}$, 10000 shocks in one of the three positions of the cell.

Vibration

 $2.5 g_{\text{peak}}$, 50 Hz, during 32 hours in each of the three positions of the cell.

LIMITING VALUES (Absolute max. rating system)

| Cell voltage, d.c. and repetitive peak | V | max. 100 | V |
|---|--|-------------------------------|-------------------|
| Cell voltage, pulse, T _{imp} = max. 5 ms P _{rr} = max. once per minute | Vp | max. 250 | v |
| Power dissipation, t_{av} = 2 s | Р | See sheet B | |
| Power dissipation, pulse | Pp | max. 5 x P | W |
| Cell current, d.c. and repetitive peak | Ι | max. 100 | mA |
| Illumination | Е | max. 50000 | lux |
| Temperature CdS tablet, operating | T _{tablet} | max. +85 | °C 3) |
| Ambient temperature, storage and operating storage operating | T _{amb} T _{amb} T _{amb} | min40 max. +50 max. +70 | °C °C 4) °C |

NOTES

- 1. The spread of the dark resistance is large and values higher than $30~M\Omega$ and $2000~M\Omega$ are possible for the initial dark resistance and the equilibrium dark resistance respectively.
- 2. After 16 hours in darkness changes in the CdS material are still occurring, but have only insignificant effect on the illumination resistance and on the resistance decay time.
- 3. If no forced air cooling is used, the envelope temperature opposite the centre of the sensitive area is about 83 °C when the CdS tablet temperature is 85 °C. This temperature can be determined e.g. with a thermocouple fastened on the envelope.
- 4. Operation of the cell counteracts the deteriorating effect of long periods at high temperature. The maximum operating temperature is therefore higher than the maximum storage temperature.



A



в

CADMIUM SULPHIDE PHOTOCONDUCTIVE CELL

Cadmium sulphide photoconductive cell with side sensitivity. The device satisfies Test C: Damp heat test (long term exposure), severity IV (56 days exposure) of Publication 68-2 of the International Electrotechnical Commission (IEC).

| QUICK REFERENCE DATA | | | | | | | | |
|--|---|---------|----------|----|--|--|--|--|
| Power dissipation at T_{amb} = 25 °C | Р | max. | 0.75 | W | | | | |
| Cell voltage, d.c. and repetitive peak | V | max. | 400 | v | | | | |
| Cell resistance at 50 lux, 2700 ^o K colour temperature | r | | 1500 | Ω | | | | |
| Spectral response.curve | | type D | | | | | | |
| Outline dimensions | | max.30. | 5x13.5x2 | mm | | | | |

MECHANICAL DATA

Dimensions in mm



Soldering

The cell may be soldered directly into the circuit but heat conducted to the tablet should be kept to a minimum by the use of a thermal shunt. The cell may be dip-soldered at a solder temperature of 240 $^{\circ}$ C for a maximum of 10 s up to a point 5 mm from the seal.

Mounting

The cell is not insulated electrically and should be mounted accordingly.

7Z2 7978

TENTATIVE DATA

ELECTRICAL DATA

General

The electrical properties of CdS cells are dependent on many factors such as illumination, colour temperature of the light source, voltage, current, temperature, total time of operation in the circuit and time of operation during the last 24 hours prior to the measurement. The following basic characteristics are therefore only checkpoints of the electrical properties of these devices measured with defined values of the various conditions and at delivery.

| Basic | characteristics | at | Tamb | = 25 | °С, | illumination | with | colour | temperature |
|--------|------------------------------|------|------|------|-----|--------------|------|--------|-------------|
| of 270 | 0 ^o K and at deli | very | 7 | | | | | | |

| | symbol | min. | typical | max. | unit |
|--|-----------------|---------|---------|------|------|
| Initial dark resistance | | | | | |
| measured with 300 V d.c. applied via 1 M Ω , 20 s after switching off | | - 1.04 | | 1.00 | |
| the illumination | rdo | 10 | | 1) | MΩ |
| Equilibrium dark resistance measured with 400 V d.c. applied via 1 MQ 30 minutes after switch- | | | | | |
| ing off the illumination | rde | 200 | | 1) | MΩ |
| Initial illumination resistance measured at 10 V d.c. illumina- | | * | ht a h | | |
| tion = 50 lux, after 16 hrs in darkness 2) | r _{lo} | 700 | 1500 | 3300 | Ω |
| Equilibrium illumination resistance measured at 10 V d.c. illumina- | | | | | |
| tion = 50 lux, after 15 minutes | | 1.1.7.1 | | | |
| under the measuring conditions | rle | 700 | 1900 | 4500 | Ω |

¹) The spread of the dark resistance is large and values higher than 100 M Ω and 10 000 M Ω are possible for the intial dark resistance and the equilibrium dark resistance respectively.

²) After 16 hours in darkness changes in the CdS material are still occurring, but have only insignificant effect on the illumination resistance and on the resistance decay time. 7Z2 7979

| Basic characteristics at T_{amb} = 25 °C, illumination with colour temperature | | | | | | |
|--|-----------------|------------|---------|------|-----------|--|
| of 2700 °K and at delivery (continued) | | | | | | |
| | symbol | min. | typical | max. | unit | |
| Resistance decay time Time to reach 10 k Ω , measured from the instant of starting the il- lumination of 50 lux at 10 V d.c. after 16 hrs in darkness ²) | t _{fr} | | | 0.2 | S | |
| Resistance rise time Time to reach 1 M Ω , measured from the instant of stopping the il- lumination after 5 minutes or longer illumination of 50 lux, at 10 V d.c. | trr | | 0.9 | 1.5 | S | |
| Sensitivity at 50 lux, with 10 V d.c. applied | N | D I va | 0.15 | | mA/lux | |
| Negative temperature response of illumination resistance | | 5 9 H (16) | 0.2 | 0.5 | %/°C | |
| Voltage response $\frac{r \text{ at } 0.5 \text{ V d.c.}}{r \text{ at } 10 \text{ V d.c.}}$ | α | | 1.05 | | in larget | |

THERMAL DATA

Continuous temperature of CdS tablet

Ttablet +85

CLIMATIC DATA

The device satisfies test C: Damp heat test (long term exposure), severity IV (56 days exposure) of Publication 68-2 of the International Electrotechnical Commission (IEC).

2) After 16 hours in darkness changes in the CdS material are still occurring, but have only insignificant effect on the illumination resistance and on the resistance decay time.

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OC

LIMITING VALUES (Absolute maximum rating system)

| Cell voltage, d.c. and repetitive peak | v | max. 400 | v |
|--|---------------------|-------------|-------|
| Cell voltage, pulse, timp = max, 5 ms | | | |
| $p_{rr} = max.$ once per minute | Vp | max. 1000 | V |
| Power dissipation, $t_{av} = 2 s$ | Р | see sheet C | |
| Power dissipation, pulse | Pp | max. 5xP | |
| Cell current, d.c. and repetitive peak | I | max. 500 | mA |
| Illumination | Е | max. 50000 | lux |
| Temperature CdS tablet, operating | T _{tablet} | max. +85 | oС |
| Ambient temperature, storage and operating | T _{amb} | min40 | °С |
| storage | T _{amb} | max. +50 | °C 1) |
| operating | T _{amb} | max. +70 | oC |

DESIGN CONSIDERATIONS

Apparatus with CdS cells should be designed so that changes in resistance values of the cells during life from -30% to +70% do not impair the circuit performance. Direct sunlight irradiation should be avoided.

SHOCK AND VIBRATION

An indication for the ruggedness of the cell is the following: Samples taken from normal production are submitted to shock and vibration tests mentioned below. More than 95% of the devices pass these tests without perceptible damage.

Shock

25 g_{peak} , 10000 shocks in one of the three positions of the cell.

Vibration

 $2.5 g_{peak}$, 50 Hz, during 32 hours in each of the three positions of the cell.

 Operating of the cell counteracts the deteriorating effect of long periods at high temperature. The maximum operating temperature is therefore higher than the maximum storage temperature 7Z2 7981



A



В



С



Photomultiplier tubes



PHOTOMULTIPLIER TUBES APPLICATION DIRECTIONS

1. GENERAL

- 1.1 <u>A photomultiplier</u> is a photosensitive vacuum device comprising a photoemissive cathode, a photo-electron collection system and one or more stages of current multiplication utilizing secondary emission electrodes (dynodes), plus an anode.
- 1.2 A photocathode consists of a light-sensitive film (the emission layer) and \overline{a} supporting layer on which the emission layer is deposited.

Two types of cathode may be distinguished:

- a. the opaque photocathode
- b. the semi-transparent photocathode.

In the first type, the emission layer is deposited on a metal surface. In the second type the light quanta must pass through the wall of the tube and the transparent carrier layer before penetrating the photosensitive film. Al-though opaque photocathodes can be made more easily, semi-transparent photocathodes are most widely used, since they can be placed in the front of the tube, which has many advantages for the construction and use of the photomultipliers.

1.3 <u>The photo-electron collection system</u> (electron-optical input system) is that part of the photomultiplier which focuses the photo-electrons on the first dynode. This mainly determines the spread of the electron transit times. The quality of the input optics can be measured not only by the spread of the electron transit times, but also by the collection efficiency, i.e. the percentage of electrons emitted by the photocathode which land on the first dynode.

Because of the variation in magnitude and direction of the initial velocity of the electrons, each point on the cathode corresponds to a small image area on the dynode. In practice, it is sufficient to ensure that the first dynode is large enough to capture all electrons.

It is possible to improve the input optics by adding other electrodes, or by making an accelerating electrode separate from the first dynode, and one or more focusing electrodes separate from the cathode, but the improvement is only noticeable in very high-quality fast tubes such as the 56AVP, XP1020, etc.

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1.4 The dynode system consists of a number of secondary-emission electrodes (dynodes). Several dynode constructions are possible. All tubes mentioned in this book have a dynode structure of the linear-focused type, which is built up from dynodes of caesium-coated silver magnesium, excepted the windowless types which are equipped with copper-beryllium dynodes. Every electron which lands on a dynode does not produce the same number of secondary electrons: this number depends on the angle of incidence and velocity of the electron. Usually, however, it is sufficient to consider the mean secondary-emission factor δ_p of the pth dynode, which is equal to the total number of secondary electrons falling on to it. As a rule it is also permissible to assume that all dynodes have the same value of this factor, δ , so that the amplification produced by the tube is given by

 $G = \delta^n$

where n is the number of dynodes.

1.5 The anode is usually made of wire mesh in order to ensure a low anode capacitance, and is placed directly in front of the last dynode. Although the secondary-emission factor of the anode material is very small, it cannot be ignored completely, since the number and velocity of the electrons landing on the anode is relatively large.

The ions, possibly formed in the anode space, are mainly attracted to the last dynode. Since the distance between the anode and this dynode is relatively small, the ions do not acquire enough energy to give rise to any secondary electrons.

2. INTERPRETATION OF CHARACTERISTICS

The characteristics given in the Data section are typical values which indicate the performance of the device under certain operating conditions.

Characteristic curves represent an average tube; individual tubes may have characteristics that deviate from the values given in the characteristic curves. All tubes are accompanied by a test-card which indicates the test conditions of the tube.

The more important characteristics for photomultipliers are discussed below.

2.1 Spectral response

The materials employed to make the photocathode are of great importance to obtain the desired response. Many substances show photo-emission, but often differ greatly in their spectral sensitivity and quantum yield.

Usually the spectral response of a photosensitive device is given as a function of wavelength in per cent of the maximum response.

As to the spectral response our range of photomultipliers can be subdivided into the following categories:

- 2.1.1 <u>the A-types (S11)</u>, which are equipped with a semi-transparent cesiumantimony photocathode precipitated on the inner side of a polished B40glass end window; these types are sensitive to light in the visible region, and have their maximum sensitivity in the blue region (see fig.1).
- 2.1.2 the U-types (S13), which have the same photocathodes as the A-types, but are provided with a polished optical quartz window, which gives them a sensitivity that extends into the ultraviolet region (see fig.2), and guarantees the absence of K^{40} radiation.
- 2.1.3 the C-types (S1), which have a semi-transparent caesium-on-silver oxide photocathode on a polished B40-glass window. Its sensitivity lies mainly in the red and near-infrared region, with a maximum at about 8000 Å (see fig.3).
- 2.1.4 the T-types (S20), which have a trialkali semi-transparent photocathode on a polished B40-glass window. This photocathode is the most sensitive known for the region from the ultraviolet to the red end of the spectrum (see fig.4).
- 2.1.5 <u>the TU-types</u>, which have the same photocathode as the T-types, but are provided with a polished optical quartz window, which gives them a sensitivity that extends into the ultraviolet region (see fig.5).
- 2.1.6 the SB (solar blind)-types, which are provided with a semi-transparent cesium-tellurium photocathode on a polished optical quartz window. These types have an ultraviolet response with exclusion of light in the visible region (see fig.6).

2.2 Cathode luminous sensitivity

The cathode luminous sensitivity is defined as the photocurrent emitted per lumen of incident light flux, generally expressed in μ A/lm. For the measurement the multiplier is connected as a diode. The cathode current (corrected for dark current) I_k is of the order of 100 nano amperes. The voltage must be chosen so high that the tube is surely operating in the saturation range. The sensitivity is given by

$$N_k = I_k/\Phi;$$

where ϕ is the luminous flux in lumens of 2850 °K tungsten light.

2.3 Cathode radiant sensitivity

The cathode radiant sensitivity is defined as the photocurrent emitted per watt of incident light flux, generally expressed in mA/W at the wavelength of maximum response. For the measurement the same procedure is used as for the luminous sensitivity. The value of incident radiant flux is measured by a thermocouple.

2.4 Cathode quantum efficiency

The cathode quantum efficiency (η) is defined as the number of photo-electrons per incident light photon, usually expressed in per cent at a certain wavelength.

Quantum efficiency at any given wavelength can be easily calculated from the following formula:

$$\eta = N_{kr} \cdot y(\lambda_x) \cdot (\frac{12.395}{\lambda_x})$$

where N_{kr} = the cathode radiant sensitivity at max. response in mA/W.

 $y(\lambda_x)$ = is the relative spectral response in % at λ_x

 λ_x = wavelength in A

Lines of constant quantum efficiency are shown in fig.7.

2.5 Current amplification (gain) and anode sensitivity

The current amplification (G) is the ratio of the anode signal current to the cathode signal current at stated electrode voltages.

The anode sensitivity (N_a) is related to the gain (G) and the cathode sensitivity (N_k) by the formula

$$N_a = G \cdot N_k$$
.

Since the gain is so high $(> 10^6)$, it is not possible, to measure both the anode and the cathode currents under the same conditions. The anode current is normally below 1 mA, so the cathode current is thus a few tenths of a nano amp.

Since the cathode current, dynode currents and anode current are practically proportional to the incident luminous flux, the following method can be used to get over this difficulty:

First the photomultiplier is connected as a diode, and the cathode is illuminated so strongly that it gives a cathode current of about 0.1 μ A. This current is measured, and then the luminous flux falling on the photocathode is reduced to a fraction (1/a₁) of its original value by means of e.g. a neutral filter of known transmittance, the appropriate voltage is applied to the photomultiplier, and the anode current measured. The gain is then given by

$$G = \frac{I_a}{a_1 \cdot I_k}$$

The attenuation factor a_1 can also be measured with the aid of the tube, as the ratio of the currents flowing to one dynode after and before the reduction of the luminous flux. If the gain is very high, it is advisable to measure it in a number of steps: e.g. from the cathode to the p^{th} dynode and from the p^{th} dynode to the anode.

2.6 Dark current

Even when the cathode is not illuminated, a certain current flows through the anode lead. This is known as the anode dark current (I_{ac}) .

Anode dark current is measured at stated electrode voltages, or at electrode voltages required to provide a stated anode luminous sensitivity. Possible causes of anode dark current are electrical leakage, thermionic emission, field emission, residual gas ionization and tube fluorescence. At low operating voltages its major components are normally electrical leakage and thermionic emission. Thermionic emission can be recognized by its temperature dependence. At high values of applied voltage the other dark current components may become an appreciable part of the total dark current.

2.7 Linearity and saturation

The cathode and dynode currents should always be in the region of saturation so as to guarantee the proportionality between the current and the cathode illumination over the whole operating range. Fig.8 shows the cathode current as a function of the voltage for a number of different luminous fluxes. The resistance of the photocathode plays an important role in determining these characteristics. Even if the transparent, conductive supporting layer is applied with great care, the cathode resistance will be of the order of some hundreds of kilo-ohms. The voltage between the cathode and the first dynode must therefore be chosen higher than the voltage between successive dynodes if the current is to be saturating throughout the working range.



Fig.8 The cathode as a function of the voltage between the photocathode and the first dynode at various values of the luminous flux.

The saturation current of the dynodes, on the other hand, is always reached under normal operating conditions even at the highest permissible luminous flux, so there is no need to take any special measures about them.

The situation at the anode is once again different. The anode current causes a voltage drop across the resistance in series with the tube, so that the anode voltage decreases as the anode current increases. Moreover, care must be taken that the current is not limited by space-charge effects even at the largest permissible anode currents in order to ensure an undistorted output signal.

The upper limits of the electrode currents are determined by considerations of operating life and of the avoidance of fatigue and aging effects.

- 2.8 Time characteristics
- 2.8.1 The transit time of a photomultiplier tube is defined as the time interval between the arrival of a delta-function light pulse (a pulse having finite light flux and infinitesimal width) at the entrance window of the tube and the time at which the output pulse at the anode terminal reaches peak amplitude.
- 2.8.2 The anode pulse rise time indicates the time required for the amplitude to rise from 10 % to 90 % of the peak amplitude. For this measurement the incident light usually illuminates the entire photocathode.
- 2.8.3 <u>Transit-time difference expresses a systematic relationship between</u> transit time and position of illumination on the photocathode. The reference position is mostly the center of the photocathode.

3. OPERATING NOTES

3.1 <u>The overall supply voltage</u> should be well stabilized, since the gain of a photomultiplier is critically dependent on the voltage by the following relation

$$\frac{dG}{G} = n \frac{dV_b}{V_b}$$
.

So the percentage change in gain is approximately ten times the percentage change in supply voltage. Thus, to hold the gain stable within 1%, the power supply must be stabilised to within approximately 0.1 %.

Where a high current supply cannot be avoided, due to a high counting rate or the need to measure a continuous luminous flux, it is possible to employ a high current source of comparatively low voltage for the last three or four stages only, and a low current high voltage source for the remaining stages. If it is undesirable to maintain one power supply terminal at the sum of the two voltages with respect to earth, the common terminal may be earthed.

- 3.2 The voltage divider of a photomultiplier must be designed so that it does not give any troublesome potential shifts in operation. The dynode currents must therefore be small compared to the total current I_b (which flows through the voltage divider only when the cathode is in complete darkness). If this condition is not fulfilled, large dynode currents will have a serious decreasing effect on the dynode voltages between the last stages.
- 3.2.1 In continuous operation, a first approximation for the relative variation of the gain with a varying illumination of the cathode is:

$$\frac{\Delta G}{G} \approx \frac{I_{k}}{I_{b}} \left[\delta^{n} - \frac{\delta^{n+1}}{(n+1)(\delta^{-1})} \right] \approx \frac{I_{a}}{I_{b}} \left[1 - \frac{\delta}{(n+1)(\delta^{-1})} \right]$$

So the relative change in gain is approximately proportional to the ratio of the anode current to the divider current. For example, to maintain the gain stable within 1% when measuring continuous luminous flux, the current in the voltage divider should be at least 100 times the anode current.

3.2.2 In pulsed operation, as in scintillation counting, the fluctuations in gain can be restricted without the need for a high supply current by shunting each resistor in the divider chain with a capacitor. Since the former dynodes carry a very much lower current than the following ones, it is sufficient in practice to bypass the last three or four stages only. The capacitors should be chosen according to the following relationship:

where C_n = capacitor across resistor feeding last dynode C_{n-1} = capacitor across resistor feeding last dynode but one etc.

The exact calculation of the capacitively stabilised voltage divider is extremely tedious, because of the large number of parameters involved. However, with the aid of some approximations it can be shown that the relative variation of the gain is approximately:

$$\frac{\Delta G}{G} = \frac{\tau \cdot I_{a \max}}{I_{b}} \cdot \frac{e^{t/\tau} - e^{-t/RC_{n}}}{\tau - RC_{n}}$$
where τ = time constant of the scintillator
 $I_{a \max}$ = peak value of the anode current
 RC_{n} = time constant of the last stage of the voltage divider.

It follows that a peak value of the anode current of 1 mA causes a relative variation of the gain of less than 1% when the time constant RC_n is greater than 100 τ and the current in the voltage divider is at least 1 mA.

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The voltage fluctuations occurring in this arrangement are small but of long duration, so that if the count rate is high the fluctuations due to successive pulses may be partially superimposed, resulting in an error which is a function of the count rate. In the example just given, the duration of each fluctuation would be approximately 470τ and if overlapping does not occur, the count rate could not exceed $1/470\tau$ p.p.s. For a time constant of 1 μ s this corresponds to a rate of approximately 2200 p.p.s.

3.3 On no account should the tube be exposed to ambient light when the supply voltage is applied. A luminous flux of less than 10^{-5} lm is sufficient to cause the maximum permissible anode current to be exceeded. To obtain the maximum useful life from the photocathode the tube should be protected from light as far as possible even when not in use.

The dark current takes approximately 15 to 30 minutes after the application of the supply voltage to fall to a stable value. For this reason it is recommended that the equipment should be switched on half an hour before making any measurements requiring a high degree of accuracy.

The dark current may be further reduced by applying to the photocathode a jet of dry air cooled by being passed, for example, through a spiral immersed in liquid nitrogen. It is very important to ensure that no condensation occurs on the base or socket of the tube if air-cooling is adopted.


Spectral response curve type A (S11)

Fig.1



Spectral response curve type U (S13)

Fig.2



Spectral response curve type C (S1)

Fig.3



Spectral response curve type T (S20)

Fig.4





Fig.5



Spectral response curve type SB





Fig.7

LIST OF SYMBOLS

| Photocathode | k |
|--|----------------|
| Secondary emission electrode (dynode) No.n | s _n |
| Anode | а |
| Accelerating electrode | acc |
| Luminous cathode sensitivity | Nk |
| Luminous anode sensitivity | Na |
| Current amplification (Gain) | G |
| Secondary emission factor of the dynodes | δ |
| Total supply voltage | Vb |
| Anode current | Ia |
| Anode dark current | Iao |
| Cathode current | ${\tt I}_k$ |
| Efficiency | η |
| Wavelength | λ |
| Internal connection. Do not use. | i.c |

RATING SYSTEM

ABSOLUTE MAXIMUM RATING SYSTEM

Absolute maximum ratings are limiting values of operating and environmental conditions applicable to any electronic device of a specified type as defined by its published data, which should not be exceeded under the worst probable conditions.

These values are chosen by the device manufacturer to provide acceptable serviceability of the device, taking no responsibility for equipment variations, environmental variations, and the effects of changes in operating conditions due to variations in the characteristics of the device under consideration and of all other electronic devices in the equipment.

The equipment manufacturer should design so that, initially and throughout life, no absolute maximum value for the intended service is exceeded with any device under the worst probable operating conditions with respect to supply voltage variation, equipment component variation, equipment control adjustment, load variations, signal variation, environmental conditions, and variations in characteristics of the device under consideration and of all other electronic devices in the equipment.

| cathode diameter (mm) | type number | number of stages | spectral response | comments |
|-----------------------------|----------------|------------------------|----------------------|--|
| mana kis lo | XP1110 | 10 | A (S11) | esployade dans and espectation |
| | XP1111 | 10 | A (S11) | flexible leads |
| | XP1113 | 6 | A (S11) | the set of the second set in the set of |
| 14 | XP1114 | 4 | A (S11) | and the second second second second |
| 14 | XP1115 | 10 | A (S11) | flexible leads, ruggedized tube |
| | XP1116 | 10 | C (S1) | ruggedized tube |
| | XP1117 | 9 | T (S20) | ruggedized tube |
| | XP1118 | 10 | U (S13) | quartz window |
| 20 | XP1180 | 10 | A (S11) | con the month and a formally in the |
| tint e de la | 150AVP | 10 | A (S11) | na al fabric perior olla acompactation |
| | 150CVP | 10 | C (S1) | names inninginpo nio ha sere sere |
| | 150UVP | 10 | U (S13) | quartz window |
| 32 | XP1010 | 10 | A (S11) | low noise type for X-ray and low |
| | 1 | | * | energy gamma ray spectrometry |
| | XP1011 | 10 | A (S11) | ruggedized tube |
| | XP1015 | 10 | A (S11) | ruggedized tube |
| * | 56AVP | 14 | A (S11) | |
| * | 56AVP/03 | 14 | A (S11) | low noise type for single-electron |
| * | 56AVP/05 | 14 | A (S11) | photon and tritium counting extended UV response, curved window of 0.5 mm thickness |
| * | 56CVP | 10 | C (S1) | |
| * | 56TVP | 14 | T (S20) | |
| 12* | 56TUVP | 14 | TU | quartz window |
| * | 56UVP | 14 | U (S13) | quartz window |
| * | XP1021 | 12 | A (S11) | coaxial outlet with an impedance of |
| Barry . | VD1000 | 10 | 11 (010) | 50 Ω |
| * | AP1023 | 12 | U (S13) | coaxial outlet with an impedance of 50.0 quartz window |
| * | XP1140 | 6 | S4 | minimum useful cathode area 25.5 x 5.9 mm ² , high current linearity |
| * | XP1141 | 7 | A (S11) | high current linearity |

SURVEY OF PHOTOMULTIPLIERS

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1

| cathode diameter (mm) | type number | number of stages | spectral response | comments |
|-----------------------------|--|----------------------------|---|--|
| | XP1000 XP1001 | 10 10 | A (S11) A (S11) | especially useful for gamma |
| 44 | XP1002 XP1003 XP1004 XP1005 | 10 10 10 10 | T (S20) TU U (S13) C (S1) | quartz window quartz window |
| 63.5 | XP1030 XP1031 XP1032 XP1033 | 10 10 10 10 | A (S11) A (S11) U (S13) U (S13) | especially useful for gamma spectrometry quartz window of 3 mm thickness quartz window of 10 mm thickness |
| 110 * * | 54AVP 54UVP 58AVP 58UVP XP1040 | 11 11 14 14 14 | A (S11) U (S13) A (S11) U (S13) A (S11) | quartz window curved window, delivered with an acrylic-resin plano-concave adaptor and metal envelope curved quartz window plane outer window, metal envelope |
| 200 | 57AVP 60AVP | 11 12 | A (S11) A (S11) | delivered with an acrylic-resin adaptor |

* Very fast tubes designed especially for fast-coincidence techniques in nuclear physics, having an extremely low spread in transit time. They are capable of delivering anode pulses with a rise time of 2×10^{-9} s or even less. To take full advantage of this characteristic they are designed as high-gain, high-current types, thus permitting very high and steep pulses to be extracted from the anode with a 100 Ω or 50 Ω matched coaxial cable as a load.

SURVEY OF PHOTOMULTIPLIERS (continued)

Windowless Photomultipliers

| 1. | XP1120 XP1121 | Ni cathode for Photon counting (uv, X-ray) CuBeO cathode for ion detection (electrons, ions) |
|----|------------------|---|
| 2. | XP1122 XP1123 | Ni cathode; cap nut adaptation CuBeO cathode; cap nut adaptation |
| 3. | XP1130 XP1131 | Ni cathode; ultra high vacuum version CuBeO cathode; ultra high vacuum version |

SELECTION CHART

WINDOWLESS PHOTOMULTIPLIERS

| type no. | XP1120 | XP1121 | XP1122 | XP1123 | XP1130 | XP1131 |
|-----------------------------------|--|--|---|--|--|---|
| application | X -rays ($\lambda > 2 A$) uv photons ($\lambda < 1500 A$) | ions (>10 keV) electrons (0.1-10 keV) | X -rays ($\lambda > 2^{*}A$) uv photons ($\lambda < 1500 A$) | ions (>10 keV) electrons (0.1-10 keV) | uh vac. X-rays $(\lambda > 2 A)$ uv photons $(\lambda < 1500 A)$ | uh vac. ions (>10 keV) electrons (0.1-10 keV) |
| cathode | Ni | Cu Be | Ni | Cu Be | Ni | Cu Be |
| vacuum during operation (mmHg) | $10^{-5} - 10^{-6}$ | 10^5 - 10^6 | 10 ⁻⁵ - 10 ⁻⁶ | 10-2 - 10-6 | $10^{-5} - 10^{-10}$ | 10^5 - 10^-10 |
| mounting | flange O-ring | flange O-ring | cap nut O-ring | cap nut O-ring | heavy flange gold foil | heavy flange gold foil |
| envelope | glass | glass | glass | glass | stainless steel | stainless steel |
| screen | nickel plated iron | nickel plated iron | nickel plated iron | nickel plated iron | 1 | |

RECOMMENDED ACCESSORIES

1

| Sc | ocket . | Mu-metal shield | Type | Socket | Mu-metal shield |
|--------|---------|-----------------|----------------------------|-------------------|-----------------|
| FE | 31001 | 56128 | XP1140 | FE1001 | 56128 |
| FE | 10013 | 56128 | XP1141 | FE1001 | 56130 |
| FE | 10013 | 56128 | XP1180 | B8 700 67 | 56138 |
| FE | 10013 | 56128 | 53AVP | FE1001 | 56128 |
| FE | 10013 | 56128 | 53UVP | FE1001 | 56128 |
| FE | 10013 | 56128 | 54AVP | FE1001 | 56129 |
| FE | 31002 | 56127 | 54UVP | FE1001 | 56129 |
| FE | 31002 | 56127 | 56AVP | FE1003 | 56130 |
| FE | 31002 | 56127 | 56AVP/03 | FE1003 | 56130 |
| FE | 1003 | 56130 | 56AVP/05 | FE1003 | 56130 |
| FE | 31003 | 56130 | 56CVP | FE1003 | 56130 |
| FE | 31003 | 56130 | 56TUVP | FE1003 | 56130 |
| FE | 10013 | 56135 | 56TVP | FE1003 | 56130 |
| FE | 10012 | 56135 | 56UVP | FE1003 | 56130 |
| FE | 10013 | 56135 | 57AVP | FE1001 | 56132 |
| Η Η | 31001 | 56135 | 58AVP | FE1003 | 56133* |
| FE | 31003 | 56133* | 58UVP | FE1003 | 56133 |
| 56 | 073 | 56134 | 60AVP | FE1003 | 56132 |
| | 1 | 56134 | 150AVP | FE1002 | 56127 |
| .ou | val | | 150CVP | FE1002 | 56127 |
| .ou | val | | 150UVP | FE1002 | 56127 |
| | 1 | 56134 | 153AVP | FE1001 | 56128 |
| 560 | 073 | 56134 | | | |
| 56 | 073 | 56134 | HOME AND AND A CONTRACT OF | | |
| 56 | 073 | 56134 | * Without met: | al container: typ | pe 56129 |

| Type No. | Inside diameter (mm) | Length (mm) | Wall thickness (mm) |
|----------|-------------------------|----------------|------------------------|
| 56127 | 42 + 1 | 90 ± 1 | 1 |
| 56128 | 57 + 1 | 90 ± 1 | 1 |
| 56129 | 132 + 1 | 150 ± 1 | 1 |
| 56130 | 57 + 1 | 110 ± 1 | 1 |
| 56131 | 75 + 1 | 110 ± 1 | 1 |
| 56132 | 240 + 1 | 300 ± 1 | 1 |
| 56133 | 145 + 1 | 250 ± 1 | 1 |
| 56134 | 21 + 1 | 80 <u>+</u> 1 | 1 |
| 56135 | 78 + 1 | 130 <u>+</u> 1 | 1 |
| 56136 | 28 + 1 | 110 ± 1 | 1 |
| 56138 | 28 + 1 | 80 <u>+</u> 1 | 1 |

DIMENSIONS OF MU-METAL CYLINDERS

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10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in applications such as scintillation counting of alpha, beta, gamma, neutron radiation and X-rays and different kinds of optical instruments.

| QUICK REFERENCE DATA | |
|-------------------------------------|--------------|
| Spectral response | type A (S11) |
| Useful diameter of the photocathode | 44 mm |
| Anode sensitivity (at 1800 V) | 700 A/lm |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 14-pin (Jedec B14-38)





ACCESSORIES

Socket

Mu-metal shield

| type | FE1001 |
|------|--------|
| type | 56128 |

| GENERAL | | | | |
|--|-------------------|-------------|----------------|----------------|
| Photocathode | | | | |
| Description | semi-transparent, | head-or | n, flat | surface |
| Cathode material | | (| Cs-Sb | |
| Minimum useful diameter | | | 44 | mm |
| Spectral response curve 1) | | type . | A (S11) | bai an |
| Wavelength at maximum response | | 4200 | <u>+</u> 300 | Å |
| Luminous sensitivity 2) | Nk | av. min. | 70 40 | μA/lm μA/lm |
| Radiant sensitivity at 4200 A | | | 60 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 10 | |
| Dynode material | | Ag-Mg | g-O-Cs | 3 |
| Capacitances | | | | |
| Anode to final dynode | C_a/S_{10} | | 3 | pF |
| Anode to all other electrodes | Ca | | 5 | pF |
| TYPICAL CHARACTERISTICS With voltage divider A | | | | |
| Anode sensitivity at V_b = 1800 V | Na | av. min. | 700 250 | A/lm A/lm |
| Anode dark current at N_a = 100 A/lm ³ |) I _{ao} | av. max. | 0.015 0.050 | μΑ μΑ |
| Linearity between anode pulse amplitud and input light flux | le | up to | 30 | mA |
| | | | | |

 1) See spectral response curve in front of this section

 $^2)$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{\rm O}{\rm K}$

³) At an ambient temperature of 25 $^{\rm O}{\rm C}$

TYPICAL CHARACTERISTICS (continued) With voltage divider B Linearity between anode pulse amplitude and input light pulse up to 100 mA 4.10-9 Anode pulse rise time at $V_b = 1500 \text{ V}^{-1}$ S Transit time difference between the the centre of the photocathode and the edge at V_b = 1500 V 4.10^{-9} S 40.10^{-9} Total transit time at V_b = 1500 V S LIMITING VALUES (Absolute max. rating system)

| Supply voltage | Vb | max. | 1800 | V |
|---|--------------------|--------------|------------|--------|
| Continuous anode current | Ia | max. | 1 | mA |
| Voltage between cathode and first dynode | v _{k/S1} | max. min. | 500 120 | v v |
| Voltage between consecutive dynodes | $v_{S_n/S_{n+1}}$ | max. min. | 300 80 | v v |
| Voltage between anode and final dynode ²) | v _{a/S10} | max. min. | 300 80 | v v |

RECOMMENDED CIRCUITS



Voltage divider type A

- 1) For an infinitely short light pulse.
- ²) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5333

RECOMMENDED CIRCUITS (continued)



Voltage divider type B

= cathode acc = accelerating electrode $S_n = dynode No.n$ = anode a

OPERATIONAL CONSIDERATIONS

k

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be sufficient.

Different kinds of voltage dividers are possible. A circuit of type A results in the highest gain of the tube at a given total voltage; a circuit of type B gives a higher current output with better time characteristics, but the total gain is less at the same total voltage.

The accelerating electrode has a separate external connection to allow adjustment for optimum photoelectron collection on the first dynode.

When pulses with high amplitudes are taken from the anode, it is useful to decouple the last stages as indicated in the circuit by means of capacitors of a few hundred pF, to avoid a voltage drop between these stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.



A



10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in applications such as gamma-ray spectrometry.

| QUICK REFERENCE D. | ATA | |
|---|---|--------------|
| Spectral response | $\sum_{i=1}^{N_{i}} e_{i} $ | type A (S11) |
| Useful diameter of the photocathode | | 44 mm |
| Anode sensitivity (at 1800 V) | | 700 A/lm |
| Energy resolution for 0.661 -Mev Cs 137 line | | 8.5 % |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 14-pin (Jedec B14-38)



ACCESSORIES

Socket

Mu-metal shield

type FE1001 type 56128

| GENERAL | | | | |
|---|-------------------|-----------------|--------------|----------------|
| Photocathode | | | | |
| Description sen | ni-transparent, | head-on, | flat | surface |
| Cathode material | | C | s-Sb | |
| Minimum useful diameter | | | 44 | mm |
| Spectral response curve 1) | No. and a star | type A | (S11) | |
| Wavelength at maximum response | | 4200 <u>+</u> | 300 | Å |
| Luminous sensitivity 2) | Nk | av. min. | 80 70 | μA/lm μA/lm |
| Radiant sensitivity at 4200 Å | | | 65 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 10 | |
| Dynode material | | Ag-Mg- | ·O-Ca | 3 |
| Capacitances | 6.3 | | | |
| Anode to final dynode | $C_{a/S_{10}}$ | | 3 | pF |
| Anode to all other electrodes | Ca | | 5 | pF |
| TYPICAL CHARACTERISTICS | | | | |
| Anode sensitivity at V_b = 1800 V | Na | av. min. | 700 400 | A/lm A/lm |
| Anode dark current at N _a = 100 A/lm 3) | Iao | av. 0 max. 0 | .015 .050 | μΑ μΑ |
| Energy resolution for 0.661-Mev Cs^{137} lin | ae ⁴) | av. max. | 8.5 9.0 | % % |
| Linearity between anode pulse amplitude and input light flux | | up to | 30 | mA |

 1) See spectral response curve in front of this section

²) Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{\rm O}{\rm K}$

³) At an ambient temperature of 25 $^{\circ}C$

 $^4)$ Measured with a 1.5" x 1" $\rm N_aJ\ crystal$

| TYPICAL CHARACTERISTICS (continued) | | |
|---|--------------------|---|
| Anode pulse rise time at V_b = 1500 V ¹) | 4.10 ⁻⁹ | s |
| Transit time difference between the centre of the photocathode and the edge at V_b = 1500 V | 4.10 ⁻⁹ | s |
| Total transit time at V_b = 1500 V | 40.10-9 | s |
| | | |

LIMITING VALUES (Absolute max. rating system)

| Supply voltage | Vb | max. | 1800 | V | |
|---|-----------------------------------|--------------|------------|--------|--|
| Continuous anode current | I _a | max. | 1 | mA | |
| Voltage between cathode and first dynode | v _{k/S1} | max. min. | 500 120 | v v | |
| Voltage between consecutive dynodes | vs _n /s _{n+1} | max. min. | 300 80 | V V | |
| Voltage between anode and final dynode ²) | V _{a/S10} | max. | 300 | V V | |

RECOMMENDED CIRCUIT



acc = accelerating electrode a

¹) For an infintely short light pulse.

²⁾ When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5337

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be a practical value.

The best results in γ -ray spectrometry will be achieved with a voltage of 4-times "V_S" between the cathode and the first dynode; however, the limiting values must not be exceeded. At a high tension of about 1100 V the tube will work most favourably.

The accelerating electrode has a separate external connection to allow adjustment for optimum photoelectron collection on the first dynode.

At high pulse amplitudes it is useful to decouple the last stages.

When the tube has been exposed to full daylight just before mounting it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.



A



10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in laser technics, working in the orange and green range and for photometry where a high sensitivity in the whole visible region is required.

| QUICK REFERENCE DATA | | | | |
|-------------------------------------|--------------|--|--|--|
| Spectral response | type T (S20) | | | |
| Useful diameter of the photocathode | . 44 mm | | | |
| Anode sensitivity (at 1800 V) | 400 A/lm | | | |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 14-pin (Jedec 14-38)







Socket

Mu-metal shield

type FE1001 type 56128

| GENERAL | | | | |
|--|--------------------|----------------|----------------|----------------|
| Photocathode | | | | |
| Description | semi-transparent, | head-on | , flat | surface |
| Cathode material | | Sb-K-I | Na-Cs | |
| Minimum useful diameter | | | 44 | mm |
| Spectral response curve 1) | | type 7 | (S20) | 1.15 |
| Wavelength at maximum response | | 4200 - | <u>+</u> 300 | Å |
| Luminous sensitivity ²) | Nk | av. min. | 150 110 | μA/lm μA/lm |
| Radiant sensitivity at 4200 $\hbox{\AA}$ | | | 70 | mA/W |
| at 7000 Å | | | 12 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 10 | |
| Dynode material | | Ag-Mg | -0-Cs | 3 |
| Capacitances | | | | |
| Anode to final dynode | C _{a/S10} | | 3 | pF |
| Anode to all other electrodes | C _a | | 5 | pF |
| TYPICAL CHARACTERISTICS | | | | |
| With voltage divider A | | | | |
| Anode sensitivity at V_b = 1800 V | Na | av. min. | 400 100 | A/lm A/lm |
| Anode dark current at $N_a = 60 \text{ A/lm}^3$) | I _{ao} | av. (max.(|).015).050 | μΑ μΑ |
| Linearity between anode pulse amplitud and input light flux | le | up to | 30 | mA |
| | | | | |

1) See spectral response curve in front of this section

 $^2\)$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^0\mbox{K}$

 3) At an ambient temperature of 25 $^{\rm o}{\rm C}$

| TYPICAL CHARACTERISTICS (continued) | | |
|---|---------------------|----|
| With voltage divider B | | |
| Linearity between anode pulse amplitude and input light pulse | up to 100 | mA |
| Anode pulse rise time at V _b = 1500 V 1) | 4.10 ⁻⁹ | s |
| Transit time difference between the centre of the photocathode and the edge at V_b = 1500 V | 4.10 ⁻⁹ | S |
| Total transit time at V_b = 1500 V | 40.10 ⁻⁹ | s |
| LIMITING VALUES (Absolute max. rating system) | | |

| Supply voltage | Vb | max. | 1800 | V |
|---|-------------------|--------------|------------|--------|
| Continuous anode current | Ia | max. | 1 | mA . |
| Voltage between cathode and first dynode | v _{k/S1} | max. min. | 500 180 | V V |
| Voltage between consecutive dynodes | $v_{S_n/S_{n+1}}$ | max. min. | 300 80 | V V |
| Voltage between anode and final dynode ²) | $v_{a/S_{10}}$ | max. min. | 300 80 | V V |

RECOMMENDED CIRCUITS



Voltage divider type A

- ¹) For an infinitely short light pulse.
- ²) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5341

RECOMMENDED CIRCUITS (continued)



Voltage divider type B

| k | = | cathode | Sn | = | dynode No.n |
|-----|---|------------------------|----|---|-------------|
| acc | = | accelerating electrode | а | = | anode |

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be sufficient.

Different kinds of voltage dividers are possible. A circuit of type A results in the highest gain of the tube at a given total voltage; a circuit of type B gives a higher current output with better time characteristics, but the total gain is less at the same total voltage.

When pulses with high amplitudes are taken from the anode, it is useful to decouple the last stages as indicated in the circuit by means of capacitors of a few hundred pF, to avoid a voltage drop between these stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.





10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in laser technics, and photometry where a high sensitivity in the whole visible and ultraviolet region is required.

| QUICK REFERENCE DATA | | | | | | |
|-------------------------------------|------------------------|--|--|--|--|--|
| Spectral response | type TU (extended S20) | | | | | |
| Window material | quartz | | | | | |
| Useful diameter of the photocathode | 44 mm | | | | | |
| Anode sensitivity (at 1800 V) | 400 A/lm | | | | | |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 14-pin (Jedec B14-38)



ACCESSORIES

SockettypeFE1001Mu-metal shieldtype561287Z2 5390

| GENERAL | | | | |
|---|-----------------|----------------|--------------|----------------|
| Photocathode | | | | |
| Description semi | i-transparent, | head-on | , flat | surface |
| Cathode material | | Sb-K-N | la-Cs | |
| Minimum useful diameter | | | 44 | mm |
| Spectral response curve ¹) | | type T | (S20) | |
| Wavelength at maximum response | | 4200 - | <u>+</u> 300 | A |
| Luminous sensitivity ²) | Nk | av. min. | 150 110 | μA/lm μA/lm |
| Radiant sensitivity at 4200 Å | | | 70 | mA/W |
| at 7 000 Å | | | 12 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 10 | |
| Dynode material | | Ag-Mg | -0-Cs | 3 |
| Capacitances | | | | |
| Anode to final dynode | $C_{a/S_{10}}$ | | 3 | pF |
| Anode to all other electrodes | Ca | | 5 | pF |
| TYPICAL CHARACTERISTICS | | | | |
| With voltage divider A | | | | |
| Anode sensitivity at V_b = 1800 V | Na | av. min. | 400 100 | A/lm A/lm |
| Anode dark current at $N_a = 60 \text{ A/lm}^3$) | I _{ao} | av. 0 max.0 | .015 | μΑ μΑ |
| Linearity between anode pulse amplitude and input light flux | | up to | 30 | mA |
| | | | | |

1) See spectral response curve in front of this section

 $^2)$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^0\mathrm{K}$

 3) At an ambient temperature of 25 $^{\mathrm{o}}\mathrm{C}$
300 V

80 V

max.

min.

Va/S10

| TYPICAL CHARACTERISTICS (continued) | | | andres | 1.114 |
|---|-------------------|--------------|--------------------|--------|
| With voltage divider B | | | | |
| Linearity between anode pulse amplitude and input light pulse | | up to | 100 | mA |
| Anode pulse rise time at V_b = 1500 V $^{\rm l})$ | | 4. | . 10 ⁻⁹ | s |
| Transit time difference between the centre of the photocathode and the edge at $V_b = 1500 V$ | | 4. | .10-9 | S |
| Total transit time at V_b = 1500 V | | 40. | . 10 ⁻⁹ | s |
| LIMITING VALUES (Absolute max. rating sy | vstem) | | | |
| Supply voltage | Vb | max. | 1800 | V |
| Continuous anode current | Ia | max. | 1 | mA |
| Voltage between cathode and first dynode | v _{k/s1} | max. min. | 500 180 | V V |
| Voltage between consecutive dynodes | $V_{S_n/S_{n+1}}$ | max. | 300 80 | V V |

Voltage between anode and final dynode 2)

RECOMMENDED CIRCUITS



Voltage divider type A

¹) For an infinitely short light pulse

²) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5392

RECOMMENDED CIRCUITS (continued)



Voltage divider type B

| k | = | cathode | Sn | = | dynode No.n |
|-----|---|------------------------|----|---|-------------|
| acc | = | accelerating electrode | а | = | anode |

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be sufficient.

Different kinds of voltage dividers are possible. A circuit of type A results in the highest gain of the tube at a given total voltage; a circuit of type B gives a higher current output with better time characteristics, but the total gain is less at the same total voltage.

When pulses with high amplitudes are taken from the anode, it is useful to decouple the last stages as indicated in the circuit by means of capacitors of a few hundred pF, to avoid a voltage drop between these stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.





10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in optical spectrometry, ultraviolet photometry and other applications which require a good sensitivity in the ultraviolet region.

| QUICK REFERENCE DATA | |
|-------------------------------------|--------------|
| Spectral response | type U (S13) |
| Useful diameter of the photocathode | 44 mm |
| Anode sensitivity (at 1800 V) | 700 A/lm |

DIMENSIONS AND CONNECTIONS

Base: 14-pin (Jedec B14-38)





Dimensions in mm

ACCESSORIES

SZ

SE

S5

S4

S3

Socket

Mu-metal shield

type FE1001 type 56128

7Z2 5343

| GENERAL | | | | |
|--|-------------------|----------------|------------|----------------|
| Photocathode | | | | |
| Description | semi-transparent, | head-on, | flat | surface |
| Cathode material | | С | s-Sb | |
| Minimum useful diameter | | | 44 | mm |
| Spectral response curve 1) | | type U | (S13) | - |
| Wavelength at maximum response | | 4000 <u>+</u> | 300 | Å |
| Luminous sensitivity 2) | Nk | av. min. | 70 40 | μA/lm μA/lm |
| Radiant sensitivity at 4000 Å | | | 60 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 10 | |
| Dynode material | | Ag-Mg- | -0-Cs | 5 |
| Capacitances | | | | |
| Anode to final dynode | Ca/S10 | | 3 | pF |
| Anode to all other electrodes | C _a | | 5 | pF |
| TYPICAL CHARACTERISTICS | | | | |
| With voltage divider A | | | | |
| Anode sensitivity at V_b = 1800 V | Na | av. min. | 700 250 | A/lm A/lm |
| Anode dark current at $N_a = 100 \text{ A/lm}^3$ |) I _{ao} | av. 0 max.0 | .015 | μΑ μΑ |
| Linearity between anode pulse amplitud and input light flux | le | up to | 30 | mA |

 $^{1})$ See spectral response curve in front of this section

 $^2\)$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^0\ensuremath{\mathrm{K}}$

³) At an ambient temperature of 25 °C

7Z2 5344

300 V

300 V

80 V

80

V

max.

min.

max.

min.

 $v_{S_n/S_{n+1}}$

v_{a/S10}

| TYPICAL CHARACTERISTICS (continued) | | | |
|---|-------------------|--------------------|--------|
| With voltage divider B | | | |
| Linearity between anode pulse amplitude and input light pulse | | upto 100 | mA |
| Anode pulse rise time at V_b = 1500 V 1) | | 4.10-9 | s |
| Transit time difference between the centre of the photocathode and the edge at V_b = 1500 V | | 4.10 ⁻⁹ | S |
| Total transit time at V_b = 1500 V | | 40.10-9 | s |
| LIMITING VALUES (Absolute max. rating sy | /stem) | | |
| Supply voltage | Vb | max. 1800 | v |
| Continuous anode current | Ia | max. 1 | mA |
| Voltage between cathode and first dynode | V _{k/S1} | max. 500 | V V |

Voltage between consecutive dynodes

Voltage between anode and final dynode 2)

RECOMMENDED CIRCUITS



Voltage divider type A

- ¹) For an infinitely short light pulse.
- ²) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5345

RECOMMENDED CIRCUITS (continued)



Voltage divider type B

| k | = | cathode | Sn | = | dynode No.n |
|-----|---|------------------------|----|---|-------------|
| acc | = | accelerating electrode | а | = | anode |

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be sufficient.

Different kinds of voltage dividers are possible. A circuit of type A results in the highest gain of the tube at a given total voltage; a circuit of type B gives a higher current output with better time characteristics, but the total gain is less at the same total voltage.

The accelerating electrode has a separate external connection to allow adjustment for optimum photoelectron collection on the first dynode.

When pulses with high amplitudes are taken from the anode, it is useful to decouple the last stages as indicated in the circuit by means of capacitors of a few hundred pF, to avoid a voltage drop between these stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.



A



10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in applications such as infra-red telecommunication and ranging and in optical instruments operating in the far red and near infra-red region.

| QUICK REF | ERENCE DATA | | |
|-------------------------------------|--|------|--------|
| Spectral response | The second s | type | A (S1) |
| Useful diameter of the photocathode | | 44 | mm |
| Anode sensitivity (at 1800 V) | | 100 | A/lm |

DIMENSIONS AND CONNECTIONS

Base: 14-pin (Jedec B14-38)



ACCESSORIES

Socket

Mu-metal shield

| type | FE1001 |
|------|--------|
| type | 56128 |

Dimensions in mm

7Z2 7833

| GENERAL | | | | |
|--|-------------------|---------------|-----------|----------------|
| Photocathode | | | | |
| Description | semi-transparent, | head-on | , flat | surface |
| Cathode material | | Ag- | O-Cs | |
| Minimum useful diameter | | | 44 | mm |
| Spectral response curve 1) | | type C | C (S1) | |
| Wavelength at maximum response | | 8000 <u>+</u> | 1000 | Å |
| Luminous sensitivity ²) | Nk | av. min. | 20 15 | μA/lm μA/lm |
| Infra-red luminous sensitivity ³) | Nk | av. min. | 3 1.4 | μA/lm μA/lm |
| Radiant sensitivity at 8000 Å | | | 2 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 10 | |
| Dynode material | | ' Ag-Mg | -0-Cs | 5 |
| Capacitances | | | | |
| Anode to final dynode | $C_{a/S_{10}}$ | | 3 | pF |
| Anode to all other electrodes | C _a | | 5 | pF |
| TYPICAL CHARACTERISTICS | | | | |
| With voltage divider A | | | | |
| Anode sensitivity at V _b = 1800 V | Na | av. min. | 100 20 | A/lm A/lm |
| Anode dark current at $N_a = 20 \text{ A/lm}^4$) | I _{ao} | max. | 10 | μΑ |
| Linearity between anode pulse amplitud and input flux | le | up to | 5 | mA |
| | | | | |

1) See spectral response curve in front of this section

 2) Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{
m o}$ K

³) The infra-red lumen is the flux resulting from one lumen yielded by a tungsten ribbon lamp (colour temperature 2851 ^oK) going through an infra-red filter corning CS94 No.2540, fusion 1613 thickness 2.61

4) At an ambient temperature of 25 °C

TYPICAL CHARACTERISTICS (continued) With voltage divider B Linearity between anode pulse amplitude and input light pulse up to 10 mA 4.10^{-9} Anode pulse rise time at $V_b = 1500 \text{ V}^{-1}$) S Transit time difference between the centre of the photocathode and the edge at V_b = 1500 V 4.10-9 S 40.10-9 Total transit time at V_b = 1500 V S

LIMITING VALUES (Absolute max. rating system)

| Supply voltage | Vb | max. l | 800 | V |
|---|--------------------|--------------|------------|--------|
| Continuous anode current | Ia | max. | 30 | μA |
| Voltage between cathode and first dynode | v _{k/S1} | max. min. | 500 120 | v v |
| Voltage between consecutive dynodes | $v_{S_n/S_{n+1}}$ | max. min. | 300 80 | v v |
| Voltage between anode and final dynode ²) | V _{a/S10} | max. min. | 300 80 | V V |

RECOMMENDED CIRCUITS



Voltage divider type A

- 1) For an infintely short light pulse.
- ²) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5349

RECOMMENDED CIRCUITS (continued)



Voltage divider type B

S_n = dynode No.n a = anode

OPERATIONAL CONSIDERATIONS

= cathode

acc = accelerating electrode

k

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be sufficient.

Different kinds of voltage dividers are possible. A circuit of type A results in the highest gain of the tube at a given total voltage; a circuit of type B gives a higher current output with better time characteristics, but the total gain is less at the same total voltage.

The accelerating electrode has a separate external connection to allow adjustment for optimum photoelectron collection on the first dynode.

When pulses with high amplitudes are taken from the anode, it is useful to decouple the last stages as indicated in the circuit by means of capacitors of a few hundred pF, to avoid a voltage drop between these stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.



A



10 STAGE PHOTOMULTIPLIER TUBE

This low noise tube is intended for use in applications such as X- and $\gamma\text{-ray}$ spectrometry.

| QUICK REFERENCE | DATA | |
|--|-----------|------|
| Spectral response | type A (| S11) |
| Useful diameter of the photocathode | 32 m | nm |
| Anode sensitivity (at 1800 V) | 700 A | A/lm |
| Plateau length (Mn, K_{α} line 5.9 keV) | min. 70 V | 7 |
| Plateau slope | max. 0.08 | %/V |
| Background in middle of plateau | 10 c | /sec |

incident radiation

DIMENSIONS AND CONNECTIONS

S10

9C

7703932

Dimensions in mm

Base: 12-pin (Jedec B12-43)





ACCESSORIES

S

SI

ac

Socket

Mu-metal shield

type FE1002 type 56127

7Z2 5602

GENERAL

| Photocathode | | | | |
|---|-------------------|---------------|----------------|----------------|
| Description | semi-transparent, | head-or | n, flat | surface |
| Cathode material | | C | ls-Sb | |
| Minimum useful diameter | | | 32 | mm |
| Spectral response curve ¹) | | type 1 | A (S11) | nak di |
| Wavelength at maximum response | | 4200 | ± 300 | Å |
| Luminous sensitivity ²) | Nk | av. min. | 80 70 | μA/lm μA/lm |
| Radiant sensitivity at 4200 Å | | | 65 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 10 | |
| Dynode material | | Ag-Mg | ;-0-Cs | 5 |
| Capacitances | | | | |
| Anode to final dynode | C_a/S_{10} | | 3 | pF |
| Anode to all other electrodes | Ca | | 5 | pF |
| TYPICAL CHARACTERISTICS | | | | |
| Anode sensitivity at V_b = 1800 V | Na | av. min. | 700 400 | A/lm A/lm |
| Anode dark current at N _a = 60 A/lm 3) | I _{ao} | av. max. (|).010).050 | μΑ μΑ |
| Linearity between anode pulse amplitud and input light pulse | e | up to | 30 | mA |
| | | | | |

1) See spectral response curve in front of this section

2) Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{\rm O}{\rm K}$

3) At an ambient temperature of 25 $^{\rm O}{\rm C}$

7Z2 5603

2

TYPICAL CHARACTERISTICS (continued)

| Plateau length (Mn, K $_{lpha}$ line 5.9 KeV) 1) | min. | 70 | V |
|--|-------------|----------|----------|
| Plateau slope ¹) | max. | 0.08 | %/V |
| Background in middle of plateau ¹) | av. max. | 10 50 | Hz Hz |
| Total voltage in middle of plateau | | 1100 | V |
| Energy resolution for Cu, K_{α} (8 KeV) | * | 50 | % |

LIMITING VALUES (Absolute max. rating system)

| Supply voltage | Vb | max. | 1800 | V |
|---|----------------------|--------------|------------|--------|
| Continuous anode current | Ia | max. | 1 | mA |
| Voltage between cathode and first dynode | v_{k/S_1} | max. min. | 500 120 | V V |
| Voltage between consecutive dynode | V _{Sn/Sn+1} | max. min. | 300 80 | V V |
| Voltage between anode and final dynode 2) | $V_{a/S_{10}}$ | max. min. | 300 80 | V V |

RECOMMENDED CIRCUIT



 Measured with a 32 mm x 1 mm NaI crystal, at a counting rate of about 2500 Hz in the middle of the plateau, and with the discriminator bias set at 0.7 V. Preamplifier gain 250 x (source 100 μC Fe⁵⁵).

2) When caluclating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 7834

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be sufficient.

When pulses with high amplitudes are taken from the anode, it is useful to decouple the last stages as indicated in the circuit by means of capacitors of a few hundred pF, to avoid a voltage drop between these stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.





10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for scintillation counting and optical measurements under severe operating conditions. Its rugged construction makes it particularly suitable for geophysical and astronomical missile experiments.

| QUICK REFERENCE DATA | |
|-------------------------------------|--------------|
| Spectral response | type A (S11) |
| Useful diameter of the photocathode | 32 mm |
| Anode sensitivity (at 1800 V) | 700 A/lm |
| Shock | 30 g |

DIMENSIONS AND CONNECTIONS

Base: 12-pin (Jedec B12-43)





Dimensions in mm

ACCESSORIES

S

acc

7703932

Socket

Mu-metal shield

type FE1002 type 56127

7Z2 5606

| GENERAL | | | |
|--|--------------------|-------------------|----------------|
| Photocathode | | | |
| Description | semi-transparent, | head-on, flat | surface |
| Cathode material | | Cs-Sb | |
| Minimum useful diameter | | 32 | mm |
| Spectral response curve ¹) | | type A (S1 | 1) |
| Wavelength at maximum response | | 4200 <u>+</u> 300 | A |
| Luminous sensitivity 2) | Nk | av. 60 min. 35 | μA/lm μA/lm |
| Radiant sensitivity at 4200 Å | | 50 | mA/W |
| Multinlier system | | | |
| Number of stages | | 10 | |
| Durada matarial | | | |
| Dynode material | | Ag - Mg - O-C | -5 |
| Capacitances | | | |
| Anode to final dynode | C _{a/S10} | 3 | pF |
| Anode to all other electrodes | Ca | 5 | pF |
| TYPICAL CHARACTERISTICS | | | |
| Shock | | | |
| Shape of shock pulses | | half-wave sin | nusoidal |
| Peak acceleration | | 30 ± 3 | g |
| Duration | | 11 | ms |
| Number of shocks in each of 3 orthogon | al axes | 6 | |
| Vibration | | | |
| Shape | | sinusoidal | |
| Acceleration for 5- 14 Hz | | 0.5 | g |
| 14- 400 Hz | | 5 | g |
| Duration in each of 3 orthogonal axes | | 25 | g min. |
| | | | |

 $^{1}\ensuremath{)}$ See spectral response curve in front of this section

 $^2\)$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{\rm O}\rm K$

| TYPICAL CHARACTERISTICS (continued) | | | | |
|---|-------------------|----------------------|-------------------|--------------|
| With voltage divider A | | | | |
| Anode sensitivity at V_b = 1800 V | Na | av. min. | 700 100 | A/lm A/lm |
| Anode dark current at $N_a = 60 \text{ A/lm}^{-1}$) | I _{ao} | av. m ax . | 0.010 0.050 | μΑ μΑ |
| Linearity between anode pulse amplitude and input light pulse | | up to | 30 | mA |
| With voltage divider B | | | | |
| Linearity between anode pulse amplitude and input light pulse | | up to | 100 | mA |
| Anode pulse rise time at V _b = 1500 V ²) | | 4 | .10-9 | s |
| Transit time difference between the centre of the photocathode and the edge at V_b = 1500 V | | 3 | .10 ⁻⁹ | S |
| Total transit time at V_b = 1500 V | | 36 | .10-9 | S |
| LIMITING VALUES (Absolute max. rating s | system) | | | |
| Supply voltage | Vb | max. | 1800 | v |
| Continuous anode current | Ia | max. | 1 | mA |
| Voltage between cathode and first dynode | v_{k/S_1} | max. min. | 500 120 | v v |
| Voltage between consecutive dynodes | $v_{s_n/s_{n+1}}$ | max. min. | 300 80 | v v |
| Voltage between anode and final dynode ³) | $v_{a/S_{10}}$ | max. min. | 300 . 80 | v v |

 $^{\rm l})$ At an ambient temperature of 25 $^{\rm o}C.$

2) For an infinitely short light pulse.

³) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5608

RECOMMENDED CIRCUITS



Voltage divider type A



Voltage divider type B

| k | = | cathode | Sn | Ξ | dynode No.n |
|-----|---|------------------------|----|---|-------------|
| acc | = | accelerating electrode | а | = | anode |

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be sufficient.

Different kinds of voltage dividers are possible. A circuit of type A results in the highest gain of the tube at a given total voltage; a circuit of type B gives a higher current output with better time characteristics, but the total gain is less at the same total voltage.

When pulses with high amplitudes are taken from the anode, it is useful to decouple the last stages as indicated in the circuit by means of capacitors of a few hundred pF, to avoid a voltage drop between these stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.

7Z2 5610



A

10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for scintillation counting and optical measurements under severe operating conditions. Its rugged construction makes it particularly suitable for geophysical and astronomical missile experiments.

| QUICK REFERENCE DATA | | | | |
|-------------------------------------|--------------|--|--|--|
| Spectral response | type A (S11) | | | |
| Useful diameter of the photocathode | 32 mm | | | |
| Anode sensitivity (at 1800 V) | 700 A/lm | | | |
| Shock | 30 g | | | |

DIMENSIONS AND CONNECTIONS

Dimensions in mm



XP1015 XP1015C

| GENERAL | | | |
|--|-------------------|-------------------|----------------|
| Photocathode | | | |
| Description | semi-transparent, | head-on, flat | surface |
| Cathode material | | Cs-Sb | |
| Minimum useful diamter | | 32 | mm |
| Spectral response curve ¹) | | type A (S1) | 1) |
| Wavelength at maximum response | | 4200 ± 300 | 8 |
| Luminous sensitivity 2) | Nk | av. 60 min. 40 | μA/lm μA/lm |
| Radiant sensitivity at 4200 Å | | 60 | mA/W |
| Multiplier system | | | |
| Number of stages | | 10 | |
| Dynode material | | Ag-Mg-O-C | Cs |
| Capacitances | | | |
| Anode to final dynode | C_a/S_{10} | 3 | pF |
| Anode to all other electrodes | Ca | 5 | pF |
| TYPICAL CHARACTERISTICS | | | |
| Shock | | | |
| Shape of shock pulses | | half-wave sin | nusoidal |
| Peak acceleration | | 30 <u>+</u> 3 | g |
| Duration | | 11 | ms |
| Number of shocks in each of 3 orthogon | al axes | 6 | |
| Vibration | | | |
| Shape | | sinusoidal | |
| Acceleration for 5- 14 Hz 14- 400 Hz 400-2000 Hz | | 0.5 5 7.5 | g g |
| Duration in each of 3 orthogonal axes | | 25 | min. |
| ¹) See spectral response curve in front | of this section | | |

 $^2\)$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^0\mbox{K}$ 7Z2 8249

min.

max.

min. max.

min.

120 V

300 V

80 V

300 V

80

V

| TYPICAL CHARACTERISTICS (continued) | | | |
|--|-----------------|-------------------------|--------------|
| With voltage divider A | | | |
| Anode sensitivity at V_b = 1800 V | Na | av. 700 min. 100 | A/lm A/lm |
| Anode dark current at $N_a = 60 \text{ A/lm}^{-1}$) | I _{ao} | av. 0.010 max. 0.050 | μΑ μΑ |
| Linearity between anode pulse amplitude and input light pulse | | up to 30 | mA |
| With voltage divider B | | | |
| Linearity between anode pulse amplitude and input light pulse | | up to 100 | mA |
| Anode pulse rise time at V _b = 1500 V 2) | | 4.10-9 | S |
| Transit time difference between the centre of the photocathode and the edge at V _b = 1500 V | | 3.10 ⁻⁹ | S |
| Total transit time at V_b = 1500 V | | 36.10-9 | S |
| LIMITING VALUES (Absolute max. rating | system) | | |
| Supply voltage | Vb | max. 1800 | V |
| Continuous anode current | Ia | max. 1 | mA |
| | | max. 500 | V |

 $\label{eq:Voltage} Voltage \mbox{ between cathode and first dynode } V_k/S_1$

 $\label{eq:Voltage} {\rm Voltage \ between \ consecutive \ dynodes} \qquad \qquad {\rm V}_{S_n/S_{n+1}}$

Voltage between anode and final dynode ³) $V_{a/S_{10}}$

 $^{\rm l})$ At an ambient temperature of 25 $^{\rm o}C.$

2) For an infinitely short light pulse.

³) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5613

XP1015 XP1015C

RECOMMENDED CIRCUITS



Voltage divider type A



Voltage divider type B

| k | = | cathode | Sn | = | dynode No.n |
|-----|---|------------------------|----|---|-------------|
| acc | = | accelerating electrode | а | = | anode |

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be sufficient.

Different kinds of voltage dividers are possible. A circuit of type A results in the highest gain of the tube at a given total voltage; a circuit of type B gives a higher current output with better time characteristics, but the total gain is less at the same total voltage.

When pulses with high amplitudes are taken from the anode, it is useful to decouple the last stages as indicated in the circuit by means of capacitors of a few hundred pF, to avoid a voltage drop between these stages.

The semiflexible leads of the tube may be soldered into the circuit; care must be taken to conduct the heat away from the glass seals. Excessive bending of the leads is to be avoided. The tube is provided with a 12-pin base to facilitate testing. After testing, the attached base should be removed prior to installing the tube in a given system.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.

7Z2 5615

XP1015 XP1015 C



A

12 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in nuclear physics where a high degree of time definition or a high time resolution is required (fast coincidences, "time-of-flight" measurements, Cerenkov counters).

| QUICK REFERE | NCE DATA | b.c.c.ma | and a |
|-------------------------------------|----------|------------------------------|-------|
| Spectral response | artan | type A | (S11) |
| Useful diameter of the photocathode | | 42 | mm |
| Gain (at 2500 V) | | 10 ⁸ | |
| Anode pulse rise time | | < 1.8 | ns |
| Coaxial outlet | | 100 | Ω |
| Linearity | | up to 300 | mA |

DIMENSIONS AND CONNECTIONS

Dimensions in mm



 1) The tube is delivered with a coaxial cable connector LEMO 3.C 100.

7Z2 7835

MAINTENANCE TYPE

| Socket ¹) | type | FE1003 |
|--------------------------------|--------------|----------------|
| Mu-metal shield ²) | type type | 56130 56131 |

GENERAL

| Photocathode | | | | |
|--|---------------------|--------------|----------|----------------|
| Description | semi-transparent, l | nead-on, cur | ved | surface |
| Cathode material | | Cs | -Sb | |
| Minimum useful diameter | | | 42 | mm |
| Spectral response curve ³) | type A (S11) | | | |
| Wavelength at maximum response | | $4200 \pm$ | 300 | A |
| Luminous sensitivity 4) | Nk | av. min. | 65 45 | μA/lm μA/lm |
| Radiant sensitivity at 4200 $ m \AA$ | | | 55 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 12 | |
| Dynode material | Ag-Mg-O-Cs | | | |
| Capacitances | | | | |
| Grid No.1 to cathode | C_{k/g_1} | | 25 | pF |
| Grid No.1 to all other electrodes | C_{g_1} | | 30 | pF |
| Grid No.1 to grid No.2 | C_{g_1/g_2} | 2 | 17 | pF |
| Anode to final dynode | Ca/S12 | 2 | 8 | pF |
| Anode to all other electrodes | C _a | | 9 | pF |

1) The tube is delivered with a coaxial cable connector LEMO 3.C.100

²) To avoid field distortion in the electron optical input system it is advised to connect the aquadag shield (pin No.9) to the cathode. If the cathode is circuited to a negative high tension care should be taken to ensure a high tension insulation between the aquadag-shield and the mu-metal screen

 3) See spectral response curve in front of this section

4) Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{0}\mathrm{K}$ 7Z2 5476
| TYPICAL CHARACTERISTICS | | | |
|--|-----------------------------------|--------------------|--------------|
| With voltage divider A | | | |
| Supply voltage for $G = 10^8$ | v _b | av. 250 max.300 | 00 V 00 V |
| Anode dark current at G = 10^8 ¹) | I _{ao} | max. | 5 μΑ |
| Linearity between anode pulse amplitude and input light pulse | | up to 10 | 00 m.A |
| With voltage divider B | | | |
| Linearity between anode pulse amplitude and input light pulse | | up to 30 |)0 m.A |
| Anode pulse rise time at V _b = 2500 V 2) | | <1.8 10 | -9 s |
| Anode pulse width at half height at V_b = 2500 V | ²) | 4.10- | -9 s |
| Transit time difference between the centre of the photocathode and 18 mm out of the centre at V_b = 2500 V | | <0,2.10 | -9 s |
| Total transit time at 2500 V 2) | | 28.10- | -9 s |
| Maximum peak current | | 0.5 to | 1 A |
| LIMITING VALUES (Absolute max. rating syst | em) | | |
| Supply voltage ³) | Vb | max. 300 | 00 V |
| Continuous anode current | Ia | max. | 2 mA |
| Voltage between cathode and first dynode | v _{k/S1} | max. 60 min. 30 | 00 V 00 V |
| Voltage between consecutive dynodes | vs _n /s _{n+1} | max. 50 min. 8 | 00 V 30 V |
| Voltage between anode and final dynode 4) | V _{a/S12} | max. 50 min. 8 | 00 V 30 V |

- $^{\rm l})$ At an ambient temperature of 25 $^{\rm o}C.$
- 2) For an infinitely short light pulse, fully illuminating the photocathode.
- $^3)$ Or the voltage at which the tube circuited in the voltage-divider A has a gain of about $10^9,$ whichever is lowest.
- ⁴) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5477

RECOMMENDED CIRCUITS



Voltage divider type A^{1})





- k = cathode
 g1 = focusing electrode No.1
 g2 = focusing electrode No.2
 acc = accelerating electrode
- $g_3 = shadow grid$
- $S_n = dynode No.n$
- a = anode

Voltage between k and g_1 to be adjusted at about 1 Vs

Voltage between S_1 and S_2 to be adjusted at about 1.2 $\rm Vs$

Voltage between g_3 and S_{12} to be adjusted for optimum time characteristics.

1) To avoid field distortion in the electron optical input system it is advised to connect the aquadag shield (pin No.9) to the cathode. If the cathode is circuited to a negative high tension care should be taken to ensure a high tension insulation between the aquadag-shield and the mu-metal screen.

7Z2 5478

4

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of about 3 mA will be sufficient.

The last stages must be decoupled by means of capacitances to avoid a serious voltage drop on the dynodes. A practical value for C_1 could be 2.10^{-9} F. In the case of high counting rates and large peak power output, and to avoid a high-tension supply of large power, it is possible to supply the first stages with a high tension of small output and the end stages with an average voltage of high output.

A. The electron optical input system consists of five elements:

the photocathode k; the focusing electrode g_1 ; the focusing electrode g_2 ; the accelerating electrode acc; the deflector.

To reduce transit-time fluctuations, geometrical time spread, pulse amplitude spread or dark current, this system has the following advantages:

- 1. the photocathode is curved, though the outer window surface is flat, thus facilitating optical coupling;
- 2. a high and homogeneous extraction field at the cathode reduces as much as possible the influence of the initial electron velocities. A cathode-to-accelerator (internally connected to the ninth dynode) voltage of 1750 V ensures a field strength of about 200 V/cm. This field is homogenized at the cathode surface by the focusing electrode g_1 . Fig.1 shows the electron path in the input system.
- 3. The potential of electrode g_1 to the photocathode can be adjusted in order to obtain one of the following characteristics:
 - a. the most satisfactory collection (i.e. for a given luminous flux the largest obtainable anode signal); the optimum of the potential is about 1 V_s ;
 - b. the slightest transit-time fluctuations (the most homogeneous extraction field);
 - c. the most satisfactory uniformity of collection giving the most constant output amplitude.

4. Because the first dynode cannot be placed parallel to the photocathode, the beam of primary electrons is deflected by the deflector to make it impinge at right angles to the first dynode surface. Collection on the first dynode is controlled by the potential of the second dynode (see recommended circuits). 7Z2 5479

OPERATIONAL CONSIDERATIONS (continued)



Fig.1: Electron optical input system

B. The multiplier system consists of 12 stages, providing a total current amplification of 10⁸ at about 2500 V (see figures 4 and 5).

The tube is capable of producing very strong peak currents (up to 1 A). Actually the time constant at the output of the multiplier must be very small. Therefore it is necessary to use a low load resistance, well matched to the associated electronic circuitry. For this reason the tube is provided with an coaxial outlet, having a characteristic impedance of 100 Ω . With this load the tube easily delivers pulses of tens of volts, so that an amplifier is rendered superfluous, without attenuation or distortion.

To avoid the effects, which are responsible for rounding of the leading edge and the "jagged" trailing edges, a shadow grid (g_3) is placed parallel to the anode with its wires aligned with those of the anode.

Thus electrons walking from the next-to-last dynode (S11) to the last dynode (S12) are prevented to impinge directly upon the anode.

At the same time induction and oscillations in the anode grid are minimized. The potential of this electrode is to be adjusted at an optimum close to that of the last dynode. Figure 2 shows anode pulses produced by a 50 Ω version of the tube.

OPERATIONAL CONSIDERATIONS (continued)







Fig. 3 Anode sensitivity as a function of shadow grid potential

ordinate - 10 volts per major division

A further characteristic of g_3 is that it can be used as a control electrode determining the amplitude of anode pulses without the necessity of adjusting the incident light or the gain of the tube, and hence the H.V. supply. Figure 3 illustrates the control characteristics of g_3 .

It should be noted that at equal high tensions the gain of the tube is smaller for voltage divider type B than for one according to type A. (See figures 4 and 5.)

It is advisable to screen the tube with a mu-metal cylinder against magnetic field influences.



Fig.4

A



Fig.5

В



12 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in nuclear physics where a high degree of time definition or a high time resolution is required (fast coincidences, "time-of-flight" measurements, Cerenkov counters).

| QUICK REFERENCE DATA | | | |
|-------------------------------------|-----------------|-------|--|
| Spectral response | type A | (S11) | |
| Useful diameter of the photocathode | 42 | mm | |
| Gain (at 2500 V) | 10 ⁸ | | |
| Anode pulse rise time | < 1.8 | ns | |
| Coaxial outlet | 50 | Ω | |
| Linearity | up to 300 | mA | |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 20-pin (Jedec B20-102) with coaxial outlet



ACCESSORIES

| Socket | | type | FE1003 |
|--------------------------------|-----------------|--------------|----------------|
| Coaxial cable connector | "General Radio" | type | 874/C8A |
| Mu-metal shield ¹) | | type type | 56130 56131 |

GENERAL

| Photocathode | | | | |
|--|-------------------|------------|----------------|----------------|
| Description | semi-transparent, | head-on, | curved | surface |
| Cathode material | | | Cs-Sb | |
| Minimum useful diameter | | | 42 | mm |
| Spectral response curve ²) | | type | A (S1) | L) |
| Wavelength at maximum response | | 4200 |) <u>+</u> 300 | R |
| Luminous sensitivity ³) | N _k | av. min | 65 45 | μA/lm μA/lm |
| Radiant sensitivity at 4200 Å | | | 55 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 12 | |
| Dynode material | | Ag-1 | Mg-0-0 | Cs |
| Capacitances | | | | |
| Grid No.1 to cathode | C_{k/g_1} | | 25 | pF |
| Grid No.2 to all other electrodes | C _{g1} | | 30 | pF |
| Grid No.1 to grid No.2 | Cg1/8 | 52 | 17 | pF |
| Anode to final dynode | C _{a/S1} | 2 | 8 | pF |
| Anode to all other electrodes | Ca | | 9 | pF |

- 1) To avoid field distortion in the electron optical input system it is advised to connect the aquadag shield (pin No.9) to the cathode. If the cathode is circuited to a negative high tension care should be taken to ensure a high tension insulation between the aquadag-shield and the mu-metal screen.
- 2) See spectral response curve in front of this section
- $^3)$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^0\mathrm{K}$ 7Z2 5483

| TYPICAL | CHARACTERISTICS | |
|---------|-----------------|--|
|---------|-----------------|--|

| With voltage divider A | | | | |
|--|--------------------|--------------|--------------|--------|
| Supply voltage for $G = 10^8$ | Vb | av. max. | 2500 3000 | v v |
| Anode dark current at G = 10^8 ¹) | I _{ao} | max. | 5 | μA |
| Linearity between anode pulse amplitude and input light pulse | | up to | 100 | mA |
| With voltage divider B | | | | |
| Linearity between anode pulse amplitude and input light pulse | | up to | 300 | mA |
| Anode pulse rise time at V_b = 2500 V ²) | | <1,8. | 10-9 | s |
| Anode pulse width at half height at V_b = 2500 | V ²) | 4. | 10-9 | s |
| Transit time difference between the centre of the photocathode and 18 mm out of the centre at $V_{\rm b}$ = 2500 V | | < 0, 2. | 10-9 | S |
| Total transit time at V_b = 2500 V ²) | | 28. | 10-9 | s |
| Maximum peak currents | | 0.5 | 5 to 1 | A |
| LIMITING VALUES (Absolute max. rating sy | vstem) | | | |
| Supply voltage ³) | Vb | max. | 3000 | V |
| Continuous anode current | Ia | max. | 2 | mA |
| Voltage between cathode and first dynode | v_{k/S_1} | max. min. | 600 300 | V V |
| Voltage between consecutive dynodes | $v_{S_n/S_{n+1}}$ | max. min. | 500 80 | v v |
| Voltage between anode and final dynode 4) | V _{a/S12} | max. min. | 500 80 | V V |

- ¹) At an ambient temperature of 25 ^oC.
- 2) For an infinitely short light pulse, fully illuminating the photocathode.
- $^3)$ Or the voltage at which the tube circuited in the voltage-divider A has a gain of about 10^9, whichever is lowest.
- When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5484

RECOMMENDED CIRCUITS



Voltage divider type A^{1})





- k = cathode
- g_1 = focusing electrode No.1
- g₂ = focusing electrode No.2
- acc = accelerating electrode
- g₃ = shadow grid
- $S_n = dynode No.n$
- a = anode

Voltage between k and $g_1 \, \text{to}$ be adjusted at about 1 $V_{\rm S}$

Voltage between S_1 and S_2 to be adjusted at about 1.2 V_S

Voltage between g_3 and S_{12} to be adjusted for optimum time characteristics.

¹) To avoid field distortion in the electron optical input system it is advised to connect the aquadag shield (pin No.9) to the cathode. If the cathode is circuited to a negative high tension care should be taken to ensure a high tension insulation between the aquadag-shield and the mu-metal screen.

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of about 3 mA will be sufficient.

The last stages must be decoupled by means of capacitances to avoid a serious voltage drop on the dynodes. A practical value for C_1 could be 2.10^{-9} F. In the case of high counting rates and large peak power output, and to avoid a high-tension supply of large power, it is possible to supply the first stages with a high tension of small output and the end stages with an average voltage of high output.

A. The electron optical input system consists of five elements:

the photocathode k; the focusing electrode g_1 ; the focusing electrode g_2 ; the accelerating electrode acc; the deflector.

To reduce transit-time fluctuations, geometrical time spread, pulse amplitude spread or dark current, this system has the following advantages:

- 1. the photocathode is curved, though the outer window surface is flat, thus facilitating optical coupling;
- 2. a high and homogeneous extraction field at the cathode reduces as much as possible the influence of the initial electron velocities. A cathode-to-accelerator (internally connected to the ninth dynode) voltage of 1750 V ensures a field strength of about 200 V/cm. This field is homogenized at the cathode surface by the focusing electrode g_1 . Fig.1 shows the electron path in the input system.
- 3. The potential of electrode g₁ to the photocathode can be adjusted in order to obtain one of the following characteristics:
 - a. the most satisfactory collection (i.e. for a given luminous flux the largest obtainable anode signal); the optimum value of the potential is about 1 V_s;
 - b. the slightest transit-time fluctuations (the most homogeneous extraction field);
 - c. the most satisfactory uniformity of collection giving the most constant output amplitude.
- 4. Because the first dynode cannot be placed parallel to the photocathode, the beam of primary electrons is deflected by the deflector to make it impinge at right angles to the first dynode surface. Collection on the first dynode is controlled by the potential of the second dynode (see recommended circuits).

OPERATIONAL CONSIDERATIONS (continued)



Fig.1: Electron optical input system

B. The multiplier system consists of 12 stages, providing a total current amplification of 10⁸ at about 2500 V (see figures 4 and 5).

The tube is capable of producing very strong peak currents (up to 1 A). Actually the time constant at the output of the multiplier must be very small. Therefore it is necessary to use a low load resistance, well matched to the associated electronic circuitry. For this reason the tube is provided with an coaxial outlet, having a characteristic impedance of 50 Ω . With this load the tube easily delivers pulses of tens of volts, so that an amplifier is rendered superfluous, without attenuation or distortion.

To avoid the effects, which are responsible for rounding of the leading edge and the "jagged" trailing edges, a shadow grid (g_3) is placed parallel to the anode with its wires aligned with those of the anode.

Thus electrons walking from the next-to-last dynode (S11) to the last dynode (S12) are prevented to impinge directly upon the anode.

At the same time induction and oscillations in the anode grid are minimized. The potential of this electrode is to be adjusted at an optimum close to that of the last dynode. Figure 2 shows anode pulses of the tube.

OPERATIONAL CONSIDERATIONS (continued)





Fig.2 Photograph of anode pulses abscissa - 5 nanoseconds per major division



ordinate - 10 volts per major division

A further characteristic of g_3 is that it can be used as a control electrode determining the amplitude of anode pulses without the necessity of adjusting the incident light or the gain of the tube, and hence the H.V. supply. Figure 3 illustrates the control characteristics of g_3 .

It should be noted that at equal high tensions the gain of the tube is smaller for voltage divider type B than for one according to type A. (See figures 4 and 5.)

It is advisable to screen the tube with a mu-metal cylinder against magnetic field influences.



Fig.4

A





12 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in nuclear physics where a high degree of time definition or a high time resolution is required, combined with a good sensitivity in the ultraviolet region.

| QUICK REFERENCE D | DATA | |
|-------------------------------------|-----------------|-------|
| Spectral response | type U | (S13) |
| Useful diameter of the photocathode | 42 | mm |
| Gain (at 2500 V) | 10 ⁸ | |
| Anode pulse rise time | < 1.8 | ns |
| Coaxial outlet | 50 | Ω |
| Linearity | up to 300 | mA |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 20-pin (Jedec B20-102) with coaxial outlet



ACCESSORIES

| Socket | | type | FE1003 |
|---------------------------------|-----------------|--------------|----------------|
| Coaxial cable connector | "General Radio" | type | 874/C8A |
| Mu-metal shields ¹) | | type type | 56130 56131 |

GENERAL

| Photocathode | | | |
|--|------------------------|-------------------|--------------------------|
| Description | semi-transparent, head | 1-on, curve | d surface |
| Cathode material | | Cs-Sh |) |
| Minimum useful diameter | | 42 | 2 mm |
| Spectral response curve ²) | Withe photomy and h | type U (S | 13) |
| Wavelength at maximum response | | 4000 ± 300 |) A |
| Luminous sensitivity ³) | . N _k | av. 65 min. 45 | $\mu A/lm$ $\mu A/lm$ |
| Radiant sensitivity at 4000 Å | | 55 | mA/W |
| Multiplier system | | | |
| Number of stages | | 12 | poperi ' |
| Dynode material | | Ag-Mg-O- | ·Cs |
| Capacitances | | | |
| Grid No.1 to cathode | C_{k/g_1} | 25 | pF |
| Grid No.1 to all other electrodes | C _{g1} | 30 |) pF |
| Grid No.1 to grid No.2 | C_{g_1/g_2} | 17 | ′ pF |
| Anode to final dynode | $C_{a/S_{12}}$ | 8 | b pF |
| Anode to all other electrodes | C _a | 9 | pF |
| | | | |

¹) To avoid field distortion in the electron optical input system it is advised to connect the aquadag shield (pin No.9) to the cathode. If the cathode is circuited to a negative high tension care should be taken to ensure a high tension insulation between the aquadag-shield and the mu-metal screen.

2) See spectral response curve in front of this section

 $^3)$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{\rm 0}{\rm K}$ 7Z2 5490

| TYPICAL CHARACTERISTICS | | | | |
|--|----------------------|--------------|--------------|--------|
| With voltage divider A | | | | |
| Supplý voltage for G = 10 ⁸ | Vb | av. max. | 2500 3000 | v v |
| Anode dark current at G = 10^{8} ¹) | I _{ao} | max. | 5 | μA |
| Linearity between anode pulse amplitude and input light pulse | | up to | 100 | mA |
| With voltage divider B | | | | |
| Linearity between anode pulse amplitude and input light pulse | | up to | 300 | mA |
| Anode pulse rise time at V _b = 2500 V 2) | | <1,8 | .10-9 | s |
| Anode pulse width at half height at V_b = 2500 $^{\circ}$ | V ²) | 4 | .10-9 | s |
| Transit time difference between the centre of the photocathode and 18 mm out of the centre at V_b = 2500 V | | < 0, 2 | .10-9 | S |
| Total transit time at V_b = 2500 V ²) | | 28 | .10-9 | s |
| Maximum peak currents | | 0. | 5 to 1 | А |
| LIMITING VALUES (Absolute max. rating sys | stem) | | | |
| Supply voltage ³) | Vb | max. | 3000 | V |
| Continuous anode current | Ia | max. | 2 | mA |
| Voltage between cathode and first dynode | v_{k/S_1} | max. min. | 600 300 | v v |
| Voltage between consecutive dynodes | v _{Sn/Sn+1} | max. min. | 500 80 | v v |
| Voltage between anode and final dynode 4) | $v_{a/S_{12}}$ | max. min. | 500 80 | V V |

- $^{\rm 1})$ At an ambient temperature of 25 $^{\rm o}{\rm C}.$
- ²) For an infinitely short light pulse, fully illuminating the photocathode.
- $^{3})$ Or the voltage at which the tube circuited in the voltage-divider A has a gain of about $10^{9},$ whichever is lowest.
- When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5491

RECOMMENDED CIRCUITS



Voltage divider type A^{1})



Voltage divider type B¹)

- k = cathode
- g_1 = focusing electrode No.1
- g_2 = focusing electrode No.2
- acc = accelerating electrode
- g₃ = shadow grid
- $S_n = dynode No.n$
- a = anode

Voltage between k and g_1 to be adjusted at about 1 V_S

Voltage between S_1 and S_2 to be adjusted at about 1.2 V_{S}

Voltage between g_3 and S_{12} to be adjusted for optimum time characteristics.

¹) To avoid field distortion in the electron optical input system it is advised to connect the aquadag shield (pin No.9) to the cathode. If the cathode is circuited to a negative high tension care should be taken to ensure a high tension insulation between the aquadag-shield and the mu-metal screen.

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of about 3 mA will be sufficient.

The last stages must be decoupled by means of capacitances to avoid a serious voltage drop on the dynodes. A practical value for C_1 could be 2.10^{-9} F. In the case of high counting rates and large peak power output, and to avoid a high-tension supply of large power, it is possible to supply the first stages with a high tension of small output and the end stages with an average voltage of high output.

A. The electron optical input system consists of five elements:

the photocathode k; the focusing electrode g₁; the focusing electrode g₂; the accelerating electrode acc; the deflector.

To reduce transit-time fluctuations, geometrical time spread, pulse amplitude spread or dark current, this system has the following advantages:

- 1. the photocathode is curved, though the outer window surface is flat, thus facilitating optical coupling;
- 2. a high and homogeneous extraction field at the cathode reduces as much as possible the influence of the initial electron velocities. A cathode-to-accelerator (internally connected to the ninth dynode) voltage of 1750 V ensures a field strength of about 200 V/cm. This field is homogenized at the cathode surface by the focusing electrode g_1 . Fig.1 shows the electron path in the input system.
- 3. The potential of electrode g_1 to the photocathode can be adjusted in order to obtain one of the following characteristics:
 - a. the most satisfactory collection (i.e. for a given luminous flux the largest obtainable anode signal); the optimum of the potential is about 1 V_S ;
 - b. the slightest transit-time fluctuations (the most homogeneous extraction field);
 - c. the most satisfactory uniformity of collection giving the most constant output amplitude.

4. Because the first dynode cannot be placed parallel to the photocathode, the beam of primary electrons is deflected by the deflector to make it impinge at right angles to the first dynode surface. Collection on the first dynode is controlled by the potential of the second dynode (see recommended circuits). 7Z2 5493

OPERATIONAL CONSIDERATIONS (continued



Fig.1: Electron optical input system

B. The multiplier system consists of 12 stages, providing a total current amplification of 10⁸ at about 2500 V (see figures 4 and 5).

The tube is capable of producing very strong peak currents (up to 1 A). Actually the time constant at the output of the multiplier must be very small. Therefore it is necessary to use a low load resistance, well matched to the associated electronic circuitry. For this reason the tube is provided with an coaxial outlet, having a characteristic impedance of 50 Ω . With this load the tube easily delivers pulses of tens of volts, so that an amplifier is rendered superfluous, without attenuation or distortion.

To avoid the effects, which are responsible for rounding of the leading edge and the "jagged" trailing edges, a shadow grid (g_3) is placed parallel to the anode with its wires aligned with those of the anode.

Thus electrons walking from the next-to-last dynode (S11) to the last dynode (S12) are prevented to impinge directly upon the anode.

At the same time induction and oscillations in the anode grid are minimized. The potential of this electrode is to be adjusted at an optimum close to that of the last dynode. Figure 2 shows anode pulses of the tube.

OPERATIONAL CONSIDERATIONS (continued)







(arbitrary units)

of shadow grid potential

ordinate - 10 volts per major division

A further characteristic of g_3 is that it can be used as a control electrode determining the amplitude of anode pulses without the necessity of adjusting the incident light or the gain of the tube, and hence the H.V. supply. Figure 3 illustrates the control characteristics of g_3 .

It should be noted that at equal high tensions the gain of the tube is smaller for voltage divider type B than for one according to type A. (See figures 4 and 5.)

It is advisable to screen the tube with a mu-metal cylinder against magnetic field influences.



Fig.4

A



Fig.5



10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in applications such as scintillation counting in nuclear research together with large size crystals, plastic or liquid scintillators and in optical equipment in which a photomultiplier with a photosensitive area larger than usual is required.

| QUICK REFERENCE DAT | A |
|-------------------------------------|--------------|
| Spectral response | type A (S11) |
| Useful diameter of the photocathode | 63.5 mm |
| Anode sensitivity (at 1800 V) | 250 A/lm |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 14-pin (Jedec B14-38)





ACCESSORIES

57

Socket

S6

S5

S4

S3-S2

Mu-metal shield

type FE1001 type 56135

GENERAL

| Photocathode | | | | |
|--|-------------------|-------------|--------------|----------------|
| Description | semi-transparent, | head-or | ı, flat | surface |
| Cathode material | | (| Cs-Sb | |
| Minimum useful diameter | | | 63.5 | mm |
| Spectral response curve 1) | | type | A (S1) | 1) |
| Wavelength at maximum response | | 4200 | <u>+</u> 300 | A |
| Luminous sensitivity 2) | Nk | av. min. | 70 40 | μA/lm μA/lm |
| Radiant sensitivity at 4200 Å | | | 60 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 10 | |
| Dynode material | | Ag-Mg-O-Cs | | |
| Capacitances | | | | |
| Anode to final dynode | $C_{a/S_{10}}$ | | 3 | pF |
| Anode to all other electrode | C _a | | 5 | pF |
| TYPICAL CHARACTERISTICS | | | | |
| With voltage divider A | | | | |
| Anode sensitivity at V_b = 1800 V | Na | av. min. | 250 100 | A/lm A/lm |
| Anode dark current at $N_a = 100 \text{ A/lm}^3$ | I _{ao} | max. | 0.2 | μΑ |
| Linearity between anode pulse amplitud and input light pulse at $\rm V_b$ = 1800 V | e | up to | 50 | mA |
| | | | | |

1) See spectral response curve in front of this section

2) Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{\rm O}{\rm K}$

 $^{3})$ At an ambient temperature of 25 $^{\rm O}{\rm C}$

| TYPICAL CHARACTERISTICS (continued) | | | |
|--|--------------------|----------------------|--------|
| With voltage divider B | | | |
| Linearity between anode pulse amplitude and input light pulse at V_b = 1800 V | | up to 100 | mA |
| Anode pulse rise time at V_b = 1400 V ¹) | | 7.10-9 | s |
| Anode pulse width at half height at V_b = 1400 V | | 15.10-9 | s |
| Transit time difference between the centre of the photocathode and the edge at V _b = 1400 V | | 7.10 ⁻⁹ | s |
| Total transit time at V_b = 1400 V | | 60.10 ⁻⁹ | s |
| LIMITING VALUES (Absolute max. rating sys | stem) | | |
| Supply voltage | Vb | max. 2000 | V |
| Continuous anode current | Ia | max. 1 | mA |
| Voltage between cathode and first dynode | v_{k/S_1} | max. 500 min. 100 | v v |
| Voltage between cathode and accelerator electrode | V _{k/acc} | max. 500 | v |
| Voltage between consecutive dynodes | $v_{S_n/S_{n+1}}$ | max. 300 min. 80 | v v |
| Voltage between anode and final dynode 2) | V _{a/S10} | max. 300 | V V |

1) For an infinitely short light pulse.

3

 $^{^{2}\}ensuremath{)}$ When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5708

RECOMMENDED CIRCUITS



Voltage divider type A



Voltage divider type B

 $k = cathode & S_n = dynode No.n \\ acc = accelerating electrode & a = anode \\$

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA to 1 mA will be sufficient.

A circuit of type A results in the highest gain of the tube at a given total voltage. A circuit of type B gives a higher current output with better time characteristics, but the total gain is less at the same total voltage.

The accelerating electrode has a seperate external connection to allow adjustment for optimum photoelectron collection on the first dynode.

With high amplitude pulses, it is useful to decouple the last stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.



A

10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in applications such as gamma-ray spectrometry and gamma scintillation cameras.

| QUICK REFERENCE DATA | | | | | |
|---|--------------|--|--|--|--|
| Spectral response | type A (S11) | | | | |
| Useful diameter of the photocathode | 63.5 mm | | | | |
| Anode sensitivity (at 1800 V) | 250 A/lm | | | | |
| Energy resolution for 0.661 MeV Cs^{137} line | 8.5 % | | | | |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 14-pin (Jedec B14-38)



| GENERAL | | | | |
|--|--------------------|-------------|--------------|----------------|
| Photocathode | | | | |
| Description | emi-transparent, | head-or | ı, flat | surface |
| Cathode material | | C | s-Sb | |
| Minimum useful diameter | | | 63.5 | mm |
| Spectral response curve ¹) | | type | A (S1) | L) |
| Wavelength at maximum response | | 4200 - | <u>-</u> 300 | 8 |
| Luminous sensitivity ²) | N _k | av. min. | 80 70 | μA/lm μA/lm |
| Radiant sensitivity at 4200 Å | | | 65 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 10 | |
| Dynode material | | Ag-M | g-0-0 | Cs |
| Capacitances | | | | |
| Anode to final dynode | $C_{a/S_{10}}$ | | 3 | pF |
| Anode to all other electrodes | Ca | | 5 | pF |
| TYPICAL CHARACTERISTICS | | | | |
| Anode sensitivity at V_b = 1800 V | Na | av. min. | 300 100 | A/lm A/lm |
| Anode dark current at $N_a = 100 \text{ A/lm}^3$) | I _{ao} | max. | 0.2 | μA |
| Linearity between anode pulse amplitude and input light pulse at V $_{\rm b}$ = 1800 V | | up to | 50 | mA |
| Anode pulse rise time at V_b = 1400 V ⁴) | | 7. | 10-9 | S |
| Anode pulse width at half height at V_b = 14 | 400 V | 15. | 10^{-9} | S |
| Transit time difference between the centre of the photocathode and the edge at V _b = 1400 V | | 7. | 10-9 | S |
| Total transit time at V_b = 1400 V | | 60. | 10-9 | S |
| Energy resolution for 0.661 MeV Cs^{137} li | ine ⁵) | av. max. | 8.5 9.0 | % % |
| | | | | |

 $(1)^{2}(3)^{3}(5)$ see page 3.
| LIMITING VALUES (Absolute max. rating system | ı) | | | |
|---|----------------------|--------------|------------|--------|
| Supply voltage | Vb | max. | 2000 | V |
| Continuous anode current | Ia | max. | 1 | mA |
| Voltage between cathode and first dynode | V _{k/S1} | max. min. | 500 100 | V V |
| Voltage between cathode and accelerator electrode | V _{k/acc} | max. | 500 | v |
| Voltage between consecutive dynodes | V _{Sn/Sn+1} | max. min. | 300 80 | v v |
| Voltage between anode and final dynode ⁶) | $v_{a/S_{10}}$ | max. min. | 300 80 | v v |

RECOMMENDED CIRCUIT



| k | = | cathode | Sn | = | dynode No.n | C_1 | = | 470 pF |
|-----|---|------------------------|----|---|-------------|-------|---|---------|
| acc | = | accelerating electrode | а | = | anode | C_2 | = | 1000 pF |

¹) See spectral response curve in front of this section

- 2) Measured with a tungsten ribbon lamp having a colour temperature of 2850 0 K
- ³) At an ambient temperature of 25 $^{\circ}C$
- ⁴) For an infinitely short light pulse
- 5) Measured with a 2" x 2" NaI crystal
- When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked 7Z2 8078

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be a practical value.

Each tube is accompanied by a sheet with characteristics, on which is indicated the voltage to be applied between the cathode and the first dynode. The best results in gamma-ray spectrometry will be achieved with this voltage, when the recommended voltage-divider bridge is used.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.



A



10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in applications which require a good sensitivity in the ultraviolet region, combined with a photosensitive area larger than usual.

| QUICK REFERENCE DAT | 'A | |
|-------------------------------------|----|--------------|
| Spectral response | | type U (S13) |
| Useful diameter of the photocathode | | 63.5 mm |
| Anode sensitivity (at 1800 V) | | 250 A/lm |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 14-pin (Jedec B14-38)





ACCESSORIES

S8

1 14.1

110

acc

7201271

59 510

Socket

S6

S5 S4

53

SZ

Mu-metal shield.

| type | FE1001 |
|------|--------|
| type | 56135 |

7Z2 7838

1

| GENERAL | | | | |
|---|-------------------|-------------|----------------|----------------|
| Photocathode | | | | |
| Description | semi-transparent, | head-on, | flat | surface |
| Cathode material | | C | s-Sb | |
| Minimum useful diameter | | - bardin | 63.5 | mm |
| Spectral response curve ¹) | | type l | J (S 13 | 3) |
| Wavelength at maximum response | | 4000 ± | : 300 | A |
| Luminous sensitivity 2) | N _k | av. min. | 70 40 | μA/lm μA/lm |
| Radiant sensitivity at 4000 Å | | | 60 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 10 | |
| Dynode material | | | g-0-0 | Cs |
| Capacitances | | | | |
| Anode to final dynode | $C_{a/S_{10}}$ | | 3 | pF |
| Anode to all other electrodes | Ca | | 5 | pF |
| | | | | |
| TYPICAL CHARACTERISTICS | | | | |
| with voltage divider A | | | 050 | . /1 |
| Anode sensitivity at V_b = 1800 V | Na | av. min. | 100 | A/lm A/lm |
| Anode dark current at $N_a = 100 \text{ A/lm}^3$ |) I _{ao} | max. | 0.2 | μA |
| Linearity between anode pulse amplitude and input light pulse at V_b = 1800 V | de | up to | 50 | mA |

 1) See spectral response curve in front of this section

 $^2\)$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^0\mbox{K}$

³) At an ambient temperature of 25 $^{\circ}C$

TYPICAL CHARACTERISTICS (continued)

With voltage divider B

| Linearity between anode pulse amplitude and input light pulse at $\rm V_b$ = 1800 V $$\rm V$$ | up to 100 | mA |
|---|---------------------|----|
| Anode pulse rise time at V_b = 1400 V ¹) | 7.10-9 | s |
| Anode pulse width at half height at V_b = 1400 V | 15.10 ⁻⁹ | s |
| Transit time difference between the centre of the photocathode and the | | |
| edge at V_b = 1400 V | 7.10 ⁻⁹ | s |
| Total transit time at V _b = 1400 V | 60.10 ⁻⁹ | s |

LIMITING VALUES (Absolute max. rating system)

| Supply voltage | Vb | max. | 2000 | V |
|---|---------------------------------|--------------|------------|--------|
| Continuous anode current | Ia | max. | 1 | mA |
| Voltage between cathode and first dynode | v_k/s_1 | max. min. | 500 100 | v v |
| Voltage between cathode and accelerator electrode | V _{k/acc} | max. | 500 | v |
| Voltage between consecutive dynodes | V _{Sn/Sn+1} | max. min. | 300 80 | v v |
| Voltage between anode and final dynode 2) | V _a /S ₁₀ | max. min. | 300 80 | v v |

RECOMMENDED CIRCUITS



Voltage divider type A

¹) For an infinitely short light pulse.

²) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 7839

RECOMMENDED CIRCUITS (continued)



Voltage divider type B

| k | = | cathode | Sn | = | dynode No.1 |
|-----|---|------------------------|----|---|-------------|
| acc | = | accelerating electrode | a | = | anode |

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA to 1 mA will be sufficient.

A circuit of type A results in the highest gain of the tube at a given total voltage. A circuit of type B gives a higher current output with better time characteristics, but the total gain is less at the same total voltage.

The accelerating electrode has a separate external connection to allow adjustment for optimum photoelectron collection on the first dynode.

With high amplitude pulses, it is useful to decouple the last stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.



A



10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for geophysical measurements in which the thick quartz window serves as a medium for Cerenkov radiation caused by cosmic-rays.

| QUICK REFERE | ENCE DATA | . A share |
|-------------------------------------|-----------|-----------|
| Spectral response | type | U (S13) |
| Useful diameter of the photocathode | 63.5 | 5 mm |
| Window thickness (quartz) | 10 |) mm |
| Anode sensitivity (at 1800 V) | 250 |) A/lm |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 14-pin (Jedec B14-38)





ACCESSORIES

S2

S6

S5

S4

S3

S7 S8

SI

59

110

S10

C

acc

7201271

Socket

Mu-metal shield

| type | FE1001 | | |
|------|--------|--|--|
| type | 56135 | | |

GENERAL

| Photocathode | | | |
|---|------------------------|--------------------|----------------|
| Description | semi-transparent, head | d-on, flat | surface |
| Cathode material | | Cs-Sb | |
| Minimum useful diameter | | 63.5 | mm |
| Spectral response curve ¹) | ty | pe U (S13 | 3) |
| Wavelength at maximum response | 40 | 000 ± 300 | Å |
| Luminous sensitivity ²) | N _k ar | v. 60 nin. 35 | μA/lm μA/lm |
| Radiant sensitivity at 4000 Å | | 50 | mA/W |
| Multiplier system | | | |
| Number of stages | | 10 | |
| Dynode material | Ag-Mg-O-Cs | | |
| Capacitances | | | |
| Anode to final dynode | $C_{a/S_{10}}$ | 3 | pF |
| Anode to all other electrodes | C _a | 5 | pF |
| TYPICAL CHARACTERISTICS | | | |
| With voltage divider A | | | |
| Anode sensitivity at V_b = 1800 V | N _a am | v. 250 nin. 100 | A/lm A/lm |
| Anode dark current at $N_a = 100 \text{ A/lm}^3$ |) I _{ao} m | ax. 0.2 | μA |
| Linearity between anode pulse amplitud and input light pulse | e up | o to 50 | mA |
| | | | |

¹) See spectral response curve in front of this section

 $^2)$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^0\mathrm{K}$

³) At an ambient temperature of 25 $^{\circ}C$

TYPICAL CHARACTERISTICS (continued)

With voltage divider B

| Linearity between anode pulse amplitude and input light pulse at V_b = 1800 V | up to 100 | mA |
|---|---------------------|----|
| Anode pulse rise time at V _b = 1400 V 1) | 7.10-9 | s |
| Anode pulse width at half height at V_b = 1400 V | 15.10-9 | s |
| Transit time difference between the centre of the photocathode and the | a state | |
| edge at V_b = 1400 V | 7.10^{-9} | s |
| Total transit time at V_b = 1400 V | 60.10 ⁻⁹ | s |

LIMITING VALUES (Absolute max. rating system)

| Supply voltage | Vb | max. | 2000 | V |
|---|---|--------------|------------|--------|
| Continuous anode current | Ia | max. | 1 | mA |
| Voltage between cathode and first dynode | v_k/s_1 | max. min. | 500 100 | V V |
| Voltage between cathode and accelerator electrode | V _{k/acc} | max. | 500 | v |
| Voltage between consecutive dynodes | ^V S _n /S _{n+1} | max. min. | 300 80 | v v |
| Voltage between anode and final dynode ²) | v _a /s ₁₀ | max. min. | 300 80 | v v |

RECOMMENDED CIRCUITS



Voltage divider type A

¹) For an infinitely short light pulse.

²) When caculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 7841

RECOMMENDED CIRCUITS (continued)



Voltage divider type B

| k | = | cathode | |
|-----|---|--------------|-----------|
| acc | = | accelerating | electrode |

S_n = dynode No.n a = anode

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA to 1 mA will be sufficient.

A circuit of type A results in the highest gain of the tube at a given total voltage. A circuit of type B gives a higher current output with better time characteristics, but the total gain is less at the same total voltage.

The accelerating electrode has a separate external connection to allow adjustment for optimum photoelectron collection on the first dynode.

With high amplitude pulses, it is useful to decouple the last stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.



A



14 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in nuclear -physics applications where a high degree of time definition is required (fast coincidences, Cerenkov counters).

| QUICK REFERENCE DATA | | | |
|-------------------------------------|-----------------|-------|--|
| Spectral response | type A (| (S11) | |
| Useful diameter of the photocathode | 110 | mm | |
| Gain (at 2400 V) | 10 ⁸ | | |
| Anode pulse rise time | 2 | ns | |
| Linearity | up to 300 | mA | |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 20-pin (Jedec B20-102)



ACCESSORIES

Socket

Mu-metal shield (tube with metal container) (tube without metal container) type FE1003 type 56133 type 56129 7Z2 8051

GENERAL Photocathode semi-transparent, head-on, curved surface 1) Description Cathode material Cs-Sb Minimum useful diameter 110 mm Radius of curvature 180 + 5mm Spectral response curve 2) type A (S11) 4200 + 3008 Wavelength at maximum response 70 av. $\mu A/lm$ Luminous sensitivity ³) Nk min. 45 $\mu A/lm$ Radiant sensitivity at 4200 Å 60 mA/W Multiplier system Number of stages 14 Dynode material Ag-Mg-O-Cs Capacitances Anode to final dynode Ca/S14 5 pF Anode to all other electrodes Ca 7 pF TYPICAL CHARACTERISTICS With voltage divider A av. 2400 V Supply voltage for $G = 10^8$ Vh max. 3000 V 2 av. μA Anode dark current at G = $10^8 4$) Iao max. 12 μA Linearity between anode pulse amplitude and input light pulse up to 100 mA

 The tube has a plane-concave window and is delivered with a metal envelope.

²) See spectral response curve in front of this section

 3) Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{\mathrm{O}}$ K

 4) At an ambient temperature of 25 $^{\circ}$ C



TYPICAL CHARACTERISTICS (continued)

With voltage divider B

| Linearity between anode pulse amplitude and input light pulse | up to 300 | mA |
|---|--------------------|----|
| Anode pulse rise time at V_b = 3000 V 1) | 2.10-9 | s |
| Anode pulse width at half height at V _b = 3000 V 1) | 4.10 ⁻⁹ | s |
| Transit time difference between the centre of the photocathode and the edge at V_b = 3000 V | 10-9 | S |
| Total transit time at V _b = 3000 V ¹) | 45.10-9 | s |
| Maximum peak currents | 0.5 to 1 | А |

LIMITING VALUES (Absolute max. rating system)

| Supply voltage ²) | v _b | max. | 3000 | V |
|---|--------------------|--------------|-------------|--------|
| Continuous anode current | Ia | max. | 2 | mA |
| Voltage between cathode and first dynode + grid No.2 | v_{k/S_1+g_2} | max. min. | 800 250 | V V |
| Voltage between cathode and accelerator electrode | V _{k/acc} | 1400 to | 1800 | v |
| Voltage between grid No.1 and cathode | V _{k/g1} | max. | 300 | V |
| Voltage between grid No.3 and first dynode | v_{g_3/S_1} | max. | 100 | v |
| Voltage between consecutive dynodes | $v_{S_n/S_{n+1}}$ | max. min. | 500 80 | V V |
| Voltage between anode and final dynode ³) | $v_{a/S_{14}}$ | max. min. | 500 · 80 | V V |

¹) For an infinitely short light pulse, fully illuminating the photocathode.

 $^{^2)}$ Or the voltage at which the tube circuited in the voltage divider A has a gain of about 10⁹, whichever is lowest.

³) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5701



RECOMMENDED CIRCUITS



Voltage divider type A 1)



Voltage divider type B 1)

k = cathode

- g_1 = focusing electrode
- g₂ = focusing electrode
- acc = accelerating electrode
- $g_3 = deflector$
- $S_n = dynode No.n$
- a = anode

voltage between k and g_1 to be adjusted at about 2 V_S; voltage between S₂ and S₃ to be adjusted at about 1.2 V_S; decoupling capacitances C₁ = 100q/V_S, C₂ = 100q/3V_S, C₃ = 100q/9V_S, C₄ = 100q/27V_S etc. with q = quantity of electricity transported by the anode.

4

¹) If the cathode is connected to negative HT, precautions should be taken to ensure a high-tension insulation between the aquadag shield and the metal envelope or mu-metal shield. 7Z2 5702

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of about 3 mA will be sufficient.

The last stages must be decoupled by means of capacitances to avoid a serious voltage drop on the dynodes. A practical value of C_1 will be 2.10^{-9} F

In the case of high counting rates and large peak power outputs, and to avoid a high-tension supply of large power, it is possible to supply the first stages with a high tension of small output and the end stages with an average voltage of high output.

A. The electron optical system consists of five elements:

the photocathode k; the focusing electrode g_1 ; the focusing electrode g_2 ; the accelerating electrode acc; the deflector g_3 .

To reduce transit-time fluctuations and geometrical time spread, this system has the following advantages.

- 1. The photocathode is curved, with a curvature radius of 183 mm. To facilitate optical coupling to scintillators the tube is provided with a plane-concave window.
- 2. A high and homogeneous extraction field at the cathode reduces as much as possible the influence of the initial electron velocities. A cathode-to-accelerating voltage of about 1500 V (to be connected to the tenth or a subsequent dynode) ensures a field strength of about 40 V/cm. This field is homogenized at the cathode surface by the focusing electrode g_1 . Fig.1 shows the electron paths in the input system.
- 3. The potential of the electrode g_1 to the photocathode can be adjusted in order to obtain one of the following characteristics:
 - (a) the most satisfactory collection (i.e. for a given luminous flux the largest obtainable anode signal); the optimum value of the potential is about 2 V_s;
 - (b) the slightest transit-time fluctuations (the most homogeneous extraction field);
 - (c) the most satisfactory uniformity of collection giving the most constant output pulse amplitude.

OPERATIONAL CONSIDERATIONS (continued)





OPERATIONAL CONSIDERATIONS (continued)

4. Because the first dynode cannot be placed parallel to the photocathode, the beam of primary electrons is deflected by the electrode g_3 to make them impinge at right angles to the first dynode surface.

Collection on the first dynode is controlled by the potential of the third dynode.

B. The multiplier system consists of 14 stages, providing a total current amplification of 10^8 at about 2400 V (see fig.2) The tube is capable of producing very strong peak currents (up to 1 A). Actually, the time constant at the output of the multiplier must be very small. Therefore it is necessary, taking into account the parasitic capacitances, to use a low load resistance. It is advisable to use a resistance-matched coaxial cable (e.g. 75 or 100Ω). With this load the tube easily delivers pulses of tens of volts, so that an amplifier is rendered superfluous.

It should be noted that in a number of applications it is not necessary for the current to be proportional to the incident luminous flux. As a matter of fact, such pulses are needed for time measurements only, so not for spectro-graphy purposes.

If at the same time it is required, however, to determine the energy of the incident radiation, it is possible to select from one of the dynodes a signal proportional to the incident flux. In fact, when ascending the dynodes progressively, starting from the anode, the current is divided at each stage by d-1, d representing the secondary-emission coefficient of each stage (d \approx 3.5) It is therefore possible to locate a dynode, the current of which is lower than, or equal to, the saturation limit of the dynodes.

Fig.3 illustrates the variation of the anode current as a function of the incident flux, the voltage divider being of type B. The anode current is then linear up to 300 mA.

Care should be taken that the anode voltage is adjusted to its optimum value. In fig.4 the anode current variation is plotted against anode-to-final dynode voltage.

It should be noted that for equal high tensions the gain of the tube is smaller for voltage divider type B than for one according to type A.

In practice, therefore, it will be preferable to use the A type distribution, or a distribution between A and B, (e.g. starting with 1.2 V_S between S₈ and S₉, 1.5 V_S between S₉ and S₁₀ etc., maintaining the same progression).

It is advisable to screen the tube with a mu-metal cylinder against magneticfield influence.

7Z2 5705

7



Fig. 2

A



Fig.3





С



10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in applications such as scintillation counting under limited dimensional conditions, optical measurements with narrow light beams, in-microscope light transmission measurements, and computer punch-tape or punch-card reading etc.

| QUICK REFERENCE DAT | ĨA. |
|-------------------------------------|--------------|
| Spectral response | type A (S11) |
| Useful diameter of the photocathode | 14 mm |
| Anode sensitivity (at 1800 V) | 250 A/lm |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 12-pin (glass)



| GENERAL | |
|---------|--|
|---------|--|

| Photocathode | | | | |
|---|--------------------|-------------|-----------|----------------|
| Description semi-tr | ansparent, | head-on | , flat | surface |
| Cathode material | | C | s-Sb | |
| Minimum useful diameter | | | 14 | mm |
| Spectral response curve ¹) | | type | A (S11 | L) |
| Wavelength at maximum response | | 4200 - | ± 300 | Å |
| Luminous sensitivity ²) | N _k | av. min. | 70 40 | μA/lm μA/lm |
| Radiant sensitivity at 4200 Å | | | 60 | mA/W |
| Multiplier system | | | | |
| Number of stages | | •r- 98 | 10 | |
| Dynode material | | Ag-M | g-0-0 | 2s |
| Capacitances | | | | |
| Anode to final dynode | Ca/S ₁₀ | | 1.5 | pF |
| Anodé to all other electrodes | Ca | | 2.5 | pF |
| TYPICAL CHARACTERISTICS | | | | |
| With voltage divider A | | | | |
| Anode sensitivity at V_b = 1800 V | Na | av. min. | 250 30 | A/lm A/lm |
| Anode dark current at $N_a = 30 \text{ A/lm}^3$) | I _{ao} | av. max. | 0.02 | μΑ μΑ |
| Linearity between anode pulse amplitude and input light flux | | up to | 10 | mA |
| | | | | |

1) See spectral response curve in front of this section

 $^2)$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{\rm O}{\rm K}$

³) At an ambient temperature of 25 $^{\rm O}{\rm C}$

TYPICAL CHARACTERISTICS

With voltage divider B

| Linearity between anode pulse amplitude | | |
|--|----------|----|
| and input light pulse | up to 30 | mA |
| Anode pulse rise time at V_b = 1800 V 1) | 3.10-9 | s |
| Total transit time | 30.10-9 | s |

LIMITING VALUES (Absolute max. rating system)

| Supply voltage | Vb | max. | 1800 | V |
|---|----------------------|--------------|------------|---------|
| Continuous anode current | Ia | max. | 1 | mA |
| Voltage between cathode and first dynode | v _{k/S1} | max. min. | 300 120 | V ·V |
| Voltage between consecutive dynodes | V _{Sn/Sn+1} | maż. min. | 200 80 | v v |
| Voltage between anode and final dynode ²) | V _{a/S10} | max. min. | 200 80 | v v |

RECOMMENDED CIRCUITS



Voltage divider type A

- ¹) For an infinitely short light pulse.
- ²) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5353

RECOMMENDED CIRCUITS (continued)



k = cathode
acc = accelerating electrode

S_n = dynode No.n a = anode

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be sufficient.

Different kinds of voltage dividers are possible. A circuit of type A results in the highest gain of the tube at a given total voltage; a circuit of type B gives a higher current output with better time characteristics, but the total gain is less at the same total voltage.

When pulses with high amplitudes are taken from the anode, it is useful to decouple the last stages as indicated in the circuit by means of capacitors of a few hundred pF, to avoid a voltage drop between these stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.



A



10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in applications such as scintillation counting under limited dimensional conditions, optical measurements with narrow light beams, in-microscope light transmission measurements, and computer punch-tape or punch-card reading etc.

| QUICK REFERENCE DA | ATA | |
|-------------------------------------|--------|-------|
| Spectral response | type A | (S11) |
| Useful diameter of the photocathode | 14 | mm |
| Anode sensitivity (at 1800 V) | 250 | A/lm |

DIMENSIONS AND CONNECTIONS

Base: 12 isolated flexible leads

Dimensions in mm



1

XP 1111 XP 1111 B

| ACCESSORIES | | | |
|--|---------------------|-----------------------|----------------|
| Mu-metal shield type | 2 56134 | | |
| GENERAL | | | |
| Photocathode | | | |
| Description | semi-transparent, h | nead-on, flat | surface |
| Cathode material | | Cs-Sb | |
| Minimum useful diameter | | 14 | mm |
| Spectral response curve 1) | | type A (S11 |) |
| Wavelength at maximum response | | 4200 ± 300 | Å |
| Luminous sensitivity 2) | N _k | av. 70 min. 40 | μA/lm μA/lm |
| Radiant sensitivity at 4200 $\hbox{\AA}$ | | 60 | mA/W |
| Multiplier system | | | r weater |
| Number of stages | | 10 | |
| Dynode material | | Ag-Mg-O-C | Cs |
| Capacitances | | | |
| Anode to final dynode | $C_{a/S_{10}}$ | 1.5 | pF |
| Anode to all other electrodes | C _a | 2.5 | pF |
| TYPICAL CHARACTERISTICS | | | |
| With voltage divider A | | | |
| Anode sensitivity at V_b = 1800 V | Na | av. 250 min. 30 | A/lm A/lm |
| Anode dark current at $N_a = 30 \text{ A/lm}^3$) | I _{ao} | av. 0.02 max. 0.10 | μΑ μΑ |
| Linearity between anode pulse amplitud and input light flux | le | up to 10 | mA |
| 1 | | | |

 $1) \\ \mbox{See} spectral response curve in front of this section$

 $^2)$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^0\mathrm{K}$

 3) At an ambient temperature of 25 $^{\mathrm{O}}\mathrm{C}$

XP 1111 XP 1111 B

TYPICAL CHARACTERISTICS (continued)

With voltage divider B

| Linearity between anode pulse amplitude | | | |
|---|--------|-----|----|
| and input light pulse | up to | 30 | mA |
| Anode pulse rise time at V _b = 1800 V 1) | 3.10-9 | | s |
| Total transit time | 30.1 | 0-9 | s |

LIMITING VALUES (Absolute max. rating system)

| Supply voltage | Vb | max. | 1800 | V |
|---|----------------------|--------------|------------|--------|
| Continuous anode current | Ia | max. | 1 | mA |
| Voltage between cathode and first dynode | v _{k/S1} | max. min. | 300 120 | v v |
| Voltage between consecutive dynodes | v _{Sn/Sn+1} | max. min. | 200 80 | v v |
| Voltage between anode and final dynode 2) | v _{a/S10} | max. min. | 200 80 | v v |

RECOMMENDED CIRCUITS



Voltage divider type A

¹) For an infinitely short light pulse.

²⁾ When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5357

XP 1111 XP 1111 B

RECOMMENDED CIRCUITS (continued)



Voltage divider type B

k = cathode S_n = dynode No.n acc = accelerating electrode a = anode

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be sufficient.

Different kinds of voltage dividers are possible. A circuit of type A results in the highest gain of the tube at a given total voltage; a circuit of type B gives a higher current output with better time characteristics, but the total gain is less at the same total voltage.

When pulses with high amplitudes are taken from the anode, it is useful to decouple the last stages as indicated in the circuit by means of capacitors of a few hundred pF, to avoid a voltage drop between these stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.
XP 1111 XP 1111 B



A



Dimensions in mm

6 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in optical applications, where space is very restricted and relatively high light fluxes are to be measured $(10^{-5} \text{ to } 10^{-3} \text{ lm})$.

| QUICK REFERENCE DATA | |
|-------------------------------------|--------------|
| Spectral response | type A (S11) |
| Useful diameter of the photocathode | 14 mm |
| Anode sensitivity (at 1200 V) | 0.7 A/lm |

DIMENSIONS AND CONNECTIONS

Base: 9-pin miniature with pumping stem (Jedec E9-37)



ACCESSORIES

Socket

type 2422 502 90007

03

acc, S1

80/53

7203704

7Z2 8082

TENTATIVE DATA

| GENERAL | | | | |
|--|--------------------------------|-------------|------------|--------------|
| Photocathode | | | | |
| Description | semi-transparent, | head-on | , flat | surface |
| Cathode material | | С | s-Sb | |
| Minimum useful diameter | | | 14 | mm |
| Spectral response curve 1) | | type A | (S11) | |
| Wavelength at maximum response | | 4200 - | - 300 | Å |
| Luminous sensitivity 2) | Nk | | 40 | µA/lm |
| Radiant sensitivity at 4200 Å | | | 35 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 6 | |
| Dynode material | | Ag-Mg | -0-Cs | s. and the |
| Capacitances | | | | |
| Anode to final dynode | C _{a/S6} | | 1.6 | pF |
| Anode to all other electrode | Ca | | 1.3 | pF |
| TYPICAL CHARACTERISTICS | | | | |
| With voltage divider A | | | | |
| Anode sensitivity at V_b = 1200 V | Na | av. min. | 0.7 0.2 | A/lm A/lm |
| Anode dark current at $N_a = 0.3 \text{ A/lm}^3$ | ³) I _{ao} | max. C | .010 | μΑ |
| Linearity between anode pulse amplitu and input light flux | de | up to | 15 | mA |
| With voltage divider B | | | | |
| Linearity between anode pulse amplitu and input light pulse | de | up to | 30 | mA |
| | | | | |

1) See spectral response curve in front of this section

 $^2)$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{\rm O}{\rm K}$

³) At an ambient temperature of 25 $^{\circ}C$

7Z2 8083

LIMITING VALUES (Absolute max. rating system) Supply voltage max. 1200 V Vb Continuous anode current Ia max. 0.5 mA Voltage between cathode and first dynode Vk/S1 200 V max. 200 V max. Voltage between consecutive dynodes $V_{S_n/S_{n+1}}$ min. 80 V 200 V max. Voltage between anode and final dynode 1) Va/S6 min. 50 V

RECOMMENDED CIRCUITS



Voltage divider type A



k = cathode $S_n = \text{dynode No.n}$ acc = accelerating electrode a = anode

 When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5361

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be sufficient.

Different kinds of voltage dividers are possible. A circuit of type A results in the highest gain of the tube at a given total voltage, a circuit of type B gives higher currents in the last stages, but the total gain is less at the same total voltage.

At high pulse amplitudes it is useful to decouple the last stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube against the influence of magnetic fields by means of a mu-metal cylinder.



A



4 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in optical applications, where space is very restricted and relatively high light fluxes are to be measured $(10^{-4} \text{ to } 10^{-1} \text{ lm})$.

| QUICK REFERENCE DATA | | | | |
|-------------------------------------|----------|---------|--|--|
| Spectral response | type | A (S11) | | |
| Useful diameter of the photocathode | 14 | mm | | |
| Anode sensitivity (at 900 V) | 15 | mA/lm | | |
| Dark current (at 4 mA/lm) | max. 0.1 | nA | | |

DIMENSIONS AND CONNECTIONS

Base: 9-pin miniature with pumping stem (Jedec E9-37)



ACCESSORIES

Socket

type 2422 502 90007

Dimensions in mm

TENTATIVE DATA

GENERAL

| motocatnode | |
|---------------------------------|---|
| Description | semi-transparent, head-on, flat surface |
| Cathode material | Cs-Sb |
| Minimum useful diameter | 14 mm |
| Spectral response curve 1) | type A (S11) |
| Wavelength at maximum response | 4200 ± 300 Å |
| Luminous sensitivity 2) | N _k 40 µA/lm |
| Radiant sensitivity at 4200 $Å$ | 35 mA/W |
| Multiplier system | |
| Number of stages | 4 |
| Dynode material | Ag-Mg-O-Cs |
| Capacitances | |
| Anode to final dynode | C _{a/S4} 1.9 pF |
| Anode to all other electrodes | C _a 2.7 pF |
| 2 176 mar. 21 - 12 | |
| TYPICAL CHARACTERISTICS | |

| With voltage divider A | | | | |
|---|----------------|------|-----|-------|
| Anode consitivity at $V_{\rm c} = 900 \text{ V}$ | N | av. | 15 | mA/lm |
| Anode sensitivity at $v_b = 900 v_b$ | ¹ a | min. | 4 | mA/lm |
| Anode dark current at $N_a = 4 \text{ mA/lm}^3$) | Iao | max. | 0.1 | nA |

1) See spectral response curve in front of this section

 $^2\ensuremath{)}$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^0\ensuremath{K}$

 3) At an ambient temperature of 25 $^{\mathrm{o}}\mathrm{C}$

7Z2 8085

LIMITING VALUES (Absolute max. rating system) Supply voltage Vb max. 900 V Continuous anode current Ia max. 0.1 mA Voltage between cathode and first dynode V_{k/S_1} V max. 200 max. 200 V Voltage between consecutive dynodes $v_{S_n/S_{n+1}}$ 80 V min. max. 200 V Voltage between anode and final dynode 1) Va/S4 min. 50 V

RECOMMENDED CIRCUITS



Voltage divider type A

 When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked.
 7Z2 8086

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be sufficient.

Different kinds of voltage dividers are possible. A circuit of type A results in the highest gain of the tube at a given total voltage, a circuit of type B gives higher currents in the last stages, but the total gain is less at the same total voltage.

At high pulse amplitudes it is useful to decouple the last stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube against the influence of magnetic fields by means of a mu-metal cylinder.



A



10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in applications such as scintillation counting and optical measurements under limited dimensional conditions. Its revolutionary rugged construction makes it particularly suitable for geophysical and astronomical missile experiments.

| QUICK REFERENCE DA | TA |
|-------------------------------------|--------------|
| Spectral response | type A (S11) |
| Useful diameter of the photocathode | 14 mm / |
| Anode sensitivity (at 1800 V) | 200 A/lm |
| Shock | 30 g |
| Vibration | 25 g |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 12 semi-flexible leads



TENTATIVE DATA

| XF | XP 1115 B XP 1115 C | | | | | | | | | |
|----|--|------|----|----------------|------|-------|-------|-------|--------------|----------------|
| | ACCESSORIES | | | | | | | | | |
| | Socket | type | | 56073 | | | | | | |
| | Mu-metal shield | type | | 56134 | | | | | | |
| | GENERAL | | | | | | | | | |
| | Photocathode | | | | | | | | | |
| | Description | 5 | se | mi - tr | ansp | arent | , hea | ad-on | , flat | surface |
| | Cathode material | | | | | | | С | ls-Sb | |
| | Minimum useful diameter | | | | | | | | 14 | mm |
| | Spectral response curve ¹) | | | | | | t | ype | A (S1) | L) |
| | Wavelength at maximum response | | | | | | 4 | 200 - | ± 300 | Å |
| | Luminous sensitivity ²) | | | | | | | | 70 40 | μA/lm μA/lm |
| | Radiant sensitivity at 4200 ${ m \AA}$ | | | | | | | | 60 | mA/W |
| | Multiplier system | | | | | | | | | |
| | Number of stages | | | | | | | | 10 | |
| | Dynode material | | | | | | 4 | Ag-M | g-0-0 | Cs |
| - | Capacitances | | | | | | | | | |
| | Anode to final dynode | | | | | | | | 1.9 | pF |
| | Anode to all other electrodes | | | | | | | | 3.0 | pF |
| | TYPICAL CHARACTERISTICS | | | | | | | | | |
| - | Shock | | | | | | | | | |
| | Shape of shock pulses | | | | | | ha | lf-wa | ave sin | nusoidal |
| | Peak acceleration | | | | | | | 6 | 0 <u>+</u> 6 | g |
| | Duration | | | | | | | | 10 | ms |

Number of shocks in each of 3 orthogonal axes

1) See spectral response curve in front of this section

 $^2)$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^0\mathrm{K}$ 7Z2 8088

| | | XP 1115 X | P 1115 C |
|--|---------------------|------------------------|----------------|
| TYPICAL CHARACTERISTICS (continued) | | | |
| Vibration | | | • |
| Shape | | sinusoidal | |
| Acceleration for 20 to 2000 Hz | | 5 to 20 | g |
| Duration in each of 3 orthogonal axes | | 30 | min. |
| With voltage divider A | | | |
| Anode sensitivity at V_b = 1800 V | Na | av. 200 min. 30 | A/lm ← A/lm |
| Anode dark current at N_a = 30 A/lm ¹) | I _{ao} | av. 0.02 max. 0.10 | μΑ μΑ |
| Linearity between anode pulse amplitude and input light flux | | up to 10 | mA |
| With voltage divider B | | | |
| Linearity between anode pulse amplitude and input light pulse | | upto 30 | mA |
| Anode pulse rise time at V_b = 1800 V ²) | | 3.10 ⁻⁹ | S |
| Total transit time | | 30.10-9 | S |
| LIMITING VALUES (Absolute max. rating sys | stem) | | |
| Supply voltage | Vb | max. 1800 | V |
| Continuous anode current | Ia | max. 0.5 | mA 🔶 |
| Voltage between cathode and first dynode | v_{k/S_1} | max. 300 min. 220 | v v 🔶 |
| Voltage between consecutive dynodes | v _{Sn/Sn+} | max. 200 -1 min. 80 | V V |
| Voltage between anode and final dynode ³) | v _{a/S10} | max. 200 min. 80 | V V |
| | | | |

- ¹) At an ambient temperature of 25 $^{\circ}$ C.
- ²) For an infinitely short light pulse.
- ³) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked.

XP1115 B





Voltage divider type B

k = cathode $S_n = dynode No.n$ acc = accelerating electrode a = anode

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be sufficient.

Different kinds of voltage dividers are possible. A circuit of type A results in the highest gain of the tube at a given total voltage; a circuit of type B gives a higher current output with better time characteristics, but the total gain is less at the same total voltage.

When pulses with high amplitudes are taken from the anode, it is useful to decouple the last stages as indicated in the circuit by means of capacitors of a few hundred pF, to avoid a voltage drop between these stages.

OPERATIONAL CONSIDERATIONS (continued)

The semi-flexible leads of the tube may be soldered into the circuit; care must be taken to conduct the heat away from the glass seals. Excessive bending of the leads is to be avoided.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.

7Z2 5371

XP 1115 B XP 1115 C



A

10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in applications such as infra-red telecommunication and ranging, under limited dimensional conditions. Its rugged construction makes it particularly suitable for industrial equipment.

| QUICK REFERENCE DATA | A | |
|-------------------------------------|------|--------|
| Spectral response | type | C (S1) |
| Useful diameter of the photocathode | 14 | mm |
| Anode sensitivity (at 1800 V) | 20 | A/lm |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 12-pin (glass)



Socket

Mu-metal shield

type 56073 type 56134

7Z2 8090

TENTATIVE DATA

1

| GENERAL | | | | |
|---|--------------------|-----------------|------|---------|
| Photocathode | | | | |
| Description | semi-transparent, | head-on, | flat | surface |
| Cathode material | | Ag-O | -Cs | |
| Minimum useful diameter | | | 14 | mm |
| Spectral response curve 1) | | type C | (S1) | |
| Wavelength at maximum response | | 8000 <u>+</u> 1 | .000 | Å |
| Luminous sensitivity ²) | Nk | | 20 | µA/lm |
| Radiant sensitivity at 8000 \AA | | | 2 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 10 | |
| Dynode material | | Ag-Mg- | 0-Cs | S |
| Capacitances | | | | |
| Anode to final dynode | C _{a/S10} | | 1.5 | pF |
| Anode to all other electrodes | Ca | | 2.5 | pF |
| Shock and vibration | | | | |
| To be specified | | | | |
| TYPICAL CHARACTERISTICS | | | | |
| Voltage divider A | | | | |
| Anode consitivity at $W_{\rm c} = 1800$ V | NT | | 201 | A / 1mg |

| Anode sensitivity at $V_b = 1800$ V | Na | 20 | A/lm |
|---|-----------------|----|------|
| Anode dark current at $N_a = 10 \text{ A/lm}^3$) | I _{ao} | 10 | μA |

 1) See spectral response curve in front of this section

 $^2)$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{\rm O}{\rm K}$

 $^{3}\ensuremath{)}$ At an ambient temperature of 25 $^{o}\ensuremath{C}$

7Z2 8091

LIMITING VALUES (Absolute max. rating system)

| Supply voltage | Vb | max. 180 | 0 V |
|---|--------------------|--------------------|------------|
| Continuous anode current | Ia | max. 3 | 0 μΑ |
| Voltage between cathode and first dynode | v_{k/S_1} | max. 30 min. 12 | 0 V 0 V |
| Voltage between consecutive dynodes | $v_{S_n/S_{n+1}}$ | max. 20 min. 8 | 0 V 0 V |
| Voltage between anode and final dynode 1) | v _{a/S10} | max. 20 min. 8 | 0 V 0 V |

RECOMMENDED CIRCUITS







Voltage divider type B

k = cathode $S_n = dynode No.n$ acc = accelerating electrode a = anode

 When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5374

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be sufficient.

Different kinds of voltage dividers are possible. A circuit of type A results in the highest gain of the tube at a given total voltage; a circuit of type B gives a higher current output with better time characteristics, but the total gain is less at the same total voltage.

When pulses with high amplitudes are taken from the anode, it is useful to decouple the last stages as indicated in the circuit by means of capacitors of a few hundred pF, to avoid a voltage drop between these stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.

9 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in laser-technics working in the orange, yellow and green range, under limited dimensional conditions. Its rugged construction makes it particularly suitable for industrial equipment.

| QUICK REFERENCE DA | TA |
|-------------------------------------|--------------|
| Spectral response | type T (S20) |
| Useful diameter of the photocathode | 14 mm |
| Anode sensitivity (at 1800 V) | 100 A/lm |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 12-pin (glass)



ACCESSORIES

S9

S

Socket

Mu-metal shield

type 56073 type 56134

7Z2 8251

TENTATIVE DATA

GENERAL.

| Photocathode | | | |
|--------------------------------------|-------------------|---------------|---------|
| Description | semi-transparent, | head-on, flat | surface |
| Cathode material | Sb-K-Na-Cs | | |
| Minimum useful diameter | | 14 | mm |
| Spectral response curve 1) | | type T (S20 |)) |
| Wavelength at maximum response | | 4200 ± 300 | Å |
| Luminous sensitivity ²) | Nk | 100 | µA/lm |
| Radiant sensitivity at 4200 $ m \AA$ | | 60 | mA/W |
| Multiplier system | | | |
| Number of stages | | 9 | |
| Dynode material | | Ag-Mg-O-O | Cs |
| Capacitances | | | |
| Anode to final dynode | Ca/So | 1.5 | pF |
| Anode to all other electrodes | C _a | 2.5 | pF |
| Shock and vibration | | | |
| To be specified. | | | |
| TYPICAL CHARACTERISTICS | | | |

| With voltage divider A | | | |
|---|-----------------|------|------|
| Anode sensitivity at V_b = 1800 V | Na | 100 | A/lm |
| Anode dark current at $N_a = 30 \text{ A/lm}^3$) | I _{ao} | 0.02 | μΑ |

1) See spectral response curve in front of this section

2) Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{\rm O}{\rm K}$

3) At an ambient temperature of 25 $^{\circ}C$

7Z2 8252

LIMITING VALUES (Absolute max. rating system)

| Supply voltage | Vb | max. | 1800 | V |
|---|-------------------|--------------|------------|----------|
| Continuous anode current | Ia | max. | 1 | mA |
| Voltage between cathode and first dynode | v _{k/S1} | max. min. | 300 120 | V V |
| Voltage between consecutive dynodes | $v_{S_n/S_{n+1}}$ | max. min. | 200 80 | • V V |
| Voltage between anode and final dynode 1) | V _{a/S9} | max. min. | 200 80 | V V |

RECOMMENDED CIRCUITS



Voltage divider type B

When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5384

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be sufficient.

Different kinds of voltage dividers are possible. A circuit of type A results in the highest gain of the tube at a given total voltage; a circuit of type B gives a higher current output with better time characteristics, but the total gain is less at the same total voltage.

When pulses with high amplitudes are taken from the anode, it is useful to decouple the last stages as indicated in the circuit by means of capacitors of a few hundred pF, to avoid a voltage drop between these stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.



Α



Dimensions in mm

10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in optical applications which require a good sensitivity in the ultraviolet region, under limited dimensional conditions.

| QUICK REFERENCE DATA | |
|-------------------------------------|--------------|
| Spectral response | type U (S13) |
| Useful diameter of the photocathode | 14 mm |
| Anode sensitivity (at 1800 V) | 250 A/lm |

DIMENSIONS AND CONNECTIONS

Base: 12-pin (glass)



1

| GENERAL | | | |
|--|-----------------------------|------------|----------------|
| Photocathode | | | |
| Description | semi-transparent, head-or | ı, flat | surface |
| Cathode material | (| Cs-Sb | |
| Minimum useful diameter | | 14 | mm |
| Spectral response curve ¹) | type | U (S13 | 3) |
| Wavelength at maximum response | 4000 | ±300 | Å |
| Luminous sensitivity ²) | N _k av. min. | 70 40 | μA/lm μA/lm |
| Radiant sensitivity at 4000 ${ m \AA}$ | | 60 | mA/W |
| Multiplier system | | | |
| Number of stages | | 10 | |
| Dynode material | Ag-M | Ag-Mg-O-Cs | |
| Capacitances | | | |
| Anode to final dynode | C _{a/S10} | 1.5 | pF |
| Anode to all other electrodes | C _a | 2.5 | pF |
| TYPICAL CHARACTERISTICS | | | |
| With voltage divider A | | | |
| Anode sensitivity at V_b = 1800 V | N _a av. min. | 250 30 | A/lm A/lm |
| Anode dark current at $N_a = 30 \text{ A/lm}^3$) | I _{ao} av. max. | 0.02 | μΑ μΑ |
| Linearity between anode pulse amplitud and input light flux | e up to | 10 | mA |
| | | | |

 1) See spectral response curve in front of this section

 $^2)$ Measured with a tungsten ribbon lamp having a colour temperature of $2850\,^{\rm O}{\rm K}$

³) At an ambient temperature of 25 $^{\circ}C$

7Z2 5387

TYPICAL CHARACTERISTICS (continued)

With voltage divider B

| Linearity between anode pulse amplitude | | | |
|--|-------|-----|----|
| and input light pulse | up to | 30 | mA |
| Anode pulse rise time at V_b = 1800 V 1) | 3.1 | 0-9 | s |
| Total transit time | 30.1 | 0-9 | s |
| | | | |

LIMITING VALUES (Absolute max. rating system)

| Supply voltage | Vb | max. 1800 | V |
|---|--------------------|----------------------|--------|
| Continuous anode current | Ia | max. 1 | mA |
| Voltage between cathode and first dynode | v_{k/S_1} | max. 300 min. 120 | V V |
| Voltage between consecutive dynodes | $v_{S_n/S_{n+1}}$ | max. 200 min. 80 | V V |
| Voltage between anode and final dynode ²) | V _{a/S10} | max. 200 min. 80 | V V |

RECOMMENDED CIRCUITS



Voltage divider type A

¹) For an infinitely short light pulse.

²) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5388

RECOMMENDED CIRCUITS (continued)



Voltage divider type B

= dynode No.n = cathode Sn acc = accelerating electrode a = anode

OPERATIONAL CONSIDERATIONS

k

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be sufficient.

Different kinds of voltage dividers are possible. A circuit of type A results in the highest gain of the tube at a given total voltage; a circuit of type B gives a higher current output with better time characteristics, but the total gain is less at the same total voltage.

When pulses with high amplitudes are taken from the anode, it is useful to decouple the last stages as indicated in the circuit by means of capacitors of a few hundred pF, to avoid a voltage drop between these stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.



A


WINDOWLESS PHOTOMULTIPLIER

The tube is intended for use in applications such as spectroscopy in the far ultraviolet region ($\lambda < 1500$ Å) and soft x-ray counting ($\lambda > 2$ Å).

| QUICK REFERENCE DATA | | |
|--|-------------------------------------|-----------------|
| Quantum efficiency for UV-photons (at 800 Å) | 10 | % |
| Useful area of the Ni photocathode | 22 x 22 | mm ² |
| Gain (at 4000 V) | 5.107 | |
| Dark current | 6.10-12 | А |
| Pressure during operation | 10 ⁻⁵ - 10 ⁻⁶ | mmHg |
| Potted voltage divider | | |

GENERAL

| Photocathode | | | | |
|--------------------------------------|------------|--------------------|------------------|-----------------|
| Description | opaque, he | ad-on, vene | tian blind str | ucture |
| Cathode material | | | Ni | |
| Minimum useful area | | | 22 x 22 | mm^2 |
| Wavelength at maximum response (s | ee fig.1) | | 800 <u>+</u> 100 | 8 |
| Quantum efficiency for UV,-photons a | t 800 Å | | 10 | % |
| Multiplier system | | | | |
| Number of stages | | | 17 | |
| Dynode material | | | Cu-Be-O | |
| Capacitances | | | | |
| Anode to final dynode | | Ca/S ₁₇ | 7 | pF |
| Anode to all other electrodes | | Ca | 9.5 | pF |
| | | | | |

7Z2 5725

TENTATIVE DATA

1

DIMENSIONS AND CONNECTIONS

Dimensions in mm



High voltage connector Signal connector

TYPICAL CHARACTERISTICS

 $\frac{\text{With potted voltage divider}}{\text{Gain at V}_{\text{b}} = 4000 \text{ V}}$ Anode dark current at G = 10⁶

"LEMO" type III C40 H.T.10 "LEMO" type OC50

| G | av. 5.10' | S.m.A. |
|-----|------------|--------|
| Iao | av. 6.10-6 | μΑ |

| LIMITING VALUES (Absolute max. rating s | ystem) | | | |
|--|-----------------------------------|--------------|-----------|--------|
| Supply voltage 1) | Vb | max. | 5000 | V |
| Continuous anode current | Ia | max. | 1 | μΑ |
| Voltage between cathode and first dynode | V _{k/S1} | max. | 500 | V |
| Voltage between consecutive dynodes | vs _n /s _{n+1} | max. min. | 300 80 | V V |
| Voltage between anode and finaly dynode | V _{a/S17} | max. min. | 300 80 | v v |
| Pressure during operation ²) | | max. | 10-5 | mmH |

RECOMMENDED CIRCUIT



potted resistor chain type 56120



- ¹) When the tube is to be used at 5000 V preferably the cathode should be grounded.
- ²) The HT shall never be applied to the tube when the inner pressure exceeds 10^{-5} mmHg. 7Z2 7843

OPERATIONAL CONSIDERATIONS

A good collection on the first dynode of the electrons originating from the cathode is obtained with the eid of an electrostatic focusing system equivalent to the one in the 56AVP-family.

The tube may be used both in counting circuits and integrating current circuits. In the latter case the cathode emission should be at least 10^3 el/sec (approx. 10^{-17} A) while the anode current may never mount to values over 1 μ A. If the cathode emission is lower than 10^3 el/sec it is practically necessary to operate the tube in a pulse circuit.

The tube has a glass envelope which is sealed to a metal flange to facilitate mounting to a vacuum system (vacuum seal with O-ring). The glass envelope is protected by a nickel plated iron mantle, which contains a complete potted voltage divider. The external connections are made via two coaxial connectors. Because of the O-ring the tube may not be heated for outgassing.

The high-vacuum pumps must be provided with a liquid nitrogen trap to avoid oil deposits on the dynodes.

In principle the electrodes are resistant to exposure to dry air but for longer periods in stock it is advised to keep the tube under primary vacuum.

A counter-flange with cock is delivered with the tube.



A



В

WINDOWLESS PHOTOMULTIPLIER

The tube is intended for use in applications such as spectroscopy in the far ultraviolet region ($\lambda < 1400$ Å) detection of ions (> 10 Kev) and electrons (0.1 - 10 Kev).

| QUICK REFERENCE DATA | | |
|--|-------------------------------------|-----------------|
| Quantum efficiency for UV-photons (at 680 A) | 20 | % |
| Useful area of the Cu Be O photocathode | 22 x 22 | mm^2 |
| Gain (at 4000 V) | 5.107 | |
| Dark current | 6.10-12 | А |
| Pressure during operation | 10 ⁻⁵ - 10 ⁻⁶ | mmHg |
| Potted voltage divider | | |

GENERAL

| Photocathode | | | | | |
|--------------------------------------|--------------|----------|--------------------|----------|-----------------|
| Description | opaque, | head-on, | venetian bl | ind stru | ucture |
| Cathode material | | | Cu- | Be-O | |
| Minimum useful area | | | 2 | 2 x 22 | mm ² |
| Wavelength at maximum response (se | e fig.1) | | 680 | ± 100 | A |
| Quantum efficiency for UV-photons at | 680 A | | | 20 | % |
| Multiplier system | | | | | |
| Number of stages | | | | 17 | |
| Dynode material | | | Cu- | -Be-O | |
| Capacitances | | | | | |
| Anode to final dynode | | | C _{a/S17} | 7 | pF |
| Anode to all other electrodes | | | Ca | 9.5 | pF |
| | | | | | |

DIMENSIONS AND CONNECTIONS

Dimensions in mm



High voltage connector Signal connector

TYPICAL CHARACTERISTICS

 $\label{eq:With potted voltage divider} \hline Gain at V_b = 4000 \ V \\ \mbox{Anode dark current at } G = 10^6 \\ \label{eq:Gain}$

"LEMO" type III C40 H.T.10 "LEMO" type OC50

> G av. 5.10^7 I_{ao} av. $6.10^{-6} \mu A$

| LIMITING VALUES (Absolute max. rating | system) | | | |
|--|-----------------------------------|--------------|-----------|--------|
| Supply voltage ¹) | Vb | max. | 5000 | v |
| Continuous anode current | Ia | max. | 1 | μA |
| Voltage between cathode and first dynode | v_{k/S_1} | max. | 500 | V |
| Voltage between consecutive dynodes | vs _n /s _{n+1} | max. min. | 300 80 | v v |
| Voltage between anode and final dynode | V _{a/S17} | max. min. | 300 80 | v v |
| Pressure during operation 2) | | max. | 10-5 | mmHg |
| | | | | |

RECOMMENDED CIRCUIT



potted resistor chain type 56120



- ¹) When the tube is to be used at 5000 V preferably the cathode should be grounded.
- ²) The HT shall never be applied to the tube when the inner pressure exceeds 10^{-5} mmHg. 7Z2 7844

OPERATIONAL CONSIDERATIONS

A good collection on the first dynode of the electrons originating from the cathode is obtained with the aid of an electrostatic focusing system equivalent to the one in the 56AVP-family.

The tube may be used both in counting circuits and integrating current circuits. In the latter case the cathode emission should be at least 10^3 el/sec (approx. 10^{-17} A) while the anode current may never mount to values over 1 μ A. If the cathode emission is lower than 10^3 el/sec it is practically necessary to operate the tube in a pulse circuit.

The tube has a glass envelope which is sealed to a metal flange to facilitate mounting to a vacuum system (vacuum seal with O-ring). The glass envelope is protected by a nickel plated iron mantle, which contains a complete potted voltage divider. The external connections are made via two coaxial connectors. Because of the O-ring the tube may not be heated for outgassing.

The high-vacuum pumps must be provided with a liquid nitrogen trap to avoid oil deposits on the dynodes.

In principle the electrodes are resistant to exposure to dry air but for longer periods in stock it is advised to keep the tube under primary vacuum.

A counter-flange with cock is delivered with the tube.



A



В

WINDOWLESS PHOTOMULTIPLIER

The tube is intended for use in applications such as spectroscopy in the far ultraviolet region ($\lambda < 1500$ Å) and detection of soft x-rays ($\lambda > 2$ Å).

| QUICK REFERENCE DATA | A | |
|--|-------------|-----------------|
| Quantum efficiency for UV-photons (at 800 A) | 10 | % |
| Useful area of the Ni photocathode | 22 x 22 | mm ² |
| Gain (at 4000 V) | 5.107 | |
| Dark current | 6.10-12 | А |
| Pressure during operation | 10-5 - 10-6 | mmHg |
| Potted voltage divider | | |

GENERAL

| Photocathode | | | | | |
|--------------------------------------|--------------|----------|-----------------|------------------|-----------------|
| Description | opaque, | head-on, | venetiar | blind str | ucture |
| Cathode material | | | | Ni | |
| Minimum useful area | | | | 22 x 22 | mm ² |
| Wavelength at maximum response (se | e fig.1) | | 8 | 300 <u>+</u> 100 | 8 |
| Quantum efficiency for UV-photons at | 800 A | | | 10 | % |
| Multiplier system | | | | | |
| Number of stages | | | | 17 | |
| Dynode material | | | (| Cu-Be-O | |
| Capacitances | | | | | |
| Anode to final dynode | | Ca/S | S ₁₇ | 7 | pF |
| Anode to all other electrodes | | Ca | ** | 9.5 | pF |
| | | | | | |

7Z2 5733

TENTATIVE DATA

DIMENSIONS AND CONNECTIONS

Dimensions in mm



High voltage connector Signal connector "LEMO" type III C40 H.T.10 "LEMO" type OC50

av.

G

Ia

TYPICAL CHARACTERISTICS

With potted voltage divider Gain at V_b = 4000 V Anode dark current at G = 10⁶

| 0 | av. | 6.10-6 | μA |
|---|-----|--------|----|
| | | | |

5.107

| stem) | | | |
|-----------------------------------|---|--|--|
| Vb | max. | 5000 | V |
| Ia | max. | 1 | μA |
| v_{k/S_1} | max. | 500 | V |
| vs _n /s _{n+1} | max. min. | 300 80 | v v |
| V _{a/S17} | max. min. | 300 80 | v v |
| | max. | 10 ⁻⁵ | mmHg |
| | stem) V_b I_a V_k/S_1 V_{S_n}/S_{n+1} V_a/S_{17} | $\begin{array}{llllllllllllllllllllllllllllllllllll$ | $\begin{array}{llllllllllllllllllllllllllllllllllll$ |

RECOMMENDED CIRCUIT



potted resistor chain type 56120



- ¹) When the tube is to be used at 5000 V preferably the cathode should be grounded.
- ²) The HT shall never be applied to the tube when the inner pressure exceeds 10⁻⁵ mmHg. 7Z2 7845

OPERATIONAL CONSIDERATIONS

A good collection on the first dynode of the electrons originating from the cathode is obtained with the aid of an electrostatic focusing system equivalent to the one in the 56 AVP-family.

The tube may be used both in counting circuits and integrating current circuits. In the latter case the cathode emission should be at least 10^3 el/sec (approx. 10^{-17} A) while the anode current may never mount to values over 1 μ A. If the cathode emission is lower than 10^3 el/sec it is practically necessary to operate the tube in a pulse circuit.

The tube has a glass envelope which is sealed to a metal flange to facilitate mounting to a vacuum system (vacuum seal with O-ring). The glass envelope is protected by a nickel plated iron mantle, which contains a complete potted voltage divider. The external connections are made via two coaxial connectors. Because of the O-ring the tube may not be heated for outgassing.

The high-vacuum pumps must be provided with a liquid nitrogen trap to avoid oil deposits on the dynodes.

In principle the electrodes are resistant to exposure to dry air but for longer periods in stock it is advised to keep the tube under primary vacuum.

A counter-flange with cock is delivered with the tube.



A



В

WINDOWLESS PHOTOMULTIPLIER

The tube is intended for use in applications such as spectroscopy in the far ultraviolet region ($\lambda < 1400$ Å) detection of ions (> 10 Kev) and electrons (0.1 - 10 Kev).

| QUICK REFERENCE DAT | Ά | |
|--|-------------|-----------------|
| Quantum efficiency for UV-photons (at 680 🎗) | 20 | % |
| Useful area of the Cu Be O photocathode | 22 x 22 | mm ² |
| Gain (at 4000 V) | 5.107 | |
| Dark current | 6.10-12 | A |
| Pressure during operation | 10-5 - 10-6 | mmHg |
| Potted voltage divider | | |

GENERAL

| Filotocatilode | | | | |
|-------------------------------------|-----------------|--------------------|--------------|-----------------|
| Description | opaque, head-or | ı, venetian bli | ind stru | ucture |
| Cathode material | | Cu- | Be-O | |
| Minimum useful area | | 2: | 2 x 22 | mm ² |
| Wavelength at maximum response (s | ee fig.1) | 680 | <u>+</u> 100 | A |
| Quantum efficiency for UV-photons a | nt 680 A | | 20 | % |
| Multiplier system | | | | |
| Number of stages | | | 17 | |
| Dynode material | | Cu- | Be-O | |
| Capacitances | | | | |
| Anode to finaly dynode | | Ca/S ₁₇ | 7 | pF |
| Anode to all other electrodes | | Ca | 9.5 | pF |
| | | | | |

7Z2 5737

TENTATIVE DATA

DIMENSIONS AND CONNECTIONS

Dimensions in mm



High voltage connector Signal connector

"LEMO" type III C40 H.T.10 "LEMO" type OC50

TYPICAL CHARACTERISTICS

With potted voltage divider Gain at V_b = 4000 V Anode dark current at G = 10⁶

G av. 5.10^7 I_{ao} av. 6.10^{-6} μ A 7Z2 5738 LIMITING VALUES (Absolute max. rating system) Supply voltage 1) max. 5000 Vb V Continuous anode current Ia max. 1 μA Voltage between cathode and first dynode V_k/S_1 500 V max. max. 300 V Voltage between consecutive dynodes VS_n/S_{n+1} min. 80 V 300 max. V Voltage between anode and final dynode Va/S17 min. 80 V Pressure during operation 2) max. 10^{-5} mmHg

RECOMMENDED CIRCUIT



potted resistor chain type 56120



- ¹) When the tube is to be used at 5000 V preferable the cathode should be grounded.
- ²) The HT shall never be applied to the tube when the inner pressure exceeds 10^{-5} mmHg. 7Z2 7846

OPERATIONAL CONSIDERATIONS

A good collection on the first dynode of the electrons originating from the cathode is obtained with the aid of an electrostatic focusing system equivalent to the one in the 56AVP-family.

The tube may be used both in counting circuits and integrating current circuits. In the latter case the cathode emission should be at least 10^3 el/sec (approx. 10^{-17} A) while the anode current may never mount to values over 1 μ A. If the cathode emission is lower than 10^3 el/sec it is practically necessary to operate the tube in a pulse circuit.

The tube has a glass envelope which is sealed to a metal flange to facilitate mounting to a vacuum system (vacuum seal with O-ring). The glass envelope is protected by a nickel plated iron mantle, which contains a complete potted voltage divider. The external connections are made via two coaxial connectors. Because of the O-ring the tube may not be heated for outgassing.

The high-vacuum pumps must be provided with a liquid nitrogen trap to avoid oil deposits on the dynodes.

In principle the electrodes are resistant to exposure to dry air but for longer periods in stock it is advised to keep the tube under primary vacuum.

A counter-flange with cock is delivered with the tube.



A



В

WINDOWLESS PHOTOMULTIPLIER

The tube is intended for use in applications such as spectroscopy in the far ultraviolet region ($\lambda < 1500$ Å) and soft x-ray detection ($\lambda > 2$ Å) under ultra high vacuum conditions.

| QUICK REFERENCE DAT | Γ A | |
|--|----------------------|-----------------|
| Quantum efficiency for UV-photons (at 800 Å) | 10 | % |
| Useful area of the Ni photocathode | 22 x 22 | mm ² |
| Gain (at 4000 V) | 5.107 | |
| Dark current | 6.10-12 | А |
| Pressure during operation | $10^{-5} - 10^{-10}$ | mmHg |
| Potted voltage divider | | |

GENERAL

| Photocathode | | | |
|-------------------------------------|--------------|-------------------------|--------|
| Description | opaque, head | on, venetian blind stru | ucture |
| Cathode material | | Ni | |
| Minimum useful area | | 22 x 22 | mm2 |
| Wavelength at maximum response (s | see fig.1) | 800 <u>+</u> 100 | Å |
| Quantum efficiency for UV-photons a | at 800 Å | 10 | % |
| Multiplier system | | | |
| Number of stages | | 17 | |
| Dynode material | | Cu-Be-O | |
| Capacitances | | | |
| Anode to final dynode | | 7 | pF |
| Anode to all other electrodes | | 9.5 | pF |
| | | | |

7Z2 5741

TENTATIVE DATA

1

DIMENSIONS AND CONNECTIONS

Dimensions in mm



"LEMO" type III C40 H.T.10 "LEMO" type OC50

G





TYPICAL CHARACTERISTICS

With potted voltage divider Gain at V_b = 4000 V Anode dark current at $G = 10^6$

6.10⁻⁶ µA Iao

5.107

| LIMITING VALUES (Absolute max. rating sy | /stem) | | |
|--|-----------------------------------|-----------------------|--------|
| Supply voltage ¹) | Vb | max. 5000 | V |
| Continuous anode current | Ia | max. 1 | μA |
| Voltage between cathode and first dynode | V_k/S_1 | max. 500 | V |
| Voltage between consecutive dynodes | V _{Sn} /S _{n+1} | max. 300 min. 80 | v v |
| Voltage between anode and final dynode | V _{a/S17} | max. 300 min. 80 | v v |
| Pressure during operation ²) | | max. 10 ⁻⁵ | mmHg |

RECOMMENDED CIRCUIT



- ¹) When the tube is to be used at about 5000 V preferable the cathode should be grounded, to avoid gas emission from the focusing electrodes of the input.
- ²) The HT shall never be applied to the tube when the inner pressure exceeds 10^{-5} mmHg. 7Z2 7848

OPERATIONAL CONSIDERATIONS

A good collection on the first dynode of the electrons originating from the cathode is obtained with the aid of an electrostatic focusing system equivalent to the one in the 56AVP-family.

The tube may be used both in counting circuits and integrating current circuits. In the latter case the cathode emission should be at least 10^3 el/sec (approx. 10^{-17} A) while the anode current may never mount to values over 1 μ A. If the cathode emission is lower than 10^3 el/sec it is practically necessary to operate the tube in a pulse circuit.

The tube has a stainless steel envelope and a heavy flange to facilitate mounting to a vacuum system (gold foil vacuum seal). The envelope contains also a complete potted voltage divider. The external connections are made via two coaxial connectors.

The tube may be heated to 300 $^{\circ}$ C for several hours to obtain an ultra high vacuum (10⁻¹⁰ mmHg), but this must be done with care. The temperature of the glass bottom with the pins must be kept always at about the same level as the one of the stainless steel flange by which it is carried. The potted resistor chain must be taken apart.

The high-vacuum pumps must be provided with a liquid nitrogen trap to avoid oil deposits on the dynodes.

In principle the electrodes are resistant to exposure to dry air but for longer periods in stock it is advised to keep the tube under primary vacuum. A counter flange with cock is delivered with the tube.



A



В

WINDOWLESS PHOTOMULTIPLIER

The tube is intended for use in applications such as spectroscopy in the far ultraviolet region ($\lambda < 1400$ Å), detection of ions (> 10 Kev) and electrons (0.1 - 10 Kev), under ultra high vacuum conditions.

| QUICK REFERENCE DATA | | | | |
|--|----------------------|-----------------|--|--|
| Quantum efficiency for UV-photons (at 680 A) | 20 | % | | |
| Useful area of the Cu Be O photocathode | 22 x 22 | mm ² | | |
| Gain (at 4000 V) | 5.107 | | | |
| Dark current | 6.10-12 | А | | |
| Pressure during operation | $10^{-5} - 10^{-10}$ | mmHg | | |
| Potted voltage divider | | | | |

GENERAL

| Photocathode | | | | | |
|--------------------------------------|--------------|----------|----------------|------------------|-----------------|
| Description | opaque, | head-on, | venetiar | n blind stru | ucture |
| Cathode material | | | | Cu-Be-O | |
| Minimum useful area | | | | 22 x 22 | mm ² |
| Wavelength at maximum response (se | e fig.1) | | | 680 <u>+</u> 100 | 8 |
| Quantum efficiency for UV-photons at | 680 A | | | 20 | % |
| Multiplier system | | | | | |
| Number of stages | | | | 17 | |
| Dynode material | | | | Cu-Be-O | |
| Capacitances | | | | | |
| Anode to final dynode | | | $C_{a/S_{17}}$ | 7 | pF |
| Anode to all other electrodes | | | Ca | 9.5 | pF |
| | | | | | |

7Z2 5745

TENTATIVE DATA

DIMENSIONS AND CONNECTIONS

Dimensions in mm



High voltage connector Signal connector

"LEMO" type III C40 H.T.10 "LEMO" type OC50

TYPICAL CHARACTERISTICS

With potted voltage divider Gain at V_b = 4000 V Anode dark current at G = 10⁶

| G | av. | 5.107 | |
|-----|-----|--------|----|
| Iao | av. | 6.10-6 | μA |

| LIMITING VALUES (Absolute max. rating | system) | | | |
|--|--------------------------------|--------------|------------------|--------|
| Supply voltage 1) | V _b | max. | 5000 | V |
| Continuous anode current | I _a | max. | 1 | μA |
| Voltage between cathode and first dynode | V _k /S ₁ | max. | 500 | V |
| Voltage between consecutive dynodes | $v_{S_n/S_{n+1}}$ | max. min. | 300 80 | V V |
| Voltage between anode and final dynode | V _{a/S17} | max. min. | 300 80 | V V |
| Pressure during operation 2) | | max. | 10 ⁻⁵ | mmHg |

RECOMMENDED CIRCUIT



- When the tube is to be used at about 5000 V preferable the cathode should be grounded, to avoid gas emission from the focusing electrodes of the input.
- ²) The HT shall never be applied to the tube when the inner pressure exceeds 10^{-5} mmHg.

OPERATIONAL CONSIDERATIONS

A good collection on the first dynode of the electrons originating from the cathode is obtained with the aid of an electrostatic focusing system equivalent to the one in the 56AVP-family.

The tube may be used both in counting circuits and integrating current circuits. In the latter case the cathode emission should be at least 10^3 el/sec (approx. 10^{-17} A) while the anode current may never mount to values over 1 μ A. If the cathode emission is lower than 10^3 el/sec it is practically necessary to operate the tube in a pulse circuit.

The tube has a stainless steel envelope and a heavy flange to facilitate mounting to a vacuum system (gold foil vacuum seal). The envelope contains also a complete potted voltage divider. The external connections are made via two coaxial connectors.

The tube may be heated to 300 $^{\rm O}{\rm C}$ for several hours to obtain an ultra high vacuum (10⁻¹⁰ mmHg), but this must be done with care. The temperature of the glass bottom with the pins must be kept always at about the same level as the one of the stainless steel flange by which it is carried. The potted resistor chain must be taken apart.

The high-vacuum pumps must be provided with a liquid nitrogen trap to avoid oil deposits on the dynodes.

In principle the electrodes are resistant to exposure to dry air but for longer periods in stock it is advised to keep the tube under primary vacuum. A counter flange with cock is delivered with the tube.



A



В
6 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in plasma physics where high light flashes must be measured and other applications where a high degree of time definition and linearity is required.

| *nan 9.6 x 2.89 | QUICK REFERENCE DATA | and press |
|-----------------------|----------------------|-----------------|
| Spectral response | type S4 | h ring |
| Useful window area | 150 | mm ² |
| Gain (at 3750 V) | 104 | |
| Anode pulse rise time | 1.7 | ns |
| Linearity | up to 2 | А |
| Peak current | 4 | А |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 14-pin (Jedec B14-38)



7Z2 8253

ACCESSORIES

| Socket | type | FE1001 | |
|-----------------|------|--------|--|
| Mu-metal shield | type | 56128 | |

GENERAL

| Photocathode | | | |
|--------------------------------|-----------|---------------------|----------------|
| Description | opaque, h | nead-on, flat | window |
| Cathode material | | Cs-Sb | |
| Minimum useful window area | | 25.5 x 5.9 | mm^2 |
| Spectral response curve | | type S4 | |
| Wavelength at maximum response | | 4000 <u>+</u> 500 | A |
| Luminous sensitivity 1) | Nk | av. 45 min. 25 | μA/lm μA/lm |
| Radiant sensitivity at 4200 Å | | 35 | mA/W |
| Multiplier system | | i * ipto n energ | |
| Number of stages | | 6 | |
| Dynode material | | Ag-Mg-O-O | Cs |

TYPICAL CHARACTERISTICS

| with recommended voltage divider | | | | |
|--|----------------|-------------|--------------|----------|
| Supply voltage for $G = 10^4$ | v _b | av. max. | 3750 5000 | v v |
| Anode dark current at $G = 10^4 2$) | Iao | av. max. | 0.03 | μΑ μΑ |
| Linearity (within 5%) between anode pulse amplitude and input light pulse | | up to | 2 | А |
| Supply voltage for a linearity of 2 A | v _b | av. max. | 6000 6500 | v v |

 1) Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^0\mathrm{K}$ $^2)$ At an ambient temperature of 25 $^0\mathrm{C}$ 7Z2 8254

117:41

TYPICAL CHARACTERISTICS (continued)

1 1

| with recommended voltage divider | | |
|---|-------------------|---|
| Anode pulse rise time at V_b = 6500 V 1) | $1.7 \ge 10^{-9}$ | s |
| Anode pulse width at half height at V_b = 6500 V ¹) | $3 \ge 10^{-9}$ | s |
| Total transit time at V_b = 6500 V 1) | $11 \ge 10^{-9}$ | s |
| Maximum peak current | 4 | А |

LIMITING VALUES

Supply voltage Continuous anode current

max. 7000 V Vb Ia max. 2 m

RECOMMENDED CIRCUIT



¹) For an infinitely short light pulse, fully illuminating the photocathode.

7Z2 8255

k

a

OPERATIONAL CONSIDERATIONS

A. The multiplier system of the tube is equivalent to the one in the XP1141. The first stage of this multiplier system is used as a cathode so the actual number of dynodes is 6, providing a total current amplification of 10^4 at about 3500 V.

The tube is capable of producing very strong peak currents (up to 6 A). Actually the time constant at the output of the multiplier must be very small. Therefore it is necessary to use a low load resistance, well matched to the associated electronic circuitry. With a load of 50 Ω the tube easily delivers pulses of tens of volts, so that an amplifier is rendered superfluous, without attenuation or distortion. All stages must be decoupled by means of capacitances to avoid a serious voltage drop on the dynodes.

To avoid the effects, which are responsible for rounding of the leading edge and the "jagged" trailing edges, a shadow grid (g_2) is placed parallel to the anode with its wires aligned with those of the anode.

Thus electrons walking from the next-to-last dynode (S_5) to the last dynode (S_6) are prevented to impinge directly upon the anode. At the same time induction and oscillations in the anode grid are minimized.

B. The following test procedure for linearity is used:

A very short light pulse is seen by 2 photomultiplier tubes one of which is a perfect linear reference tube and the other one the tube to be measured. The signals of both tubes are fed in phase to an oscilloscope.

The measurements are done with a voltage divider as indicated, starting with a total voltage of 4.8 kV.

Observing the oscillogramme and at the same time regulating simultaneously the tensions between $S_2 - S_3$ and $S_3 - S_4$, it is possible to find a compromise between linearity and absence of oscillations. After this the voltage between S_6 - a is increased in order to get a linearity as specified; eventually the whole procedure has to be repeated.

Each tube is accompanied by a test-card which indicates the voltages between $S_2 - S_3$, $S_3 - S_4$ and S_6 - a, at which a linearity (within 5%) of 2 A is obtained.

REMARKS

- 1. It is possible to obtain linearities even higher than 3 A by a more complicated procedure with each individual tube. Starting from the recommended voltage divider each interstage tension has to be adjusted independently and carefully.
- Linearity within 5% is defined as follows: the output pulse amplitude (up till 2 A) as a function of the input light pulse amplitude will not deviate more than 5% from a straight line.
 7Z2 5892



Α



7 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in plasma physics where high light flashes must be measured and other applications where a high degree of time definition and linearity is required.

| QUICK REFERENCE DA | TA | |
|-------------------------------------|---------|-------|
| Spectral response | type A | (S11) |
| Useful diameter of the photocathode | 42 | mm |
| Gain (at 3500 V) | 104 | |
| Anode pulse rise time | 1.9 | ns |
| Linearity | up to 1 | А |
| Peak current | 3 | А |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 14-pin (Jedec B14-38)



7Z2 8095

ACCESSORIES

| Socket | type | FE1001 | |
|-----------------|------|--------|--|
| Mu-metal shield | type | 56130 | |

GENERAL

Photocathode semi-transparent, low resistivity, head-on, curved surface Description Cathode material Cs-Sb Minimum useful diameter 42 mm Radius of curvature 72 + 2 mm Spectral response curve type A (S11) 4200 + 300 Å Wavelength at maximum response 55 μ A/lm av. Luminous sensitivity 2) Nk min. 25 $\mu A/lm$ Radiant sensitivity at 4200 Å 50 mA/W Multiplier system

Number of stages

Dynode material

TYPICAL CHARACTERISTICS

With recommended voltage divider

| Supply voltage for $G = 10^4$ | Vb | av. max. | 3500 6500 | V V |
|--|-----------------|-------------|--------------|----------|
| Anode dark current at G = 10^4 ³) | I _{ao} | av. max. | 0.1 20 | μΑ μΑ |
| Linearity (within 5%) between anode pulse amplitude and input light pulse | | up to | 1 | А |
| Supply voltage for a linearity of 1 A | v _b | av. max. | 6000 6500 | v v |

¹) See spectral response curve in front of this section

²) Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{\rm O}$ K

³) At an ambient temperature of 25 ^oC

7Z2 8255

GMA PROTEIN

Ag-Mg-O-Cs

max. 7000

max.

V

2 mA

| TITIONE CIMANCIERISTICS (Continued) | | |
|---|-----------------------|---|
| With recommended voltage divider (continued) | | |
| Anode pulse rise time at V_b = 6500 V ¹) | 1.9×10^{-9} | s |
| Anode pulse width at half height at V_b = 6500 V ¹) | 3.2×10^{-9} | s |
| Total transit time at V_b = 6500 V ⁻¹) | 16 x 10 ⁻⁹ | s |
| Maximum peak current | 3 | А |
| | | |

Vb

Ia

laantin

LIMITING VALUES (Absolute max. rating system)

Supply voltage

Continuous anode current



TYDICAL CHADACTEDISTICS



Voltage divider

| | | R1 - 47 K32 R3 - | $C_{1} = 2000 \text{ pr/okv}$ |
|----------------|---|------------------------|--|
| | | $R_2 = 100 \Omega$ | $C_2 = 10000 \text{ pF/3kV}$ |
| k | = | cathode | voltage between k and g_1 to be adjusted at |
| g ₁ | = | focusing electrode | about $2V_s$; voltage between k and acc to be |
| acc | = | accelerating electrode | adjusted at about 15 V _S ; voltages between |
| g2 | = | focusing electrode | S_4 - S_5 and S_7 -a to be adjusted for maximum |
| g3 | = | deflector | linearity (see operational considerations). |
| Sn | = | dynode No.n | |
| g4 | = | shadow grid | |
| a | = | anode | n-nan silt mort paizles enormale shift or |

¹) For an infinitely short light pulse, fully illuminating the photocathode.

7Z2 8096

OPERATIONAL CONSIDERATIONS

A. The electron optical input system consists of five elements:

the photocathode k; the focusing electrode g_1 ; the focusing electrode g_2 ; the accelerating electrode acc; the deflector g_3 .

To reduce transit-time fluctuations, geometrical time spread, pulse amplitude spread or dark current, this system has the following advantages:

- 1. the photocathode is curved, thus minimizing geometrical time spread;
- 2. a high and homogeneous extraction field at the cathode reduces as much as possible the influence of the initial electron velocities. This field is homogenized at the cathode surface by the focusing electrode g_1 .
- 3. The potential of electrode g_1 to the photocathode can be adjusted in order to obtain one of the following characteristics:
 - a. the most satisfactory collection (i.e. for a given luminous flux the largest obtainable anode signal); the optimum value of the potential is about 2 V_s;
 - b. the slightest transit-time fluctuations (the most homogeneous extraction field);
 - c. the most satisfactory uniformity of collection giving the most constant output amplitude.
- 4. Because the first dynode cannot be placed parallel to the photocathode, the beam of primary electrons is deflected by the deflector to make it impinge at right angles to the first dynode surface.
- B. The multiplier system consists of 7 stages, providing a total current amplification of 10⁴ at about 3500 V.

The tube is capable of producing very strong peak currents (up to 3 A). Actually the time constant at the output of the multiplier must be very small. Therefore it is necessary to use a low load resistance, well matched to the associated electronic circuitry. With a load of 50 Ω the tube easily delivers pulses of tens of volts, so that an amplifier is rendered superfluous, without attenuation or distortion. All stages must be decoupled by means of capacitances to avoid a serious voltage drop on the dynodes.

To avoid the effects, which are responsible for rounding of the leading edge and the "jagged" trailing edges, a shadow grid (g_4) is placed parallel to the anode with its wires aligned with those of the anode.

Thus electrons walking from the next-to-last dynode (S_6) to the last dynode (S_7) are prevented to impinge directly upon the anode. At the same time induction and oscillations in the anode grid are minimized.

C. The following test procedure for linearity is used:

A very short light pulse is seen by 2 photomultiplier tubes one of which is a perfect linear reference tube and the other one the tube to be measured. The signals of both tubes are fed in phase to an oscilloscope.

The measurements are done with a voltage divider as indicated, starting with a total voltage of 4.8 kV. Observing the oscillogramme and at the same time regulating the tension between $S_4 - S_5$, it is possible to find a compromise between linearity and absence of oscillations. After this the voltage between S_7 -a is increased in order to get a linearity as specified; eventually the whole procedure has to be repeated.

Each tube is accompanied by a test-card which indicates the voltages between $S_4 - S_5$ and $S_7 - a$, at which a linearity (within 5%) of 1 A is obtained.

REMARKS

- 1. It is possible to obtain linearities even higher than 1 A by a more complicated procedure with each individual tube. Starting from the recommended voltage divider each interstage tension has to be adjusted independently and carefully.
- 2. Linearity within 5% is defined as follows: the output pulse amplitude (up till 1 A) as a function of the input light pulse amplitude will not deviate more than 5% from a straight line.



A

10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in applications such as scintillation counting, in small medical probes or in portable equipment or any optical or nuclear application in which a small diameter is required.

| QUICK REFERENCE DAT | ГА |
|-------------------------------------|--------------|
| Spectral response | type A (S11) |
| Useful diameter of the photocathode | 20 mm |
| Anode sensitivity (at 1800 V) | 250 A/lm |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 13-pin (glass)



ACCESSORIES

Socket

Mu-metal shield

type B8 700 67 type 56138

7Z2 8092

TENTATIVE DATA

| GENERAL . | | | | |
|--|----------------------|-------------|----------------|---------------------|
| Photocathode | | | | |
| Description | semi-transparent, | head-on | , flat | surface |
| Cathode material | | C | cs-Sb | |
| Minimum useful diameter | | | 20 | mm |
| Spectral reponse curve ¹) | | type | A (S1 | i) |
| Wavelength at maximum response | | 4200 - | <u>+</u> 300 | 8 |
| Luminous sensitivity ²) | Nk | av. min. | 60 35 | μA/lm μA/lm |
| Radiant sensitivity at 4200 Å | | | 50 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 10 | |
| Dynode material | | Ag-M | g - 0-0 | Cs |
| Capacitances | | Pantos | | |
| Anode to final dynode | C_a/S_{10} | | 3 | pF |
| Anode to all other electrodes | C _a | | 5 | pF |
| TYPICAL CHARACTERISTICS | | | | |
| With voltage divider A | | | | |
| Anode sensitivity at V_b = 1800 V | Na | av. min. | 250 30 | A/lm A/lm |
| Anode dark current at $N_a = 30 \text{ A/lm}^3$) | I _{ao} | av. max. | 0.02 | μΑ μΑ |
| Linearity between anode pulse amplitud and input light pulse | le | up to | 5 | mA |
| With voltage divider B | | | | |
| Linearity between anode pulse amplitud and input light pulse | le | up to | 10 | mA |
| ¹) See spectral response curve in front | of this section | | | |
| $^{2}\ensuremath{)}$ Measured with a tungsten ribbon lam | p having a colour to | emperatu | re of | 2850 ^o K |
| $^{3}\ensuremath{)}$ At an ambient temperature of 25 $^{0}\ensuremath{\mathrm{C}}$ | | | 7 | Z2 8217 |

LIMITING VALUES (Absolute max. rating system)

| Supply voltage | Vb | max. | 1800 | V |
|---|--------------------|--------------|------------|--------|
| Continuous anode current | Ia | max. | 1 | mA |
| Voltage between cathode and first dynode | v_{k/S_1} | max. min. | 500 120 | v v |
| Voltage between consecutive dynodes | $v_{s_n/s_{n+1}}$ | max. min. | 300 80 | v v |
| Voltage between anode and final dynode 1) | V _{a/S10} | max. min. | 300 80 | v v |

RECOMMENDED CIRCUITS







¹) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 8218

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be sufficient.

In pulse techniques, such as scintillation counting, it is advisable to decouple the last two or three stages by means of capacitors of approx. 100 pF, to avoid a serious voltage drop between these stages during a pulse.

With the voltage divider type A the tube gives the highest gain, while with the voltage divider type B the tube can deliver higher anode currents at the cost of the total gain.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against magnetic field influence.



Α



11 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in applications such as scintillation counting of α , β , γ , n radiation and X rays, in flying-spot apparatus and different kinds of optical instruments.

| QUICK REFERENCE DATA | | ante data |
|-------------------------------------|--------|-----------|
| Spectral response | type . | A (S11) |
| Useful diameter of the photocathode | 44 | mm |
| Anode sensitivity (at 1800 V) | 1000 | A/lm |

DIMENSIONS AND CONNECTIONS

S11

50

53

770073

Dimensions in mm

Base: 14-pin (Jedec B14-38)





ACCESSORIES

Si

S8 56

54

SZ

acc.S1

Socket

Mu-metal shield

FE1001 type 56128 type

7Z2 5462

MAINTENANCE TYPE

53AVP

GENERAL

| Photocathode | | | | |
|--|-----------------|-------------|------------------|----------------|
| Description semi- | -transparent, | head-o | on, flat | surface |
| Cathode material | | | Cs-Sb | |
| Minium useful diameter | | | 44 | mm |
| Spectral response curve ¹) | | type | A (S11) | |
| Wavelength at maximum response | | 4200 |) <u>+</u> 300 | 8 |
| Luminous sensitivity ²) | Nk | av. min. | 70 40 | μA/lm μA/lm |
| Radiant sensitivity at 4200 Å | | | 60 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 11 | |
| Dynode material | | Ag-N | lg - O-Cs | |
| Capacitances | | | | |
| Anode to final dynode | Ca/S11 | | 3 | pF |
| Anode to all other electrodes | Ca | | 5 | pF |
| TYPICAL CHARACTERISTICS | | | | |
| With voltage divider A | | | | |
| Anode sensitivity at V_b = 1800 V | Na | av. min. | 1000 250 | A/lm A/lm |
| Anode dark current at $N_a = 60 \text{ A/lm}^3$) | I _{ao} | av. max. | 0.015 0.050 | μΑ μΑ |
| Linearity between anode pulse amplitude and input light pulse | | up to | 30 | mA |

 1) See spectral response curve in front of this section

 $^2)$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^0\mathrm{K}$

³) At an ambient temperature of 25 $^{\rm O}{\rm C}$

7Z2 5463

max.

min.

Va/S11

300

80 V

V

| TYPICAL CHARACTERISTICS (continued) | | | |
|---|-----------------------------------|----------------------|--------|
| With voltage divider B | | | |
| Linearity between anode pulse amplitude and input light pulse | | up to 100 | mA |
| Anode pulse rise time at V _b = 1500 V 1) | | 5.10-9 | s |
| Transit time difference between the centre of the photocathode and the edge at $V_b = 1500 V$ | | 4.10 ⁻⁹ | s |
| Total transit time at V_b = 1500 V | | 45.10 ⁻⁹ | s |
| LIMITING VALUES (Absolute max. rating sy | stem) | | |
| Supply voltage | Vb | max. 1800 | V |
| Continuous anode current | Ia | max. 1 | mA |
| Voltage between cathode and first dynode | v_{k/S_1} | max. 500 min. 120 | v v |
| Voltage between consecutive dynodes | vs _n /s _{n+1} | max. 300 min. 80 | v v |

Voltage between anode and final dynode 2)

RECOMMENDED CIRCUITS



k = cathode S_n = dynode No.n acc = accelerating electrode a = anode

1) For an infinitely short light pulse

²) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked 7Z2 5464

53AVP

RECOMMENDED CIRCUITS (continued)



Voltage divider type B

| k | = | cathode | Sn | = | dynode No.r |
|-----|---|------------------------|----|---|-------------|
| acc | = | accelerating electrode | а | = | anode |

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA to 1 mA will be sufficient.

Different kinds of voltage dividers are possible. A circuit of type A results in the highest gain of the tube at a given total voltage; a circuit of type B gives a higher current output with better time characteristics, but the total gain is less at the same total voltage.

When pulses with high amplitudes are taken from the anode, it is useful to decouple the last stages as indicated in the circuit by means of capacitors of a few hundred pF, to avoid a voltage drop between these stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after soveral hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.

53 AVP



A



11 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for optical spectrometry, ultraviolet photometry and other applications which require a good sensitivity in the ultraviolet region.

| QUICK REFERENCE DATA | direction |
|-------------------------------------|--------------|
| Spectral response | type U (S13) |
| Useful diameter of the photocathode | 44 mm |
| Anode sensitivity (at 1800 V) | 1000 A/lm |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 14-pin (Jedec B14-38)



ACCESSORIES

SockettypeFE1001Mu-metal shieldtype56128

7Z2 5458

| GENERAL | | | | |
|---|--------------------|----------------|-------------|----------------|
| Photocathode | | | | |
| Description | semi-transparent, | head-on | , flat | surface |
| Cathode material | | C | s-Sb | |
| Minimum useful diameter | | | 44 | mm |
| Spectral response curve ¹) | | type U | (S13) | ar el T |
| Wavelength at maximum response | | 4000 <u>+</u> | 300 | A |
| Luminous sensitivity ²) | N _k | av. min. | 70 40 | μA/lm μA/lm |
| Radiant sensitivity at 4000 $	frac{A}$ | | | 60 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 11 | |
| Dynode material | | Ag-Mg | -0-Cs | 5 |
| Capacitances | | | | |
| Anode to final dynode | C _{a/S11} | | 3 | pF |
| Anode to all other electrodes | C _a | | 5 | pF |
| TYPICAL CHARACTERISTICS | | | | |
| With voltage divider A | | | | |
| Anode sensitivity at V_b = 1800 V | Na | av. min. | 1000 250 | A/lm A/lm |
| Anode dark current at N _a = 60 A/lm 3) | I _{ao} | av. 0 max.0 | .015 | μΑ μΑ |
| Linearity between anode pulse amplitud and input light pulse | e | up to | 30 | mA |
| | | | | |

 $^{1})$ See spectral response curve in front of this section

²) Measured with a tungsten ribbon lamp having a colour temperature of 2850 ^oK ³) At an ambient temperature of 25 ^oC 7Z2 5459

max. 300

min.

max.

min.

 VS_n/S_{n+1}

 $v_{a/S_{11}}$

V

80 V

300 V

80 V

| TYPICAL CHARACTERISTICS (continued) | | | |
|---|-------------|----------------------|--------|
| With voltage divider B | | | |
| Linearity between anode pulse amplitude and input light pulse | | up to 100 | mA |
| Anode pulse rise time at V _b = 1500 V 1) | | 5.10-9 | s |
| Transit time difference between the centre of the photocathode and the edge at $V_{\rm b}$ = 1500 V | | 4.10 ⁻⁹ | s |
| Total transit time at V_b = 1500 V | | 45.10-9 | s |
| LIMITING VALUES (Absolute max. rating syst | em) | | |
| Supply voltage | Vb | max. 1800 | V |
| Continuous anode current | Ia | max. 1 | mA |
| Voltage between cathode and first dynode | v_{k/S_1} | max. 500 min. 120 | V V |

Voltage between consecutive dynodes

Voltage between anode and final dynode 2)

RECOMMENDED CIRCUITS



acc = accelerating electrode a = anode

¹) For an infinitely short light pulse

²) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked 7Z2 5460

RECOMMENDED CIRCUITS (continued)



Voltage divider type B

| k | = | cathode | Sn | = | dynode No.n |
|-----|---|------------------------|----|---|-------------|
| acc | = | accelerating electrode | а | = | anode |

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA to 1 mA will be sufficient.

Different kinds of voltage dividers are possible. A circuit of type A results in the highest gain of the tube at a given total voltage; a circuit of type B gives a higher current output with better time characteristics, but the total gain is less at the same total voltage.

When pulses with high amplitudes are taken from the anode, it is useful to decouple the last stages as indicated in the circuit by means of capacitors of a few hundred pF, to avoid a voltage drop between these stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of mangetic fields.



A



11 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in applications such as scintillation counting with large crystals, or applications in which light must be gathered from a diffusely reflecting surface (e.g. flying-spot techniques in colour printing) or from a distant source.

| QUICK REFERENCE DATA | | |
|-------------------------------------|--------|---------|
| Spectral response | type . | A (S11) |
| Useful diameter of the photocathode | 111 | mm |
| Anode sensitivity (at 1800 V) | 500 | A/lm |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 14-pin (Jedec B14-38)





7Z2 7851

54 AVP

ACCESSORIES

| Socket | type | FE1001 |
|-----------------|------|--------|
| Mu-metal shield | type | 56129 |

GENERAL

| Photocathode | | | | |
|---|--------------------|---------------|---------------|----------------|
| Description | semi-transparent, | head-on, | flat | surface |
| Cathode material | | C | s-Sb | |
| Minimum useful diameter | | | 111 | mm |
| Spectral response curve 1) | | type A | (S11) |) |
| Wavelength at maximum response | | 4200 <u>+</u> | 300 | R |
| Luminous sensitivity ²) | Nk | av. min. | 60 40 | μA/lm μA/lm |
| Radiant sensitivity at 4200 $ m \AA$ | | | 50 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 11 | |
| Dynode material | Ag-Mg-O-Cs | | | s |
| Capacitances | | | | |
| Anode to final dynode | C _{a/S11} | | 3 | pF |
| Anode to all other electrodes | Ca | | 5 | pF |
| TYPICAL CHARACTERISTICS | | | | |
| With voltage divider A | | | | |
| Anode sensitivity at V_b = 1800 V | Na | av. min. | 500 100 | A/lm A/lm |
| Anode dark current at $N_a = 250 \text{ A/lm}^3$ |) I _{ao} | max. | 0.2 0.5 | μΑ μΑ |
| Linearity between anode pulse amplitud and input light pulse | e | up to | 30 | mA |

¹⁾ See spectral response curve in front of this section

2) Measured with a tungsten ribbon lamp having a colour temperature of 2850 °K
3) At an ambient temperature of 25 °C 7Z2 5659



| TYPICAL CHARACTERISTICS (continued) | | |
|---|-----------|----|
| With voltage divider B | | |
| Linearity between anode pulse amplitude and input light pulse | up to 100 | mA |
| Anode pulse rise time at V_b = 2000 V ¹) | 7.10-9 | s |
| Anode pulse width at half height at $V_{\rm b}$ = 2000 V | 18.10-9 | s |
| Transit time difference between the centre of the photocathode and the edge at V_b = 2000 V | 15.10-9 | s |
| Total transit time at V_b = 2000 V | 70.10-9 | s |
| | | |

LIMITING VALUES (Absolute max. rating system)

| Supply voltage | Vb | max. | 2000 | V | |
|---|--------------------|--------------|------------|--------|--|
| Continuous anode current | Ia | max. | 1 | mA | |
| Voltage between cathode and first dynode | v _{k/S1} | max. min. | 500 120 | V V | |
| Voltage between consecutive dynodes | $v_{S_n/S_{n+1}}$ | max. min. | 300 80 | V V | |
| Voltage between anode and final dynode ²) | V _{a/S11} | max. min. | 300 80 | V V | |

RECOMMENDED CIRCUITS



Voltage divider type A

k = cathode
acc = accelerating electrode

S_n = dynode No.n a = anode

1) For an infinitely short light pulse

2) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5660

RECOMMENDED CIRCUITS (continued)



Voltage divider type B

| k | = | cathode | Sn | = | dynode No.n |
|-----|---|------------------------|----|---|-------------|
| acc | = | accelerating electrode | а | = | anode |

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of about 1 mA will be sufficient.

With the voltage divider type A the tube gives the highest gain, while with the voltage divider type B the tube can deliver a higher anode current output with better time characteristics.

The accelerating electrode has a separate external connection to allow adjustment for optimum photoelectron collection on the first dynode.

In pulse techniques, such as scintillation counting, it is advisable to decouple the last two or three stages by means of capacitors of 100 pF and 200 pF (the highest value at the last stage).

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.

54 AVP



A




11 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in applications which require a good sensitivity in the ultra-violet region, combined with a photosensitive area larger than usual.

| QUICK REFERENCE DATA | |
|-------------------------------------|--------------|
| Spectral response | type U (S13) |
| Useful diameter of the photocathode | 111 mm |
| Anode sensitivity (at 1800 V) | 500 A/lm |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 14-pin (B14-38)





7Z2 7852

1.1.1967

1

54UVP

| ACCESSORIES | | | | | | |
|---|------|-----------------|--------|-------------|------------|----------------|
| Socket | type | FE100 | 1 | | | |
| Mu-metal shield | type | 56129 | | | | |
| GENERAL | | | | | | |
| Photocathode | | | | | | |
| Description | semi | -transpa | arent, | head-on | , flat | surface |
| Cathode material | | | | C | s-Sb | |
| Minimum useful diameter | | | | | 111 | mm |
| Spectral response curve 1) | | | | type U | (S13) | |
| Wave length at maximum response | | | | 4000 ± | . 300 | R |
| Luminous sensitivity ²) | | N _k | | av. min. | 60 40 | μA/lm μA/lm |
| Radiant sensitivity at 4000 Å | | | | | 50 | mA/W |
| Multiplier system | | | | | | |
| Number of stages | | | | | 11 | |
| Dynode material | | | | Ag-Mg | -0-Cs | 5 |
| Capacitances | | | | | | |
| Anode to final dynode | | Ca/S | | | 3 | pF |
| Anode to all other electrodes | | C _a | 11 | | 5 | pF |
| | | | | | | |
| TYPICAL CHARACTERISTICS | | | | | | |
| With voltage divider A | | | | | | |
| Anode sensitivity at V_b = 1800 V | | Na | | av. min. | 500 100 | A/lm A/lm |
| Anode dark current at $N_a = 250 \text{ A/lm}^3$ |) | I _{ao} | | av. max. | 0.2 0.5 | μΑ μΑ |
| Linearity between anode pulse amplitud and input light pulse | е | | | up to | 30 | mA |
| | | | | | | |

1) See spectral response curve in front of this section
2) Measured with a tungsten ribbon lamp having a colour temperature of 2850 °K
3) At an ambient temperature of 25 °C 7Z2 5663

TYPICAL CHARACTERISTICS (continued)

With voltage divider B

| Linearity between anode pulse amplitude | | |
|--|-----------|----|
| and input light pulse | up to 100 | mA |
| Anode pulse rise time at V_b = 2000 V ¹) | 7.10-9 | s |
| Anode pulse width at half height at V_b = 2000 V | 18.10-9 | s |
| Transit time difference between the centre of | 4-01-4 | |
| the photocathode and the edge at V_b = 2000 V | 15.10-9 | S |
| Total transit time at $V_{\rm b}$ = 2000 V | 70.10-9 | s |

LIMITING VALUES

| Supply voltage | V _b | max. | 2000 | V |
|---|----------------------|--------------|------------|--------|
| Continuous anode current | Ia | max. | 1 | mA |
| Voltage between cathode and first dynode | v_{k/S_1} | max. min. | 500 120 | V V |
| Voltage between consecutive dynodes | V _{Sn/Sn+1} | max. min. | 300 80 | V V |
| Voltage between anode and final dynode 2) | V _{a/S11} | max. min. | 300 80 | V V |

RECOMMENDED CIRCUITS



Voltage divider type A

k = cathode
acc = accelerating electrode

S_n = dynode No.n a = anode

1) For an infinitely short light pulse

 When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5664

54UVP

RECOMMENDED CIRCUITS (continued)



Voltage divider type B

| k | = | cathode | Sn | = | dynode No.n |
|-----|---|------------------------|----|---|-------------|
| acc | ± | accelerating electrode | а | = | anode |

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of about 1 mA will be sufficient.

With the voltage divider type A the tube gives the highest gain, while with the voltage divider type B the tube can deliver a higher anode current output with better time characteristics.

The accelerating electrode has a separate external connection to allow adjustment for optimum photoelectron collection on the first dynode.

In pulse techniques, such as scintillation counting, it is advisable to decouple the last two or three stages by means of capacitors of 100 pF and 200 pF (the highest value at the last stage).

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.

54 UVP



A





14 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in nuclear physics where a high degree of time definition or a high time resolution is required (fast coincidences, life of unstable particles, Cerenkov counters).

| QUICK REFERENCE DATA | | | | | |
|-------------------------------------|-----------------|-------|--|--|--|
| Spectral response | type A | (S11) | | | |
| Useful diameter of the photocathode | 42 | mm | | | |
| Gain (at 2200 V) | 10 ⁸ | | | | |
| Anode pulse rise time | 2 | ns | | | |
| Linearity | up to 300 | mA | | | |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 20-pin (Jedec B20-102)



ACCESSORIES

| Socket | type | FE1003 |
|---------------------------------|--------------|----------------|
| Mu-metal shields ¹) | type type | 56130 56131 |

GENERAL

| Photocathode | | | | |
|--|---------------------|-------------|-----------------|----------------|
| Description | semi-transparent, h | nead-on, c | urved | surface |
| Cathode material | | (| Cs-Sb | |
| Minimum useful diameter | | | 42 | mm |
| Radius of curvature | | max. | 69 | mm |
| Spectral response curve ²) | | type | A (S1) | L) |
| Wavelength at maximum response | | 4200 | <u>+</u> 300 | 8 |
| Luminous sensitivity ³) | Nk | av. min. | 65 45 | μA/lm μA/lm |
| Radiant sensitivity at 4200 Å | | | 55 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 14 | |
| Dynode material | | Ag-N | lg - 0-0 | Cs |
| Capacitances | | | | |
| Grid No.1 to accelerator electrode | Cg1/acc, S1 | | 25 | pF |
| Grid No.2 to all other electrodes | C_{g_2} | | 7 | pF |
| Anode to final dynode | $C_{a/S_{14}}$ | | 7 | pF |
| Anode to all other electrodes | Ca | | 9.5 | pF |

To avoid electric field distortion in the electron optical system the aquadag shield (pin No.18) must be connected to a voltage near to the cathode voltage. If the cathode is connected to the negative H.T., precautions should be taken to ensure a high-tension insulation between the aquadag shield and the mumetal shield.

- 2) See spectral response curve in front of this section
- $^{3})$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{0}\mathrm{K}$ 7Z2 5783

TYPICAL CHARACTERISTICS

| With voltage divider A | | | | |
|---|-------------------|--------------------|--------------|----------|
| Supply voltage for $G = 10^8$ | v _b | av. max. | 2200 2500 | v v |
| Anode dark current at G = 10^8 ¹) | I _{ao} | av. max. | 0.5 5.0 | μΑ μΑ |
| Linearity between anode pulse amplitud and input light pulse | le | up to | 100 | mA |
| With voltage divider B | | | | |
| Linearity between anode pulse amplitud and input light pulse | le | up to | 300 | mA |
| Anode pulse rise time at V _b = 2500 V 2 | | 2.10 ⁻⁹ | s | |
| Anode pulse width at half height at V_b = | | 4.10-9 | s | |
| Transit time difference between the centre the photocathode and the edge at V_b = | ntre of 2500 V | max.5 | .10-10 | s |
| Total transit time at V_b = 2500 V ²) | 3 | 36.10-9 | | |
| Maximum peak currents | | C | .5 to 1 | А |
| LIMITING VALUES (Absolute max. ra | ting system) | | | |
| Supply voltage ³) | Vb | max. | 2500 | v |

| Suppry Voltage -) | v b | max. | 2000 | v |
|---|--------------------|--------------|------------|--------|
| Continuous anode current | Ia | max. | .2 | mA |
| Voltage between cathode and first dynode | v_{k/S_1} | max. min. | 800 250 | v v |
| Voltage between grid No.1 and cathode | V _{k/g1} | max. | 100 | v |
| Voltage between grid No.2 and first dynode | v_{g_2/S_1} | max. | 100 | V |
| Voltage between consecutive dynodes | $v_{S_n/S_{n+1}}$ | max. min. | 500 80 | V V |
| Voltage between anode and final dynode ⁴) | V _{a/S14} | max. | 500 80 | V V |

- ¹) At an ambient temperature of 25 $^{\circ}C$.
- ²) For an infinitely short light pulse, fully illuminating the photocathode.
- 3) Or the voltage at which the tube circuited in the voltage divider A has a gain of about 10⁹, whichever is lowest.
- 4) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5784

RECOMMENDED CIRCUITS



Voltage divider type A 1)



Voltage divider type B 1)

- k = cathode
- g_1 = focusing electrode
- acc = accelerating electrode
- $g_2 = deflector$
- $S_n = dynode No.n$
- a = anode

voltage between k and g_1 to be adjusted at about 0.15 V_S (see fig.2); voltage between S_2 and S_3 to be adjusted at about 1.2 V_S ; decoupling capacitances $C_1 = 100 \text{ q/V}_S$, $C_2 = 100 \text{ q/3}V_S$, $C_3 = 100 \text{ q/9}V_S$, $C_4 = 100 \text{ q/27}V_S$ etc. with q = quantity of electricity transported by the anode.

¹) To avoid electric field distortion in the electron optical system the aquadag shield (pin No.18) must be connected to a voltage near to the cathode voltage. If the cathode is connected to the negative H.T., precautions should be taken to ensure a high-tension insulation between the aquadag shield and the mumetal shield. 7Z2 5785

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of about 3 mA will be sufficient.

The last stages must be decoupled by means of capacitances to avoid a serious voltage drop on the dynodes. A practical value for C_1 could be 2.10^{-9} F. In the case of high counting rates and large peak power output, and to avoid a high-tension supply of large power, it is possible to supply the first stages with a high tension of small output and the end stages with an average voltage of high output.

A. The electron optical input system consists of four elements:

the photocathode k; the focusing electrode g_1 ; the accelerating electrode acc; the deflector g_2 .

To reduce transit-time fluctuations, geometrical time spread, pulse amplitude spread or dark current, this system has the following advantages:

- 1. the photocathode is curved, though the outer window surface is flat, thus facilitating optical coupling to a scintillator.
- 2. a high and homogeneous extraction field at the cathode reduces as much as possible the influence of the initial electron velocities. A cathode-to-accelerator (internally connected to the first dynode) voltage of 350 V ensures a field strength of about 40 V/cm. This field is homogenized at the cathode surface by the focusing electrode g_1 . Fig.1 shows the electron path in the input system.
- 3. The potential of electrode g_1 to the photocathode can be adjusted in order to obtain one of the following characteristics:
 - a. the most satisfactory collection (i.e. for a given luminous flux the largest obtainable anode signal); for this adjustment, see Fig.2 the optimum value of the potential is about 0.15 V_{s} ;
 - b. the slightest transit-time fluctuations (the most homogeneous extraction field);
 - c. the most satisfactory uniformity of collection giving the most constant output pulse amplitude;
 - d. the useful cathode area can be controlled by giving the electrode g₁ a negative potential with respect to the photocathode, as shown in Fig.3, 4 and 5; obviously this variable electronic iris has the effect of reducing the dark current since the electrons emitted at the edge of the cathode do not reach the first dynode and consequently do not contribute to the anode current.







Fig.2 Anode current variation with the adjustment of g_1

OPERATIONAL CONSIDERATIONS (continued)











Fig.5

- 4. Because the first dynode cannot be placed parallel to the photocathode, the beam of primary electrons is deflected by the electrode g_2 to make it impinge at right angles to the first dynode surface. Collection on the first dynode is controlled by the potential of the third dynode (see recommended circuits).
- B. The multiplier system consists of 14 stages, providing a total current amplification of 10^8 at about 2200 V (see Fig.6).

The tube is capable of producing very strong peak currents (up to 1 A). Actually, the time constant at the output of the multiplier must be very small. Therefore it is necessary, taking into account the parasitic capacitances, to use a low-load resistance. It is advisable to use a resistance-matched coaxial cable (e.g. 75 or 100 Ω). With this load the tube easily delivers pulses of tens of volts, so that an amplifier is rendered superfluous.

It should be noted that in a number of applications it is not necessary for the current to be proportional to the incident luminous flux. As a matter of fact such short pulses are needed for time measurements only, so not for spectro-graphy purposes. If at the same time it is required, however, to determine the energy of the incident radiation, it is possible to select from one of the dynodes a signal proportional to the incident flux. In fact, when ascending the dynodes progressively, starting from the anode, the current is divided at each stage by d-1, d representing the secondary-emission coefficient of each stage (d ≈ 3.5). It is therefore possible to locate a dynode, the current of which is lower than, or equal to, the saturation limit of the dynodes.

Fig.7 illustrates the variation of the anode current as a function of the incident flux, the voltage divider being of type B. The anode current is then linear up to 300 mA.

Care should be taken that the anode voltage is adjusted to its optimum value. In fig.8 the anode current variation is plotted against anode-to-final-dynode voltage.

It should be noted that for equal high tension the gain of the tube is smaller for voltage divider type B than for one according to type A. In practice, therefore, it will be preferable to use the type A distribution, or a distribution between A and B (e.g. starting with 1.2 V_S between S₈ and S₉ 1.5 V_S between S₉ and S₁₀ and so on, maintaining the same progression.

It is advisable to screen the tube with a mu-metal cylinder against magneticfield influences.



Fig.6

A



Fig.7

R



Fig.8

С

14 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in spectrometry where very low luminous fluxes are to be measured (single photon counting) and for detecting of soft β -radiation (C₁₄ and H₃ counting). Its fast time characteristics make the tube especially useful for fast coincidence measurements, thus reducing the background noise considerably.

| QUICK REFERENCE DATA | | | | | |
|--|-----------------|--|--|--|--|
| Spectral response | type A (S11) | | | | |
| Useful diameter of the photocathode | 42 mm | | | | |
| Gain (at 2150 V) | 10 ⁸ | | | | |
| Anode pulse rise time | 2 ns | | | | |
| Efficiency for single photons (1600 V) | min. 7 % | | | | |
| Background noise (1600 V) | 350 c/sec | | | | |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 20-pin (Jedec B20-102)



TENTATIVE DATA

ACCESSORIES

| Socket | | type | FE1003 |
|----------|------------------------|--------------|----------------|
| Mu-metal | shields ¹) | type type | 56130 56131 |

GENERAL

| Photocathode | | | | |
|--|------------------------|-------------------|--------------------------|--|
| Description | semi-transparent, head | l-on, curved | d surface | |
| Cathode material | | Cs-Sh |) | |
| Minimum useful diameter | | 42 | 2 mm | |
| Radius of curvature | | 69 | mm | |
| Spectral response curve ²) | | type A (S11) | | |
| Wavelength at maximum response | | 4200 ± 300 | A (| |
| Luminous sensitivity ³) | Nk | av. 65 min. 45 | $\mu A/lm$ $\mu A/lm$ | |
| Radiant sensitivity at 4200 $ m R$ | | 55 | mA/W | |
| Multiplier system | A Charles | | | |
| Number of stages | | 14 | | |
| Dynode material | | Ag-Mg-O-Cs | | |
| Capacitances | | | | |
| Grid No.1 to accelerator electrode | Cg1/acc,S1 | 25 | pF | |
| Grid No.2 to all other electrodes | C_{g_2} | 7 | pF | |
| Anode to final dynode | $C_{a/S_{14}}$ | 7 | pF | |
| Anode to all other electrodes | Ca | 9.5 | pF | |

To avoid electric field distortion in the electron optical system the aquadag shield (pin No.18) must be connected to a voltage near to the cathode voltage. If the cathode is connected to the negative H.T., precautions should be taken to ensure a high-tension insulation between the aquadag shield and the mumetal shield.

 2) See spectral response curve in front of this section

 3) Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{\rm 0}{\rm K}$ 7Z2 5801

| I IFICAL CHARACTERISTICS | | | | |
|---|-----------------|--------------------|--------------------|----------------|
| With voltage divider A | | | | |
| Supply voltage for $G = 10^8$ | v _b | av. max. | 2150 2500 | v v |
| Anode dark current at $G = 10^8 1$) | I _{ao} | av. max. | 0.1 | μΑ μΑ |
| Linearity between anode pulse amplitude and input light pulse | | up to | 100 | mA |
| With voltage divider B | | | | |
| Linearity between anode pulse amplitude and input light pulse | | up to | 300 | mA |
| Anode pulse rise time at V_b = 2500 V 2) | | | 2.10-9 | S |
| Anode pulse width at half height at V_b = 2500 V ²) | | | 4.10-9 | S |
| Transit time difference between the centre of the photocathode and the edge at V_b = 2500 V | | max.5 | .10 ⁻¹⁰ | S |
| Total transit time at V_b = 2500 V 36. | | 6.10 ⁻⁹ | S | |
| Maximum peak currents | | C | .5 to 1 | А |
| With voltage divider C^{3}) | | | | |
| Efficiency for single-photons | η | min. | 7 | % |
| Supply voltage for $\eta = 7 \%$ | v _b | av. max. | 1600 1800 | V V |
| Background noise for η = 7 % | В | av. max. | 350 800 | c/sec c/sec |
| Background noise at V _b = 2100 V | В | av. max. | 2000 5000 | c/sec c/sec |

 $^{\rm 1})$ At an ambient temperature of 25 $^{\rm O}{\rm C}$

TYDICAL CHADACTEDISTIC

 2) For an infinitely short light pulse, fully illuminating the photocathode

 3) Measured with a threshold at the anode of the photo multiplier of $4.25 \mathrm{x} 10^{-13} \, \mathrm{C}$. $^{722} \, 8259$

| LIMITING VALUES (Absolute max. rating sy | stem) | | | |
|---|-----------------------------------|--------------|------------|--------|
| Supply voltage ¹) | V _b | max. | 2500 | V |
| Continuous anode current | Ia | max. | 0.2 | mA |
| Voltage between cathode and first dynode | v_{k/S_1} | max. min. | 800 250 | V V |
| Voltage between grid No.1 and cathode | V _{k/g1} | max. | 100 | V |
| Voltage between grid No.2 and first dynode | v_{g_2/S_1} | max. | 100 | V |
| Voltage between consecutive dynodes | V _{Sn} /S _{n+1} | max. min. | 500 80 | V V |
| Voltage between anode and final dynode ²) | $v_{a/S_{14}}$ | max. min. | 500 80 | V V |

RECOMMENDED CIRCUITS



Voltage divider type A 3)

k = cathode

- g_1 = focusing electrode
- acc = accelerating electrode
- $g_2 = deflector$

 $S_n = dynode No.n$

a = anode

voltage between k and g_1 to be adjusted at about 0.15 V_S (see fig.2); voltage between S_2 and S_3 to be adjusted at about 1.2 V_S ; decoupling capacitances $C_1 = 100 \text{ q/V}_S$, $C_2 = 100 \text{ q/3}V_S$, $C_3 = 100 \text{ q/9}V_S$,

 $C_4 = 100 \text{ q}/27\text{V}_{\text{S}}$ etc. with q = quantity of electricity transported by the anode.

- ¹) Or the voltage at which the tube circuited in the voltage divider A has a gain of about 5.10⁸ whichever is lowest.
- ²) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5803

4

RECOMMENDED CIRCUITS (continued)



Voltage divider type B^{3})



Voltage divider type C^{3})

- k = cathode
- g_1 = focusing electrode
- acc = accelerating electrode

 $g_2 = deflector$

 $S_n = dynode No.n$

a = anode

voltage between k and g_1 to be adjusted at about 0.15 V_S (see fig.2); voltage between S_2 and S_3 to be adjusted at about 1.2 V_S ; decoupling capacitances $C_1 = 100 \text{ q/V}_S$, $C_2 = 100 \text{ q/3}V_S$, $C_3 = 100 \text{ q/9}V_S$, $C_4 = 100 \text{ q/27}V_S$ etc. with q = quantity of electricity transported by the anode.

³) To avoid electric field distortion in the electron optical system the aquadag shield (pin No.18) must be connected to a voltage near to the cathode voltage. If the cathode is connected to the negative H.T., precautions should be taken to ensure a high-tension insulation between the aquadag shield and the mumetal shield. 7Z2 5804

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

The last stages must be decoupled by means of capacitances to avoid a serious voltage drop on the dynodes. A practical value for C_1 could be 2.10^{-9} F. In the case of large peak power output, and to avoid a high-tension supply of large power, it is possible to supply the first stages with a high tension of small output and the end stages with an average voltage of high output.

A. The electron optical input system consists of four elements:

the photocathode k; the focusing electrode g_1 ; the accelerating electrode acc; the deflector g_2 .

To reduce transit-time fluctuations, geometrical time spread, amplitude fluctuation or dark current, this system has the following advantages:

- 1. the photocathode is curved, though the outer window surface is flat, thus facilitating optical coupling.
- 2. a high and homogeneous extraction field at the cathode reduces as much as possible the influence of the initial electron velocities. A cathode-to-accelerator (internally connected to the first dynode) voltage of 350 V ensures a field strength of about 40 V/cm. This field is homogenized at the cathode surface by the focusing electrode g_1 . Fig.1 shows the electron path in the input system.
- 3. the potential of electrode g_1 to the photocathode can be adjusted in order to obtain one of the following characteristics:
 - a. the most satisfactory collection (i.e. for a given luminous flux the largest obtainable anode signal); for this adjustment, see Fig.2; the optimum value of the potential is about 0.15 V_s ;
 - b. the slightest transit-time fluctuations (the most homogeneous extraction field);
 - c. the most satisfactory uniformity of collection giving the most constant output amplitude.
 - d. the useful cathode area can be controlled by giving the electrode g_1 a negative potential with respect to the photocathode, obviously this variable electronic iris has the effect of reducing the dark current since the electrons emitted at the edge of the cathode do not reach the first dynode and consequently do not contribute to the anode current.







Fig.2 Anode dark current variation with the adjustment of $\ensuremath{\mathtt{g}}_1$

- 4. Because the first dynode cannot be placed parallel to the photocathode, the beam of primary electrons is deflected by the electrode g_2 to make it impinge at right angles to the first dynode surface. Collection on the first dynode is controlled by the potential of the third dynode (see recommended circuits).
- B. The multiplier system consists of 14 stages, providing a total current amplification of 10⁸ at about 2150 V (see fig.5).

The tube is capable of producing very strong peak currents (up to 1 A). Actually, the time constant at the output of the multiplier must be very small. Therefore it is necessary, taking into account the parasitic capcitances, too use a low-load resistance. It is advisable to use a resistance-matched coaxial cable (e.g. 75 or 100 Ω). With this load the tube easily delivers pulses of tens of volts, so that an amplifier is rendered superfluous.

Fig.3 illustrates the variation of the anode current as a function of the incident flux, the voltage divider being of type B. The anode current is then linear up to 300 mA.

Care should be taken that the anode voltage is adjusted to its optimum value. In Fig.4 the anode current variation is plotted against anode-to-final-dynode voltage.

It should be noted that at equal high tensions the gain of the tube is smaller for voltage divider type B than for one according to type A.

It is advisable to screen the tube with a mu-metal cylinder against magneticfield influences.

- C. The specification of the tube characteristics for the detection of very low luminous fluxes is based on the following method of measuring:
 - 1. The photocathode of the tube is impinged by a monochromatic light flux $(\lambda = 4240 \text{ Å})$ of 1,46.10⁵ photons/sec. This flux is small enough to ensure that the interactions of the photons with the photocathode result in single photoelectron pulses.
 - 2. The tube is circuited in the voltage divider C. The threshold of the electronic system related to the anode of the photomultiplier is 4.25×10^{-13} Coulomb.
 - 3. The efficiency for single photons at a certain voltage is defined as follows:

$$\eta = \frac{n - B}{N} \ge 100 \%.$$

In which: n = number of counted pulses per unit of time

B = number of noise pulses per unit of time

N = luminous flux in photons per unit of time

Fig.6 shows the efficiency and noise curves as a function of the high tension, measured as described before.

The results obtained with a special liquid scintillation-tritium source are given in fig.7. It should be noticed that a detection efficiency for tritium of about 40% at room temperature is possible. A considerable reduction of the background noise can be obtained by means of coincidence measurements. For this purpose particularly well matched pairs of photo multipliers are available. The high voltages for these two tubes are equal within \pm 15 V at a detection efficiency of 7% for single photons and the product of the values of the background noise of both tubes is less than 25.10⁴ at the same voltage. (Type no. 56AVP/03A).







Fig.4



Fig.5



Fig.6

D





E

14 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in nuclear physics where a high degree of time definition or a high time resolution is required, combined with a good sensitivity in the near-ultraviolet region.

| QUICK REFERENCE DATA | | | |
|-------------------------------------|--------------------------|--|--|
| Spectral response | type A/05 (extended S11) | | |
| Useful diameter of the photocathode | 42 mm | | |
| Window thickness | 0.5 mm | | |
| Gain (at 2200 V) | 108 | | |
| Anode rise time | 2 ns | | |
| Linearity | up to 300 mA | | |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 20-pin (Jedec B20-102)



ACCESSORIES

| Socket | type | FE1003 |
|---------------------------------|------|--------|
| Mu-metal shields ¹) | type | 56130 |
| | type | 56131 |

GENERAL

| Photocathode | | | | |
|-------------------------------------|-----------------------|------------|----------------|----------------|
| Description | semi-transparent, hea | d-on, | curved | surface |
| Cathode material | | | Cs-Sb | |
| Minimum useful diameter | | | 42 | mm |
| Radius of curvature | | max | 69 | mm |
| Spectral response curve 2) | type | A/05 | (exten | ded S11) |
| Wavelength at maximum response | | 440 | 0 <u>+</u> 300 | A |
| Luminous sensitivity ³) | Nk | av. min | . 65 . 45 | μA/lm μA/lm |
| Radiant sensitivity at 4400 Å | | | 55 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 14 | |
| Dynode material | Ag-Mg-O-Cs | | | Cs |
| Capacitances | | | | |
| Grid No.1 to accelerator electrode | Cg1/acc,S1 | | 25 | pF |
| Grid No.2 to all other electrodes | Cg2 | | 7 | pF |
| Anode to final dynode | $C_{a/S_{14}}$ | | 7 | pF |
| Anode to all other electrodes | Ca | | 9.5 | pF |

To avoid electric field distortion in the electron optical system the aquadag shield (pin No.18) must be connected to a voltage near to the cathode voltage. If the cathode is connected to the negative H.T., precautions should be taken to ensure a high-tension insulation between the aquadag shield and the mumetal shield.

²) See spectral response curve page D.

 $^{3}\)$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{0}\mbox{K}$ $7\mbox{Z2}$ 8262

TYPICAL CHARACTERISTICS

| With voltage divider A | | | | |
|---|--|--------------|--------------|----------|
| Supply voltage for $G = 10^8$ | Vb | av. max. | 2200 2500 | v v |
| Anode dark current at G = 10^8 ¹) | Iao | av. max. | 0.5 5.0 | μΑ μΑ |
| Linearity between anode pulse amplitude and input light pulse | | up to | 100 | mA |
| With voltage divider B | | | | |
| Linearity between anode pulse amplitude and input light pulse | | up to | 300 | mA |
| Anode pulse rise time at V_b = 2500 V ²) | | | 2.10-9 | s |
| Anode pulse width at half height at V_b = 2500 V ²) | | | 4.10-9 | s |
| Transit time difference between the centre of the photocathode and the edge at V_b = 2500 V | | max.5 | .10-10 | s |
| Total transit time at V_b = 2500 V ²) | | 3 | 6.10-9 | s |
| Maximum peak currents | | (|).5 to 1 | А |
| LIMITING VALUES (Absolute max. rating s | ystem) | | | |
| Supply voltage ³) | Vb | max. | 2500 | V |
| Continuous anode current | Ia | max. | 2 | mA |
| Voltage between cathode and first dynode | v_{k/S_1} | max. min. | 800 250 | v v |
| Voltage between grid No.1 and cathode | V_{k/g_1} | max. | 100 | V |
| Voltage between grid No.2 and first dynode | V_{g_2/S_1} | max. | 100 | v |
| Voltage between consecutive dynodes | V _{S_n/S_{n+1}} | max. min. | 500 80 | v v |
| Voltage between anode and final dynode ⁴) | Va/S ₁₄ | max. min. | 500 80 | V V |

1) At an ambient temperature of 25 °C.

2) For an infinitely short light pulse, fully illuminating the photocathode.

3) Or the voltage at which the tube circuited in the voltage divider A has a gain of about 10⁹, whichever is lowest.

4) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5837

RECOMMENDED CIRCUITS



Voltage divider type A^{1})



Voltage divider type B^{1})

- k = cathode
- g_1 = focusing electrode
- acc = accelerating electrode
- $g_2 = deflector$
- $S_n = dynode No.n$
- a = anode

voltage between k and g_1 to be adjusted at about 0.15 V_S (see fig.2); voltage between S_2 and S_3 to be adjusted at about 1.2 V_S ; decoupling capacitances $C_1 = 100 \text{ q/V}_S$; $C_2 = 100 \text{ q/3}V_S$, $C_3 = 100 \text{ q/9}V_S$,

 C_4 = 100 $q/27 V_{\rm S}$ etc. with q = quantity of electricity transported by the anode.

¹) To avoid electric field distortion in the electron optical system the aquadag shield (pin No.18) must be connected to a voltage near to the cathode voltage. If the cathode is connected to the negative H.T., precautions should be taken to ensure a high-tension insulation between the aquadag shield and the mumetal shield. 7Z2 5838

4
OPERATIONÁL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of about 3 mA will be sufficient.

The last stages must be decoupled by means of capacitances to avoid a serious voltage drop on the dynodes. A practical value for C_1 could be 2.10^{-9} F. In the case of high counting rates and large peak power output, and to avoid a high-tension supply of large power, it is possible to supply the first stages with a high tension of small output and the end stages with an average voltage of high output.

A. The electron optical input system consists of four elements:

the photocathode k; the focusing electrode g_1 ; the accelerating electrode acc; the deflector g_2 .

To reduce transit-time fluctuations, geometrical time spread, pulse amplitude spread or dark current, this system has the following advantages:

- 1. the photocathode is curved, though the outer window surface is flat, thus facilitating optical coupling to a scintillator;
- 2. a high and homogeneous extraction field at the cathode reduces as much as possible the influence of the initial electron velocities. A cathode-to-accelerator (internally connected to the first dynode) voltage of 350 V ensures a field strength of about 40 V/cm. This field is homogenized at the cathode surface by the focusing electrode g_1 . Fig.1 shows the electron path in the input system.
- 3. The potential of electrode g_1 to the photocathode can be adjusted in order to obtain one of the following characteristics:
 - a. the most satisfactory collection (i.e. for a given luminous flux the largest obtainable anode signal); for this adjustment, see Fig.2 the optimum value of the potential is about 0.15 V_s ;
 - b. the slightest transit-time fluctuations (the most homogeneous extraction field);
 - c. the most satisfactory uniformity of collection giving the most constant output pulse amplitude;
 - d. the useful cathode area can be controlled by giving the electrode g_1 a negative potential with respect to the photocathode, as shown in Fig.3, 4 and 5; obviously this variable electronic iris has the effect of reducing the dark current since the electrons emitted at the edge of the cathode do not reach the first dynode and consequently do not contribute to the anode current.







Fig.2 Anode current variation with the adjustment of g_1



Fig.3







Fig.5

- 4. Because the first dynode cannot be placed parallel to the photocathode, the beam of primary electrons is deflected by the electrode g_2 to make it impinge at right angles to the first dynode surface. Collection on the first dynode is controlled by the potential of the third dynode (see recommended circuits).
- B. The multiplier system consists of 14 stages, providing a total current amplification of 10^8 at about 2200 V (see Fig.6)

The tube is capable of producing very strong peak currents (up to 1 A). Actually, the time constant at the output of the multiplier must be very small. Therefore it is necessary, taking into account the parasitic capacitances, to use a low-load resistance. It is advisable to use a resistance-matched coaxial cable (e.g. 75 or 100 Ω). With this load the tube easily delivers pulses of tens of volts, so that an amplifier is rendered superfluous.

It should be noted that in a number of applications it is not necessary for the current to be proportional to the incident luminous flux. As a matter of fact such short pulses are needed for time measurements only, so not for spectrography purposes. If at the same time it is required, however, to determine the energy of the incident radiation, it is possible to select from one of the dynodes a signal proportional to the incident flux. In fact, when ascending the dynodes progressively, starting from the anode, the current is divided at each stage by d-1, d representing the secondary-emission-coefficient of each stage (d \approx 3.5). It is therefore possible to locate a dynode, the current of which is lower than, or equal to, the saturation limit of the dynodes.

Fig.7 illustrates the variation of the anode current as a function of the incident flux, the voltage divider being of type B. The anode current is then linear up to 300 mA.

Care should be taken that the anode voltage is adjusted to its optimum value. In fig.8 the anode current variation is plotted against anode-to-final-dynode voltage.

It should be noted that for equal high tension the gain of the tube is smaller for voltage divider type B than for one according to type A. In practice, therefore, it will be preferable to use the type A distribution, or a distribution between A and B (e.g. starting with 1.2 V_S between S₈ and S₉ 1.5 V_S between S₉ and S₁₀ and so on, maintaining the same progression.

It is advisable to screen the tube with a mu-metal cylinder against magnetic-field inlfuences.



Fig.6

A



Fig.7





С



Spectral response curve A/05 Fig.9





10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in such applications as infra-red telecommunication and ranging, and in optical experiments in which a fast response is required.

| QUICK REFERENCE DAT | A | |
|-------------------------------------|------|--------|
| Spectral response | type | C (S1) |
| Useful diameter of the photocathode | 42 | mm |
| Anode sensitivity (at 2750 V) | 100 | A/lm |
| Anode pulse rise time | 2 | ns |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 20-pin (Jedec B20-102)





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56CVP

ACCESSORIES

| Socket | type | FE1003 |
|---------------------|------|--------|
| My motal abialda) | type | 56130 |
| Mu-metal smelds -) | type | 56131 |

GENERAL

| Photocathode | | | | |
|---|----------------------|---------------|----------|----------------|
| Description | semi-transparent, he | ad-on, c | urved | surface |
| Cathode material | | Ag- | 0-Cs | |
| Minimum useful diameter | | | 42 | mm |
| Radius of curvature | | max. | 69 | mm |
| Spectral response curve ²) | | type C | C (S1) | |
| Wavelength at maximum response | | 8000 <u>+</u> | 1000 | A |
| Luminous sensitivity ³) | Nk | av. min. | 25 15 | μA/lm μA/lm |
| Infra-red luminous sensitivity ⁴) | Nk | av. min. | 3 1.4 | μA/lm μA/lm |
| Radiant sensitivity at 8000 Å | | | 2 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 10 | |
| Dynode material | | Ag-Mg | -0-Cs | 5 |
| Capacitances | | | | |
| Grid No.1 to accelerator electrode | Cg1/acc, S1 | | 25 | pF |
| Grid No.2 to all other electrodes | C _{g2} | | 7 | pF |

| | 82 | | |
|-------------------------------|----------------|-----|----|
| Anode to final dynode | $C_{a/S_{10}}$ | 7 | pF |
| Anode to all other electrodes | C _a | 9.5 | pF |

1) To avoid electric field distortion in the electron optical system the aquadag shield (pin No.18) must be connected to a voltage near to the cathode voltage. If the cathode is connected to the negative H.T., precautions should be taken to ensure a high-tension insulation between the aquadag shield and the mumetal shield.

2) See spectral response curve in front of this section.

- ³) Measured with a tungsten ribbon lamp having a colour temperature of 2850 ^oK
- 4) The infra-red lumen is the flux resulting from one lumen yielded by a tungsten ribbon lamp (colour temperature 2850 °K) going through an infra-red filter corning CS94 No.2450, fusion 1613 thickness 2.61.

56 CVP

| With voltage divider 11 | | | | |
|---|---|--------------|--------------------|--------------|
| Anode sensitivity at V _b = 2750 V | | av. min. | 100 20 | A/lm A/lm |
| Anode dark current at $N_a = 20 \text{ A/lm}^{1}$) | ning and an and a second s I second | max. | 10 | μA |
| With voltage divider B | | | | |
| Anode pulse rise time at V_b = 3000 V ²) | | 1 | 2.10 ⁻⁹ | S |
| Anode pulse width at half height at V_b = 3000 |) V ²) | | 4.10-9 | s |
| Transit time difference between the centre of the photocathode and the edge at V_b = 3000 | of V | max.0, | 7.10 ⁻⁹ | S |
| LIMITING VALUES (Absolute max. rating a | system) | | | |
| Supply voltage | v _b | max. | 3000 | v |
| Continuous anode current | Ia | max. | 30 | μA |
| Voltage between cathode and first dynode | v_{k/s_1} | max. min. | 800 250 | v v |
| Voltage between grid No.1 and cathode | V_{k/g_1} | max. | 100 | V |
| Voltage between grid No.2 and first dynode | v_{g_2/S_1} | max. | 100 | V |
| Voltage between consecutive dynodes | V _{S_n/S_{n+1}} | max. min. | 500 80 | V V |
| Voltage between anode and final dynode ³) | V _{a/S10} | max. min. | 500 80 | v v |

 $^{\rm l})$ At an ambient temperature of 25 $^{\rm o}C_{\star}$

TYPICAL CHARACTERISTICS

With voltage divider A

2) For an infinitely short light pulse fully illuminating the photocathode.

³⁾ When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5829

RECOMMENDED CIRCUITS



Voltage divider type A^{1})



Voltage divider type B^{-1})

- k = cathode
- $g_1 = focusing electrode$
- acc = accelerating electrode
- $g_2 = deflector$
- $S_n = dynode No.n$
- a = anode

voltage between k and g_1 to be adjusted at about 0.15 V_S (see fig.2); voltage between S_2 and S_3 to be adjusted at about 1.2 V_S ; decoupling capacitances $C_1 = 100 \text{ q/V}_S$, $C_2 = 100 \text{ q/3}V_S$, $C_3 = 100 \text{ q/9}V_S$, $C_4 = 100 \text{ q/27}V_S$ etc. with q = quantity of

electricity transported by the anode.

 To avoid electric field distortion in the electron optical system the aquadag shield (pin No.18) must be connected to a voltage near to the cathode voltage. If the cathode is connected to the negative H.T., precautions should be taken to ensure a high-tension insulation between the aquadag shield and the mumetal shield.

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of about 3 mA will be sufficient.

The last stages must be decoupled by means of capacitances to avoid a serious voltage drop on the dynodes. A practical value for C_1 could be 2.10^{-9} F. In the case of high counting rates and large peak power output, and to avoid a high-tension supply of large power, it is possible to supply the first stages with a high tension of small output and the end stages with an average voltage of high output.

A. The electron optical input system consists of four elements:

the photocathode k; the focusing electrode g_1 ; the accelerating electrode acc; the deflector g_2 .

To reduce transit-time fluctuations, geometrical time spread, pulse amplitude spread or dark current, this system has the following advantages:

- 1. the photocathode is curved, though the outer window surface is flat, thus facilitating optical coupling to a scintillator;
- 2. a high and homogeneous extraction field at the cathode reduces as much as possible the influence of the initial electron velocities. A cathode-to-accelerator (internally connected to the first dynode) voltage of 350 V ensures a field strength of about 40 V/cm. This field is homogenized at the cathode surface by the focusing electrode g_1 . Fig.1 shows the electron path in the input system.
- 3. The potential of electrode g₁ to the photocathode can be adjusted in order to obtain one of the following characteristics:
 - a. the most satisfactory collection (i.e. for a given luminous flux the largest obtainable anode signal); for this adjustment, see Fig.2 the optimum value of the potential is about 0.15 V_{s} ;
 - b. the slightest transit-time fluctuations (the most homogeneous extraction field);
 - c. the most satisfactory uniformity of collection giving the most constant output pulse amplitude;
 - d. the useful cathode area can be controlled by giving the electrode g_1 a negative potential with respect to the photocathode, as shown in Fig.3, 4 and 5; obviously this variable electronic iris has the effect of reducing the dark current since the electrons emitted at the edge of the cathode do not reach the first dynode and consequently do not contribute to the anode current.







Fig.2 Anode current variation with the adjustment of $g_{\rm 1}$

56CVP

OPERATIONAL CONSIDERATIONS (continued)











Fig.5

- 4. Because the first dynode cannot be placed parallel to the photocathode, the beam of primary electrons is deflected by the electrode g_2 to make it impinge at right angles to the first dynode surface. Collection on the first dynode is controlled by the potential of the third dynode (see recommended circuits).
- B. The multiplier system consists of 10 stages, providing a total current amplification of 10^7 at about 3000 V

When high frequency signals are to be detected the time constant at the output of the multiplier must be very small. Therefore it is necessary, taking into account the parasitic capacitances, to use a low-load resistance. It is advisable to use a resistance-matched coaxial cable (e.g. 75 or 100Ω).

It is advisable to screen the tube with a mu-metal cylinder against magnetic-field influences.

56CVP



Fig.6



14 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in applications such as telecommunication and ranging and in optical experiments where a high-sensitivity in the whole visible and ultraviolet region is required combined with a high degree of time definition.

| QUICK REFERENCI | E DATA | |
|-------------------------------------|---------------------|-----|
| Spectral response | type TU (extended S | 20) |
| Window material | quartz | |
| Useful diameter of the photocathode | 42 r | nm |
| Gain (at 2500 V) | 10 ⁸ | |
| Anode pulse rise time | 2 n | IS |
| Linearity | up to 300 r | nA |

DIMENSIONS AND CONNECTIONS

Dimensions in mm



ACCESSORIES

| Socket | type | FE1003 |
|---------------------|------|--------|
| Mu-motal shields 1) | ţype | 56130 |
| Mu-metal smelds -) | type | 56131 |

GENERAL

| Photocathode | | | | | |
|--|------|----------------|---------------|-------------|----------------|
| Description | semi | -transpar | ent, head-on, | curved | surface |
| Cathode material | | | Sb-F | C-Na-C | S |
| Minimum useful diameter | | | | 42 | mm |
| Radius of curvature | | | max | . 69 | mm |
| Spectral response curve ²) | | | type TU | (exten | ded S20) |
| Wavelength at maximum respons | е | | 4200 | 1 ± 300 | . A |
| Luminous sensitivity ³) | | N _k | av. min | 115 . 90 | μA/lm μA/lm |
| Radiant sensitivity at 4200 🞗 | | | | 65 | mA/W |
| at 7000 Å | | | | 12 | mA/W |
| Multiplier system | | | | | |

14

Ag-Mg-O-Cs

Multiplier system

Number of stages

Dynode material

Capacitances

| Grid No.1 to accelerator electrode | Cg1/acc,S1 | 25 | pF |
|--|---|-----|----|
| Grid No.2 to all other electrodes | C_{g_2} | 7 | pF |
| Anode to final dynode | C _{a/S₁₄} | 7 | pF |
| Anode to all other electrodes | Ca | 9.5 | pF |
| Anode to final dynode Anode to all other electrodes | C _a /S ₁₄ C _a | 9.5 | |

¹) To avoid electric field distortion in the electron optical system the aquadag shield (pin No.18) must be connected to a voltage near to the cathode voltage. If the cathode is connected to the negative H.T., precautions should be taken to ensure a high-tension insulation between the aquadag shield and the mumetal shield.

²) See spectral response curve in front of this section.

³) Measured with a tungsten ribbon lamp having a colour temperature of 2850 ^oK 7Z2 5819

| With voltage divider A | | | | |
|---|--|--------------|------------------|--------|
| Supply voltage for $G = 10^8$ | v _b | av. max. | 2500 2750 | V V |
| Anode dark current at G = 10^8 ¹) | I _{ao} | max. | 5 | μA |
| Linearity between anode pulse amplitude and input light pulse | | up to | 100 | mA |
| With voltage divider B | | | | |
| Linearity between anode pulse amplitude and input light pulse | | up to | 300 | mA |
| Anode pulse rise time at V_b = 2500 V $^2)$ | | 2. | 10 ⁻⁹ | S |
| Anode pulse width at half height at V_b = 2500 V ²) | | · 4. | 10-9 | s |
| Transit time difference between the centre of the photocathode and the edge at V_b = 2500 | of V | max. | 10-9 | S |
| Total transit time at V _b = 2500 V 2) | | 36.10-9 | | s |
| Maximum peak currents | an a | 0.5 | 5 to 1 | А |
| LIMITING VALUES (Absolute max. rating | system) | | | |
| Supply voltage ³) | Vb | max. | 2750 | V |
| Continuous anode current | Ia | max. | 2 | mA |
| Voltage between cathode and first dynode | v _{k/s1} | max. min. | 800 250 | V V |
| Voltage between grid No.1 and cathode | V _{k/g1} | max. | 100 | V |
| Voltage between consecutive dynodes | vs _n /s _{n+1} | max. min. | 500 80 | V V |
| Voltage between anode and final dynode ⁴) | Va/S14 | max. | 500 | V |

 $^{1})$ At an ambient temperature of 25 $^{\mathrm{o}}\mathrm{C}.$

TYPICAL CHARACTERIST

²) For an infinitely short light pulse, fully illuminating the photocathode.

- ³) Or the voltage at which the tube circuited in the voltage divider A has a gain of about 10^9 , whichever is lowest.
- When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 7854

RECOMMENDED CIRCUITS



Voltage divider type A^{1})



Voltage divider type B^{-1})

- k = cathode
- $g_1 = focusing electrode$
- acc = accelerating electrode
- $g_2 = deflector$
- $S_n = dynode No.n$
- a = anode

voltage between k and g_1 to be adjusted at about 0.15 V_s (see fig.2); voltage between S_2 and S_3 to be adjusted at about 1.2 V_s ; decoupling capacitances $C_1 = 100 \text{ q/V}_s$, $C_2 = 100 \text{ q/3}V_s$, $C_3 = 100 \text{ q/9}V_s$, $C_4 = 100 \text{ q/27}V_s$ etc. with q = quantity of

 $C_4 = 100 q/27V_s$ etc. with q = quantity of electricity transported by the anode.

¹) To avoid electric field distortion in the electron optical system the aquadag shield (pin No.18) must be connected to a voltage near to the cathode voltage. If the cathode is connected to the negative H.T., precautions should be taken to ensure a high-tension insulation between the aquadag shield and the mumetal shield. 7Z2 5821

4

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

The last stages must be decoupled by means of capacitances to avoid a serious voltage drop on the dynodes. A practical value for C_1 could be 2.10^{-9} F. In the case of high counting rates and large peak power output, and to avoid a high-tension supply of large power, it is possible to supply the first stages with a high tension of small output and the end stages with an average voltage of high output.

A. The electron optical input system consists of four elements:

the photocathode k; the focusing electrode g_1 ; the accelerating electrode acc; the deflector g_2 .

To reduce transit-time fluctuations, geometrical time spread, pulse amplitude spread or dark current, this system has the following advantages:

- 1. the photocathode is curved, though the outer window surface is flat, thus facilitating optical coupling to a scintillator.
- 2. a high and homogeneous extraction field at the cathode reduces as much as possible the influence of the initial electron velocities. A cathode-to-accelerator (internally connected to the first dynode) voltage of 350 V ensures a field strength of about 40 V/cm. This field is homogenized at the cathode surface by the focusing electrode g_1 . Fig.1 shows the electron path in the input system.
- 3. The potential of electrode g_1 to the photocathode can be adjusted in order to obtain one of the following characteristics:
 - a. the most satisfactory collection (i.e. for a given luminous flux the largest obtainable anode signal); for this adjustment, see Fig.2 the optimum value of the potential is about $0.15 V_s$;
 - b. the slightest transit-time fluctuations (the most homogeneous extraction field);
 - c. the most satisfactory uniformity of collection giving the most constant output pulse amplitude;
 - d. the useful cathode area can be controlled by giving the electrode g₁ a negative potential with respect to the photocathode, as shown in Fig.3, 4 and 5; obviously this variable electronic iris has the effect of reducing the dark current since the electrons emitted at the edge of the cathode do not reach the first dynode and consequently do not contribute to the anode current.



Fig.1 Electron optical input system



Fig.2 Anode current variation with the adjustment of g_1

OPERATIONAL CONSIDERATIONS (continued)



Fig.3





OPERATIONAL CONSIDERATIONS (continued)





- 4. Because the first dynode cannot be placed parallel to the photocathode, the beam of primary electrons is deflected by the electrode g_2 to make it impinge at right angles to the first dynode surface. Collection on the first dynode is controlled by the potential of the third dynode (see recommended circuits).
- B. The multiplier system consists of 14 stages, providing a total current amplification of 10⁸ at about 2500 V (see Fig.6).

The tube is capable of producing very strong peak currents (up to 1 A). Actually, the time constant at the output of the multiplier must be very small. Therefore it is necessary, taking into account the parasitic capacitances, to use a low-load resistance. It is advisable to use a resistance-matched coaxial cable (e.g. 75 or 100 Ω). With this load the tube easily delivers pulses of tens of volts, so that an amplifier is rendered superfluous.

Fig.7 illustrates the variation of the anode current as a function of the incident flux, the voltage divider being of type B. The anode current is then linear up to 300 mA.

Care should be taken that the anode voltage is adjusted to its optimum value. In fig.8 the anode current variation is plotted against anode-to-final-dynode voltage.

It should be noted that at equal high tensions the gain of the tube is smaller for voltage divider type B than for one according to type A. In practice, therefore, it will be preferable to use the type A distribution, or a distribution between A and B (e.g. starting with 1.2 V_S between S₈ and S₉, 1.5 V_S between S₉ and S₁₀ and so on, maintaining the same progression.

It is advisable to screen the tube with a mu-metal cylinder against magnetic-field influences.



Fig.6

A



Fig.7

В



Fig.8

С

14 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in laser-technics working in the orange, yellow and green range.

| QUICK REFERENCE DATA | | | |
|-------------------------------------|-----------------|--|--|
| Spectral response | type T (S20) | | |
| Useful diameter of the photocathode | 42 mm | | |
| Gain (at 2500 V) | 10 ⁸ | | |
| Anode pulse rise time | 2 ns | | |
| Linearity | up to 300 mA | | |

DIMENSIONS AND CONNECTIONS

Base: 20-pin (Jedec B20-102)

Dimensions in mm



7Z2 8257

1

ACCESSORIES

| Socket | type | FE1003 |
|---------------------|------|--------|
| My motel shields 1) | type | 56130 |
| Mu-metal smelds ~) | type | 56131 |

GENERAL

Photocathode

| Description | semi-transparent, head | -on, curve | d surface | |
|---|------------------------|--------------------|------------------------------|--|
| Cathode material | | Sb-K-Na- | Cs | |
| Minimum useful diameter | | 42 | 2 mm | |
| Radius of curvature | | max. 69 | 9 mm | |
| Spectral response curve 2) | | type T (S20) | | |
| Wavelength at maximum response | | 4200 ± 300 | A | |
| Luminous sensitivity ³) | Nk | av. 115 min. 90 | 5 μ A/lm 0 μ A/lm | |
| Radiant sensitivity at 4200 Å at 7000 Å | | 65 12 | 5 mA/W 2 mA/W | |
| Multiplier system | | | | |
| Number of stages | | 14 | Ł | |
| Dynode material | | Ag-Mg-O- | -Cs | |
| Capacitances | | | | |
| Grid No.1 to accelerator electrode | Cg1/acc,S1 | 25 | 5 pF | |
| Grid No.2 to all other electrodes | Cg2 | 5 | 7 pF | |
| Anode to final dynode | $C_{a/S_{14}}$ | 7 | 7 pF | |
| Anode to all other electrodes | Ca | 9.5 | 5 pF | |

¹) To avoid electric field distortion in the electron optical system the aquadag shield (pin No.18) must be connected to a voltage near to the cathode voltage. If the cathode is connected to the negative H.T., precautions should be taken to ensure a high-tension insulation between the aquadag shield and the mumetal shield.

 2) See spectral response curve in front of this section.

³) Measured with a tungsten ribbon lamp having a colour temperature of 2850 °K 7Z2 5810

| TYPICAL CHARACTERISTICS | | | | |
|---|---|-----------------------|------------|--------|
| With voltage divider A | | | 0.500 | |
| Supply voltage for G = 10^8 | Vb | av. max. | 2500 | V V |
| Anode dark current at G = 10^{8} ¹) | Iao | max. | 5.0 | μΑ |
| Linearity between anode pulse amplitude and input light pulse | | up to | 100 | mA |
| With voltage divider B | | | | |
| Linearity between anode pulse amplitude and input light pulse | | up to | 300 | mA |
| Anode pulse rise time at V_b = 2500 V ²) | | 2.10-9 | | s |
| Anode pulse width at half height at V_b = 2500 V ²) | | | 4.10-9 | |
| Transit time difference between the centre of the photocathode and the edge at V_b = 2500 V | | max. 10 ⁻⁹ | | s |
| Total transit time at V_b = 2500 V ²) | | 36.10-9 | | s |
| Maximum peak currents | | 0.5 to 1 | | А |
| LIMITING VALUES (Absolute max. rating sy | ystem) | | | |
| Supply voltage ³) | Vb | max. | 2750 | V |
| Continuous anode current | Ia | max. | 2 | mA |
| Voltage between cathode and first dynode | v_{k/S_1} | max. min. | 800 250 | v v |
| Voltage between grid No.1 and cathode | V _{k/g1} | max. | 100 | V |
| Voltage between consecutive dynodes | ^V S _n /S _{n+1} | max. min. | 500 80 | V V |
| Voltage between anode and final dynode ⁴) | V _{a/S14} | max. | 500 80 | V V |

- 1) At an ambient temperature of 25 $^{\circ}$ C.
- 2) For an infinitely short light pulse, fully illuminating the photocathode.
- $^{3})$ Or the voltage at which the tube circuited in the voltage divider A has a gain of about 10⁹, whichever is lowest.
- ⁴) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 7853

RECOMMENDED CIRCUITS (continued)



Voltage divider type A 1)



Voltage divider type B^{-1})

- k = cathode
- $g_1 = focusing electrode$
- acc = accelerating electrode
- $g_2 = deflector$
- $S_n = dynode No.n$
- a = anode

voltage between k and g_1 to be adjusted at about 0.15 V_S (see fig.2); voltage between S_2 and S_3 to be adjusted at about 1.2 V_S ; decoupling capacitances $C_1 = 100 \text{ q/V}_S$, $C_2 = 100 \text{ q/3}V_S$, $C_3 = 100 \text{ q/9}V_S$, $C_4 = 100 \text{ q/27}V_S$ etc. with q = quantity of electricity transported by the anode.

 To avoid electric field distortion in the electron optical system the aquadag shield (pin No.18) must be connected to a voltage near to the cathode voltage. If the cathode is connected to the negative H.T., precautions should be taken to ensure a high-tension insulation between the aquadag shield and the mumetal shield.

4
OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

The last stages must be decoupled by means of capacitances to avoid a serious voltage drop on the dynodes. A practical value for C_1 could be 2.10^{-9} F. In the case of high counting rates and large peak power output, and to avoid a high-tension supply of large power, it is possible to supply the first stages with a high tension of small output and the end stages with an average voltage of high output.

A. The electron optical input system consists of four elements:

the photocathode k; the focusing electrode g_1 ; the accelerating electrode acc; the deflector g_2 .

To reduce transit-time fluctuations, geometrical time spread, pulse amplitude spread or dark current, this system has the following advantages:

- 1. the photocathode is curved, though the outer window surface is flat, thus facilitating optical coupling to a scintillator.
- 2. a high and homogeneous extraction field at the cathode reduces as much as possible the influence of the initial electron velocities. A cathode-to-accelerator (internally connected to the first dynode) voltage of 350 V ensures a field strength of about 40 V/cm. This field is homogenized at the cathode surface by the focusing electrode g_1 . Fig.1 shows the electron path in the input system.
- 3. The potential of electrode g_1 to the photocathode can be adjusted in order to obtain one of the following characteristics:
 - a. the most satisfactory collection (i.e. for a given luminous flux the largest obtainable anode signal); for this adjustment, see Fig.2 the optimum value of the potential is about $0.15 V_S$;
 - b. the slightest transit-time fluctuations (the most homogeneous extraction field);
 - c. the most satisfactory uniformity of collection giving the most constant output pulse amplitude;
 - d. the useful cathode area can be controlled by giving the electrode g_1 a negative potential with respect to the photocathode, as shown in Fig.3, 4 and 5; obviously this variable electronic iris has the effect of reducing the dark current since the electrons emitted at the edge of the cathode do not reach the first dynode and consequently do not contribute to the anode current.







Fig.2 Anode current variation with the adjustment of g_1



Fig.3







Fig.5

- 4. Because the first dynode cannot be placed parallel to the photocathode, the beam of primary electrons is deflected by the electrode g_2 to make it impinge at right angles to the first dynode surface. Collection on the first dynode is controlled by the potential of the third dynode (see recommended circuits).
- B. The multiplier system consists of 14 stages, providing a total current amplification of 10⁸ at about 2500 V (see Fig.6).

The tube is capable of producing very strong peak currents (up to 1 A). Actually, the time constant at the output of the multiplier must be very small. Therefore it is necessary, taking into account the parasitic capacitances, to use a low-load resistance. It is advisable to use a resistance-matched coaxial cable (e.g. 75 or 100 Ω). With this load the tube easily delivers pulses of tens of volts, so that an amplifier is rendered superfluous.

Fig.7 illustrates the variation of the anode current as a function of the incident flux, the voltage divider being of type B. The anode current is then linear up to 300 mA.

Care should be taken that the anode voltage is adjusted to its optimum value. In fig.8 the anode current variation is plotted against anode-to-final-dynode voltage.

It should be noted that at equal high tensions the gain of the tube is smaller for voltage divider type B than for one according to type A. In practice, therefore, it will be preferable to use the type A distribution, or a distribution between A and B (e.g. starting with 1.2 $\rm V_S$ between S₈ and S₉, 1.5 $\rm V_S$ between S₉ and S₁₀ and so on, maintaining the same progression.

It is advisable to screen the tube with a mu-metal cylinder against magnetic-field influences.

56 TVP



Fig.6

A

56TVP



Fig.7

56 TVP



Fig.8

С

14 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in nuclear physics where a high degree of time definition or a high time resolution is required, combined with a good sensitivity in the ultraviolet region.

| QUICK REFERENCE DATA | | | |
|-------------------------------------|-------------|-----|--|
| Spectral response | type U (S | 13) | |
| Useful diameter of the photocathode | 42 r | nm | |
| Gain (at 2200 V) | 108 | | |
| Anode pulse rise time | 2 r | ıs | |
| Linearity | up to 300 m | nA | |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 20-pin (Jedec B20-102)



| ACC | ESSO | RIES |
|-----|------|------|
|-----|------|------|

| Socket | type | FE1003 |
|---------------------------------|--------------|----------------|
| Mu-metal shields ¹) | type type | 56130 56131 |

GENERAL

| Photocathode | | | | |
|--|--------------------------------------|---------------|----------------|----------------|
| Description | semi-transparent, head | d-on, cu | rved | surface |
| Cathode material | | С | s-Sb | |
| Minimum useful diameter | | | 42 | mm |
| Radius of curvature | | max. | 69 | mm |
| Spectral response curve ²) | | type l | J (S 13 | 3) |
| Wavelength at maximum response | | 4000 <u>+</u> | 300 | A |
| Luminous sensitivity ³) | Nk | av. min. | 65 45 | μA/lm μA/lm |
| Radiant sensitivity at 4000 Å | | | 55 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 14 | |
| Dynode material | | Ag-Mg | g-0-0 | Cs |
| Capacitances | | | | |
| Grid No.1 to accelerator electrode | Cg ₁ /acc, S ₁ | | 25 | pF |
| Grid No.2 to all other electrodes | Cg ₂ | | 7 | pF |
| Anode to final dynode | C _{a/S₁₄} | | 7 | pF |
| Anode to all other electrodes | Ca | | 9.5 | pF |

To avoid electric field distortion in the electron optical system the aquadag shield (pin No.18) must be connected to a voltage near to the cathode voltage. If the cathode is connected to the negative H.T., precautions should be taken to ensure a high-tension insulation between the aquadag shield and the mumetal shield.

2) See spectral response curve in front of this section.

 $^3)$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{\rm 0}{\rm K}$ 7Z2 5792

TYPICAL CHARACTERISTICS

| With voltage divider A | | | | |
|--|--|--------------|--------------------|----------|
| Supply voltage for G = 10^8 | v _b | av. max. | 2200 2500 | v v |
| Anode dark current at G = 10^8 ¹) | I _{ao} | av. max. | 0.5 5.0 | μΑ μΑ |
| Linearity between anode pulse amplitude and input light pulse | | up to | 100 | mA |
| With voltage divider B | | | | |
| Linearity between anode pulse amplitude and input light pulse | | up to | 300 | mA. |
| Anode pulse rise time at V_b = 2500 V ²) | | | 2.10 ⁻⁹ | s |
| Anode pulse width at half height at V_b = 2500 | V 2) | | 4.10-9 | s |
| Transit time difference between the centre o the photocathode and the edge at V_b = 2500 | f V | max. 5 | .10-10 | s |
| Total transit time at V_b = 2500 V ²) | | 3 | 6.10-9 | s |
| Maximum peak currents | | (| 0.5 to 1 | А |
| LIMITING VALUES (Absolute max. rating s | ystem) | | | |
| Supply voltage ³) | Vb | max. | 2500 | v |
| Continuous anode current | Ia | max. | 2 | mA |
| Voltage between cathode and first dynode | v _{k/S1} | max. min. | 800 250 | V V |
| Voltage between grid No.1 and cathode | V _{k/g1} | max. | 100 | v |
| Voltage between grid No.2 and first dynode | V_{g_2}/S_1 | max. | 100 | V |
| Voltage between consecutive dynodes | V _{S_n/S_{n+1}} | max. min. | 500 80 | V V |
| Voltage between anode and final dynode ⁴) | $V_{a/S_{14}}$ | max. min. | 500 80 | V V |

 $^{\rm l})$ At an ambient temperature of 25 $^{\rm o}C.$

²) For an infinitely short light pulse, fully illuminating the photocathode.

³) Or the voltage at which the tube circuited in the voltage divider A has a gain of about 10^9 , whichever is lowest.

 When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5793

RECOMMENDED CIRCUITS







Voltage divider type B¹)

- k .= cathode
- $g_1 = focusing electrode$
- acc = accelerating electrode
- $g_2 = deflector$
- $S_n = dynode No.n$
- a = anode

voltage between k and g_1 to be adjusted at about 0.15 $V_{\rm S}$ (see fig.2); voltage between S_2 and S_3 to be adjusted at about 1.2 $V_{\rm S}$; decoupling capacitances C_1 = 100 q/V_{\rm S}, C_2 = 100 q/3V_{\rm S}, C_3 = 100 q/9V_{\rm S},

 $C_4 = 100 \text{ q}/27 \text{V}_S$ etc. with q = quantity of electricity transported by the anode.

¹) To avoid electric field distortion in the electron optical system the aquadag shield (pin No.18) must be connected to a voltage near to the cathode voltage. If the cathode is connected to the negative H.T., precautions should be taken to ensure a high-tension insulation between the aquadag shield and the mumetal shield. 7Z2 5794

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of about 3 mA will be sufficient.

The last stages must be decoupled by means of capacitances to avoid a serious voltage drop on the dynodes. A practical value for C_1 could be 2.10^{-9} F. In the case of high counting rates and large peak power output, and to avoid a high-tension supply of large power, it is possible to supply the first stages with a high tension of small output and the end stages with an average voltage of high output.

A. The electron optical input system consists of four elements:

the photocathode k; the focusing electrode g_1 ; the accelerating electrode acc; the deflector g_2 .

To reduce transit-time fluctuations, geometrical time spread, pulse amplitude spread or dark current, this system has the following advantages:

- 1. the photocathode is curved, though the outer window surface is flat, thus facilitating optical coupling to a scintillator.
- 2. a high and homogeneous extraction field at the cathode reduces as much as possible the influence of the initial electron velocities. A cathode-to-accelerator (internally connected to the first dynode) voltage of 350 V ensures a field strength of about 40 V/cm. This field is homogenized at the cathode surface by the focusing electrode g_1 . Fig.1 shows the electron path in the input system.
- 3. The potential of electrode g_1 to the photocathode can be adjusted in order to obtain one of the following characteristics:
 - a. the most satisfactory collection (i.e. for a given luminous flux the largest obtainable anode signal); for this adjustment, see Fig.2 the optimum value of the potential is about 0.15 V_S ;
 - b. the slightest transit-time fluctuations (the most homogeneous extraction field);
 - c. the most satisfactory uniformity of collection giving the most constant output pulse amplitude;
 - d. the useful cathode area can be controlled by giving the electrode g₁ a negative potential with respect to the photocathode, as shown in Fig.3, 4 and 5; obviously this variable electronic iris has the effect of reducing the dark current since the electrons emitted at the edge of the cathode do not reach the first dynode and consequently do not contribute to the anode current. 7Z2 5795







Fig.2 Anode current variation with the adjustment of g_1

OPERATIONAL CONSIDERATIONS (continued)



Fig.3







Fig.5

- 4. Because the first dynode cannot be placed parallel to the photocathode, the beam of primary electrons is deflected by the electrode g_2 to make it impinge at right angles to the first dynode surface. Collection on the first dynode is controlled by the potential of the third dynode (see recommended circuits).
- B. The multiplier system consists of 14 stages, providing a total current amplification of 10^8 at about 2200 V (See Fig.6).

The tube is capable of producing very strong peak currents (up to 1 A). Actually, the time constant at the output of the multiplier must be very small. Therefore it is necessary, taking into account the parasitic capacitances, to use a low-load resistance. It is advisable to use a resistance-matched coaxial cable (e.g. 75 or 100 Ω). With this load the tube easily delivers pulses of tens of volts, so that an amplifier is rendered superfluous.

It should be noted that in a number of applications it is not necessary for the current to be proportional to the incident luminous flux. As a matter of fact such short pulses are needed for time measurements only, so not for spectrography purposes. If at the same time it is required, however, to determine the energy of the incident radiation, it is possible to select from one of the dynodes a signal proportional to the incident flux. In fact, when ascending the dynodes progressively, starting from the anode, the current is divided at each stage by d-1, d representing the secondary-emission coefficient of each stage (d \approx 3.5). It is therefore possible to locate a dynode, the current of which is lower than, or equal to, the saturation limit of the dynodes.

Fig.7 illustrates the variation of the anode current as a function of the incident flux, the voltage divider being of type B. The anode current is then linear up to 300 mA.

Care should be taken that the anode voltage is adjusted to its optimum value. In fig.8 the anode current variation is plotted against anode-to-final-dynode voltage.

It should be noted that for equal high tension the gain of the tube is smaller for voltage divider type B than for one according to type A. In practice, therefore, it will be preferable to use the type A distribution, or a distribution between A and B (e.g. starting with 1.2 V_S between S₈ and S₉ 1.5 V_S between S₉ and S₁₀ and so on, maintaining the same progression).

It is advisable to screen the tube with a mu-metal cylinder against magnetic-field influences.



Fig.6

A



Fig.7

В



Fig.8

С

11 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in applications such as total body radiation measurements, uranium prospecting with very large scintillators, Cerenkov light measurements in large transparent objects.

| QUICK REFERENCE DATA | |
|-------------------------------------|--------------|
| Spectral response | type A (S11) |
| Useful diameter of the photocathode | 200 mm |
| Anode sensitivity (at 1800 V) | 250 A/lm |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 14-pin (Jedec B14-38)



7Z2 5753

1

| ACCESSORIES | | | | | |
|--|-------------------|---------------------|-------------|----------------|----------------------|
| Socket | type | FE1001 | | | |
| Mu-metal shield | type | 56132 | | | |
| GENERAL | | | | | |
| Photocathode | | | | | |
| Description s | emi- | transparent, head-o | on, curv | ed su | rface ¹) |
| Cathode material | | | C | s-Sb | |
| Minimum useful diameter | | | | 200 | mm |
| Radius of curvature | | | | 186 | mm |
| Spectral response curve 2) | | | type | A (S11 |) |
| Wavelength at maximum response | | | 4200 - | - 300 | R |
| Luminous sensitivity 3) | | N _k | av. min. | 50 35 | μA/lm μA/lm |
| Radiant sensitivity at 4200 ${\rm \AA}$ | | | | 45 | mA/W |
| Multiplier system | | | | | |
| Number of stages | | | | 11 | |
| Dynode material | | | Ag-M | g - 0-C | Cs |
| Capacitances | | | | | |
| Anode to final dynode | | $C_{a/S_{11}}$ | | 3 | pF |
| Anode to all other electrodes | | Ca | | 5 | pF |
| TYPICAL CHARACTERISTICS | | | | | |
| With voltage divider A | | | | | |
| Anode sensitivity at V _b = 1800 V | | Na | av. min. | 250 60 | A/lm A/lm |
| Anode dark current at $N_a = 60$ A/lm | n. ⁴) | Iao | max. | 1 | μΑ |
| Linearity between anode pulse ampliand input light pulse | litude | 9 | up to | 30 | mA |
| | | A CARLES Services | 1.18 | 1. | 10.2 |

- The tube is delivered with a plane-concave plexiglass adaptor and with a metal envelope
- 2) See spectral response curve in front of this section

3) Measured with a tungsten ribbon lamp having a colour temperature of 2850 °K
4) At an ambient temperature of 25 °C 7Z2 5754

2



max. 1000 V

max.

min.

max.

min.

300 V

300 V

80 V

80 V

| TYPICAL CHARACTERISTICS (continued) | | | |
|---|--------------------------------|--------------------|--------|
| With voltage divider B | | | |
| Linearity between anode pulse amplitude and input light pulse | | up to 100 | mA |
| Anode pulse rise time at V _b = 2500 V 1) | | 5.10-9 | S |
| Anode pulse width at half height at V_b = 2500 | V | 10.10-9 | s |
| Transit time difference between the centre of the photocathode and the edge at V_b = 2500 V | V | 4.10 ⁻⁹ | s |
| Total transit time at V_b = 2500 V | | 50.10-9 | s |
| LIMITING VALUES (Absolute max. rating sy | stem) | | |
| Supply voltage | Vb | max. 2500 | V |
| Continuous anode current | Ia | max. 1 | mA |
| Voltage between cathode and first dynode | V _k /S ₁ | max. 1000 | V V |

V_{k/acc}

 $v_{S_n/S_{n+1}}$

Va/S11

Voltage between cathode and accelerator electrode

Voltage between consecutive dynodes

Voltage between anode and final dynode 2)

1) For an infinitely short light pulse.

²) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5755

RECOMMENDED CIRCUITS









| k | = | cathode | Sn | = | dynode | No.n |
|-----|---|------------------------|----|---|--------|------|
| acc | = | accelerating electrode | а | Ξ | anode | |

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of about 1 mA will be sufficient.

With the voltage divider type A the tube gives the highest gain, while with the voltage divider type B the tube can deliver a higher anode current output with better time characteristics.

The accelerating electrode has a separate external connection to allow adjustment for optimum photoelectron collection on the first dynode.

In pulse techniques, such as scintillation counting, it is advisable to decouple the last two or three stages by means of capacitors of 100 pF and 200 pF (the highest value at the last stage).

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.



A

14 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in nuclear-physics applications where a high degree of time definition is required (fast coincidences, Cerenkov counters).

| QUICK REFERENCE DATA | | | |
|-------------------------------------|-----------------|-------|--|
| Spectral response | type A | (S11) | |
| Useful diameter of the photocathode | 110 | mm | |
| Gain (at 2400 V) | 10 ⁸ | | |
| Anode pulse rise time | 2 | ns | |
| Linearity | . up to 300 | mA | |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

g1

q2 acc g3

Base: 20-pin (Jedec B20-102) max 136.5* 115¢±1 1200 =180±5 2 aquadag shield 174±5 max 131¢ 276±5 259±5 51 80¢ S14 CCCC A S12 ac S10 S13 0 S14 58 S11 56¢ 56 59 06 54 57 23+1 **S**2 \$5 minom NOTO O DOL SE 7203273 g2+5 dag shield max 51.8¢ max 91* 7207302

ACCESSORIES

| Socket | type | FE1003 |
|---|------|----------|
| Mu-metal shield (tube with metal container) | type | 56133 |
| (tube without metal container) | type | 56129 |
| | | 7Z2 8267 |

GENERAL

| Description | semi-transparent, head | d-on, curved sur | rface ¹) |
|---|------------------------|-----------------------|----------------------|
| Cathode material | | Cs-Sb | |
| Minimum useful diameter | | 110 | mm |
| Radius of curvature | | 180 ± 5 | mm |
| Spectral response curve ²) | | type A (S1 | 1) |
| Wavelength at maximum respons | e | 4200 ± 300 | 8 |
| Luminous sensitivity 3) | N _k | av. 70 min. 45 | μA/lm μA/lm |
| Radiant sensitivity at 4200 $ m \AA$ | | 60 | mA/W |
| Multiplier system | | | |
| Number of stages | | 14 | |
| Dynode material | Ag-Mg-O-0 | | |
| Capacitances | | | |
| Anode to final dynode | $C_{a/S_{14}}$ | 5 | pF |
| Anode to all other electrodes | C _a | 7 | pF |
| TYPICAL CHARACTERISTICS | | | |
| With voltage divider A | | | |
| Supply voltage for $G = 10^8$ | V _b | av. 2400 max. 3000 | V V |
| Anode dark current at G = $10^8 \frac{4}{2}$ | I _{ao} | av. 2 max. 12 | μΑ μΑ |
| Linearity between anode pulse and and input light pulse | nplitude | up to 100 | mA |

 $^{\rm l})$ The tube is delivered with a plexiglass plane-concave adaptor and with a metal envelope

- 2) See spectral response curve in front of this section
- ³) Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{\rm O}{\rm K}$
- 4) At an ambient temperature of 25 $^{\mathrm{o}}\mathrm{C}$



TYPICAL CHARACTERISTICS (continued)

With voltage divider B

| Linearity between anode pulse amplitude | | |
|---|--------------------|----|
| and input light pulse | up to 300 | mA |
| Anode pulse rise time at V_b = 3000 V 1) | 2.10-9 | S |
| Anode pulse width at half height at V_b = 3000 V 1) | 4.10 ⁻⁹ | s |
| Transit time difference between the centre of the photocathode and the edge at V _b = 3000 V | 10-9 | s |
| Total transit time at V _b = 3000 V 1) | 45.10-9 | s |
| Maximum peak currents | 0.5 to 1 | А |
| | | |

LIMITING VALUES (Absolute max. rating system)

| Supply voltage ²) | Vb | max. | 3000 | V |
|---|--------------------|--------------|------------|--------|
| Continuous anode current | Ia | max. | 2 | mA |
| Voltage between cathode and first dynode + grid No.2 | v_{k/S_1+g_2} | max. min. | 800 250 | V V |
| Voltage between cathode and accelerator electrode | V _{k/acc} | 1400 to | 1800 | v |
| Voltage between grid No.1 and cathode | V _{k/g1} | max. | 300 | V |
| Voltage between grid No.3 and first dynode | v_{g_3/S_1} | max. | 100 | V |
| Voltage between consecutive dynodes | $v_{S_n/S_{n+1}}$ | max. min. | 500 80 | V V |
| Voltage between anode and final dynode ³) | $v_{a/S_{14}}$ | max. min. | 500 80 | V V |

¹) For an infinitely short light pulse, fully illuminating the photocathode

³) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5687

²) Or the voltage at which the tube circuited in the voltage divider A has a gain of about 10^9 , whichever is lowest.

RECOMMENDED CIRCUITS



Voltage divider type A 1)





k = cathode

- g_1 = focusing electrode
- g₂ = focusing electrode
- acc = accelerating electrode
- $g_3 = deflector$
- $S_n = dynode No.n$
- a = anode

voltage between k and g_1 to be adjusted at about 2 V_S; voltage between S₂ and S₃ to be adjusted at about 1.2 V_S; decoupling capacitances C₁ = 100q/V_S, C₂ = 100q/3V_S, C₃ = 100q/9V_S, C₄ = 100q/27V_S etc. with q = quantity of electricity transported by the anode.

 If the cathode is connected to negative HT, precautions should be taken to ensure a high-tension insulation between the aquadag shield and the metal envelope or mu-metal shield.
 7Z2 5688

4

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of about 3 mA will be sufficient.

The last stages must be decoupled by means of capacitances to avoid a serious voltage drop on the dynodes. A practical value of C_1 will be 2.10^{-9} F.

In the case of high counting rates and large peak power outputs, and to avoid a high-tension supply of large power, it is possible to supply the first stages with a high tension of small output and the end stages with an average voltage of high output.

A. The electron optical input system consists of five elements:

the photocathode k; the focusing electrode g_1 ; the focusing electrode g_2 ; the accelerating electrode acc; the deflector g_3 .

To reduce transit-time fluctutations and geometrical time spread, this system has the following advantages.

- 1. The photocathode is curved, with a curvature radius of 183 mm. To facilitate optical coupling to scintillators the tube is delivered with a plexiglass plane-concave adaptor.
- 2. A high and homogeneous extraction field at the cathode reduces as much as possible the influence of the initial electron velocities. A cathode-to-accelerating voltage of about 1500 V (to be connected to the tenth or a subsequent dynode) ensures a field strength of about 40 V/cm. This field is homogenized at the cathode surface by the focusing electrode g_1 . Fig.1 shows the electron paths in the input system.
- 3. The potential of the electrode g_1 to the photocathode can be adjusted in order to obtain one of the following characteristics:
 - (a) the most satisfactory collection (i.e. for a given luminous flux the largest obtainable anode signal); the optimum value of the potential is about 2 V_s;
 - (b) the slightest transit-time fluctuations (the most homogeneous extraction field);
 - (c) the most satisfactory uniformity of collection giving the most constant output pulse amplitude.





4. Because the first dynode cannot be placed parallel to the photocathode, the beam of primary electrons is deflected by the electrode g_3 to make them impinge at right angles to the first dynode surface.

Collection on the first dynode is controlled by the potential of the third dynode.

B. The multiplier system consists of 14 stages, providing a total current amplification of 10^8 at about 2400 V (see fig.2). The tube is capable of producing very strong peak currents (up to 1 A) Actually, the time constant at the output of the multiplier must be very small. Therefore it is necessary, taking into account the parasitic capacitances, to use a low load resistance. It is advisable to use a resistance-matched coaxial cable (e.g. 75 or 100Ω). With this load the tube easily delivers pulses of tens of volts, so that an amplifier is rendered superfluous.

It should be noted that in a number of applications it is not necessary for the current to be proportional to the incident luminous flux. As a matter of fact, such pulses are needed for time measurements only, so not for spectro-graphy purposes.

If at the same time it is required, however, to determine the energy of the incident radiation, it is possible to select from one of the dynodes a signal proportional to the incident flux. In fact, when ascending the dynodes progressively, starting from the anode, the current is divided at each stage by d-1, d representing the secondary-emission coefficient of each stage (d \approx 3.5). It is therefore possible to locate a dynode, the current of which is lower than, or equal to, the saturation limit of the dynodes.

Fig.3 illustrates the variation of the anode current as a function of the incident flux, the voltage divider being of type B. The anode current is then linear up to 300 mA.

Care should be taken that the anode voltage is adjusted to its optimum value. In fig.4 the anode current variation is plotted against anode-to-final dynode voltage.

It should be noted that for equal high tensions the gain of the tube is smaller for voltage divider type B than for one according to type A.

In practice, therefore, it will be preferable to use the A type distribution, or a distribution between A and B, (e.g. starting with 1.2 V_S between S₈ and S₉, 1.5 V_S between S₉ and S₁₀ etc., maintaining the same progression).

It is advisable to screen the tube with a mu-metal cylinder against magneticfield influence.



Fig.2

A



Fig.3



Fig.4

С
14 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in nuclear -physics applications where a high degree of time definition is required, combined with a good sensitivity in the ultraviolet region.

| QUICK REFERENCE DAT. | A | |
|-------------------------------------|-----------------|-------|
| Spectral response | type U | (S13) |
| Useful diameter of the photocathode | 110 | mm |
| Gain (at 2400 V) | 10 ⁸ | |
| Anode pulse rise time | 2 | ns |
| Linearity | up to 300 | mA |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 20-pin (Jedec B20-102)



7Z2 8268

1

ACCESSORIES

| Socket | type | FE1003 |
|--------------------------------|------|--------|
| Mu-metal shield ¹) | type | 56133 |
| Quartz adaptor | type | 56137 |

GENERAL

| Photocathode | | | |
|---|-------------------------------|--------------|----------------|
| Description | semi-transparent, head-on, cu | irved | surface |
| Cathode material | C | s-Sb | |
| Minimum useful diameter | | 110 | mm |
| Spectral response curve ²) | type | U (S13 | 3) |
| Wavelength at maximum response | 4000 - | <u>+</u> 300 | 8 |
| Luminous sensitivity 3) | N _k av. min. | 70 45 | μA/lm μA/lm |
| Radiant sensitivity at 4000 Å | | 60 | mA/W |
| Multiplier system | | | |
| Number of stages | | 14 | |
| Dynode material | Ag-Mg-O-Cs | | Cs |
| Capacitances | | | |
| Anode to final dynode | $C_{a/S_{14}}$ | 5 | pF |
| Anode to all other electrodes | C _a | 7 | pF |
| TYPICAL CHARACTERISTICS | | | |
| With voltage divider A | | | |
| Supply voltage for $G = 10^8$ | V _b av. max. | 2400 3000 | V V |
| Anode dark current at $G = 10^8 4$) | I _{ao} av. max. | 2 12 | μΑ μΑ |
| Linearity between anode pulse ampli- and input light pulse | tude up to | 100 | mA |
| | | | |

 $(1)^{2})^{3})^{4}$) See page 3.



TYPICAL CHARACTERISTICS (continued)

With voltage divider B

| Linearity between anode pulse amplitude | | |
|---|--------------------|----|
| and input light pulse | up to 300 | mA |
| Anode pulse rise time at V_b = 3000 V ⁵) | 2.10 ⁻⁹ | s |
| Anode pulse width at half height at V_b = 3000 V ⁵) | 4.10-9 | S |
| Transit time difference between the centre of | | |
| the photocathode and the edge at V_b = 3000 V- | 10-9 | S |
| Total transit time at V_b = 3000 V ⁵) | 45.10-9 | s |
| Maximum peak currents | 0.5 to 1 | А |
| | | |

LIMITING VALUES (Absolute max. rating system)

| Supply voltage ⁶) | Vb | max. | 3000 | V |
|---|--|--------------|------------|--------|
| Continuous anode current | Ia | max. | 2 | mA |
| Voltage between cathode and first dynode + grid No.2 and grid No.3 | V _k /S ₁ +g ₂ +g ₃ | max. min. | 800 250 | v v |
| Voltage between cathode and accelerator electrode | V _{k/acc} | 1400 to | 1800 | v |
| Voltage between grid No.1 and cathode | V _{k/g1} | max. | 300 | V |
| Voltage between consecutive dynodes | $v_{S_n/S_{n+1}}$ | max. min. | 500 80 | v v |
| Voltage between anode and final dynode 7) | V _a /S ₁₄ | max. min. | 500 80 | V V |

 To avoid electric-field distortion in the electron optical system the aquadag shield (pin No.18) must be connected to the cathode. If the cathode is connected to the negative HT, precautions should be taken to ensure a hightension insulation between the aquadag shield and the mu-metal shield.

 2) See spectral response curve in front of this section.

 $^3)$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{\rm O}{\rm K}$

4) At an ambient temperature of 25 °C

⁵) For an infinitely short light pulse, fully illuminating the photocathode

6) Or the voltage at which the tube circuited in the voltage divider A has a gain of about 10⁹, whichever is lowest.

7) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5694

3

RECOMMENDED CIRCUITS



Voltage divider type A 1)



Voltage divider type B 1)

- k = cathode
- $g_1 = focusing electrode$
- g₂ = focusing electrode
- acc = accelerating electrode
- $g_3 = deflector$
- $S_n = dynode No.n$
- a = anode

voltage between k and g_1 to be adjusted at about 2 V_S; voltage between S₂ and S₃ to be adjusted at about 1.2 V_S; decoupling capacitances C₁ = 100q/V_S, C₂ = 100q/3V_S, C₃ = 100q/9V_S, C₄ = 100q/27V_S etc. with q = quantity of electricity transported by the anode.

¹) To avoid electric-field distortion in the electron optical system the aquadag shield (pin No.18) must be connected to the cathode. If the cathode is connected to the negative HT, precautions should be taken to ensure a hightension insulation between the aquadag shield and the mu-metal shield.

7Z2 5695

4

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of about 3 mA will be sufficient.

The last stages must be decoupled by means of capacitances to avoid a serious voltage drop on the dynodes. A practical value of C_1 will be 2.10⁻⁹ F.

In the case of high counting rates and large peak power outputs, and to avoid a high-tension supply of large power, it is possible to supply the first stages with a high tension of small output and the end stages with an average voltage of high output.

A. The electron optical input system consists of five elements:

the photocathode k; the focusing electrode g_1 ; the focusing electrode g_2 ; the accelerating electrode acc; the deflector g_3 .

To reduce transit-time fluctuations and geometrical time spread, this system has the following advantages.

- 1. The photocathode is curved, with a curvature radius of 183 mm. To facilitate optical coupling to scintillators, a quartz adaptor can be delivered with the tube.
- 2. A high and homogeneous extraction field at the cathode reduces as much as possible the influence of the initial electron velocities. A cathode-to-accelerating voltage of about 1500 V (to be connected to the tenth or a subsequent dynode) ensures a field strength of about 40 V/cm. This field is homogenized at the cathode surface by the focusing electrode g_1 . Fig.1 shows the electron paths in the input system.
- 3. The potential of the electrode g_1 to the photocathode can be adjusted in order to obtain one of the following characteristics:
 - (a) the most satisfactory collection (i.e. for a given luminous flux the largest obtainable anode signal); the optimum value of the potential is about 2 V_s;
 - (b) the slightest transit-time fluctuations (the most homogeneous extraction field);
 - (c) the most satisfactory uniformity of collection giving the most constant output pulse amplitude.

OPERATIONAL CONSIDERATIONS (continued)





OPERATIONAL CONSIDERATIONS (continued)

4. Because the first dynode cannot be placed parallel to the photocathode, the beam of primary electrons is deflected by the electrode g_3 to make them impinge at right angles to the first dynode surface.

Collection on the first dynode is controlled by the potential of the third dynode.

B. The multiplier system consists of 14 stages, providing a total current amplification of 10^8 at about 2400 V (see fig.2). The tube is capable of producing very strong peak currents (up to 1 A). Actually, the time constant at the output of the multiplier must be very small. Therefore it is necessary, taking into account the parasitic capacitances, to use a low load resistance. It is advisable to use a resistance-matched coaxial cable (e.g. 75 or 100Ω). With this load the tube easily delivers pulses of tens of volts, so that an amplifier is rendered superfluous.

It should be noted that in a number of applications it is not necessary for the current to be proportional to the incident luminous flux. As a matter of fact, such pulses are needed for time measurements only, so not for spectro-graphy purposes.

If at the same time it is required, however, to determine the energy of the incident radiation, it is possible to select from one of the dynodes a signal proportional to the incident flux. In fact, when ascending the dynodes progressively, starting from the anode, the current is divided at each stage by d-1, d representing the secondary-emission coefficient of each stage (d \approx 3.5). It is therefore possible to locate a dynode, the current of which is lower than, or equal to, the saturation limit of the dynodes.

Fig.3 illustrates the variation of the anode current as a function of the incident flux, the voltage divider being of type B. The anode current is then linear up to 300 mA.

Care should be taken that the anode voltage is adjusted to its optimum value. In fig.4 the anode current variation is plotted against anode-to-final dynode voltage.

It should be noted that for equal high tensions the gain of the tube is smaller for voltage divider type B than for one according to type A.

In practice, therefore, it will be preferable to use the A type distribution, or a distribution between A and B, (e.g. starting with 1.2 V_S between S₈ and S₉, 1.5 V_S between S₉ and S₁₀ etc., maintaining the same progression).

It is advisable to screen the tube with a mu-metal cylinder against magnetic-field influence.



Fig.2

A



Fig.3



Fig.4

С

12 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in large solid or liquid scintillator detectors, when a high time resolution is required.

| QUICK REFERENCE DA | ATA | |
|-------------------------------------|-----------------|-------|
| Spectral response | type A (| (S11) |
| Useful diameter of the photocathode | 300 | mm |
| Gain (at 3000 V) | 10 ⁸ | |
| Anode pulse rise time | 2.5 | ns |
| Linearity | up to 300 | mA |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 20-pin (Jedec B20-102)



TENTATIVE DATA

1

| AGGEOURIED | | STOLED BEN | | | |
|--|---------|-------------------|-------------|--------------|----------------|
| Socket | type | FE1003 | | | |
| Mu-metal shield | type | 56132 | | | |
| GENERAL | | | | | |
| Photocathode | | | | | |
| Description | sem | i-transparent, he | ad-on, c | urved | surface |
| Cathode material | | | (| Cs-Sb | |
| Minimum useful diameter | | | | 200 | mm |
| Radius of curvature | | | | 186 | mm |
| Spectral response curve ¹) | | | type | A (S1) | 1) |
| Wavelength at maximum response | | | 4200 | <u>+</u> 300 | A |
| Luminous sensitivity ²) | | N _k | av. min. | 50 35 | μA/lm μA/lm |
| Radiant sensitivity at 4200 Å | | | | 45 | mA/W |
| Multiplier system | | | | | |
| Number of stages | | | | 12 | |
| Dynode material | | | Ag-N | lg-0-0 | Cs |
| Capacitances | | | | | |
| Anode to final dynode | | $C_{a/S_{12}}$ | | 7 | pF |
| Anode to all other electrodes | | Ca | | 8 | pF |
| TYPICAL CHARACTERISTICS | | | | | |
| With voltage divider A | | | | | |
| Linearity between anode pulse amp and input light pulse | olitude | 2 | up to | 100 | mA |
| Anode dark current at G = 10^8 3) | | Iao | max. | 50 | μA |
| Supply voltage for $G = 10^8$ | | Vb | av. max. | 3000 3500 | V V |
| 1) See spectral response curve in f | ront o | of this section | | | |

 $^3)$ At an ambient temperature of 25 $^{\rm o}{\rm C}$

7Z2 8080

min.

| TYPICAL CHARACTERISTICS (continued) | | | |
|---|--------------------|-----------------------|--------|
| With voltage divider B | | | |
| Linearity between anode pulse amplitude and input light pulse | | up to 300 | mA |
| Anode pulse rise time at V_b = 3000 V ¹) | | 2.5.10 ⁻⁹ | s |
| Anode pulse width at half height at V_b = 3000 V | ^{7 1}) | 4.10-9 | s |
| Transit time difference between the centre of the photocathode and the edge at $V_b = 3000 \text{ V}$ | | 2.10-9 | S |
| Total transit time at V_b = 3000 V 1) | 45.10-9 | s | |
| Maximum peak current | | 0.5 to 1 | А |
| LIMITING VALUES (Absolute max. rating sys | stem) | | |
| Supply voltage ²) | Vb | max. 3000 | v |
| Continuous anode current | Ia | max. 2 | mA |
| Voltage between cathode and first dynode | v_k/s_1 | max. 1000 min. 350 | v v |
| Voltage between consecutive dynodes | $v_{S_n/S_{n+1}}$ | max. 500 min. 80 | v v |
| Voltage between anode and final dynode ³) | V _{a/S12} | max. 500 min. 80 | V V |

¹) For an infinitely short light pulse, fully illuminating the photo cathode

 $^2)$ Or the voltage at which the tube circuited in the voltage divider A has a gain of $10^9,\,$ whichever is lowest.

3) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked 7Z2 8081

1.1.1967

RECOMMENDED CIRCUITS



Voltage divider type A





The accelerator to be adjusted for maximum gain The grid to be adjusted for fastest response

k = cathode S_n = dynode No.n acc = accelerating electrode a = anode

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of about 5 mA will be sufficient.

The last stages must be decoupled by means of capacitances to avoid a serious voltage drop on the dynodes. A practical value for C_1 could be 2.10^{-9} F. In the case of high counting rates and large peak power output, and to avoid a high-tension supply of large power, it is possible to supply the first stages with a high tension of small output and the end stages with an average voltage of high output.

The multiplier system consists of 12 stages, providing a total current amplification of 10^8 at about 3000 V (see Fig.1)

The tube is capable of producing very strong peak currents (up to 1 A). Actually, the time constant at the output of the multiplier must be very small. Therefore it is necessary, taking into account the parasitic capacitances, to use a low-load resistance. It is advisable to use a resistance-matched coaxial cable (e.g. 75 or 100Ω). With this load the tube easily delivers pulses of tens of volts, so that an amplifier is rendered superfluous.

To avoid the effects, which are responsible for rounding of the leading edge and the "jagged" trailing edges, a grid (g) is placed parallel to the anode with its wires aligned with those of the anode.

Thus electrons walking from the next-to-last dynode (S11) to the last dynode (S12) are prevented to impinge directly upon the anode.

At the same time induction and oscillations in the anode grid are minimized. The potential of this electrode is to be adjusted at an optimum close to that of the last dynode.

It should be noted that at equal high tension the gain of the tube is smaller for voltage divider type B than for one according to type A.

It is advisable to screen the tube with a mu-metal cylinder against magnetic-field influences.



Α



10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in applications such as scintillation counting, flying spot scanners, difference kinds of optical and industrial instruments.

| QUICK REFERENCE DATA | |
|-------------------------------------|--------------|
| Spectral response | type A (S11) |
| Useful diameter of the photocathode | 32 mm |
| Anode sensitivity (at 1800 V) | 700 A/lm |

DIMENSIONS AND CONNECTIONS

511

7203932

Base: 12-pin (Jedec B12-43)





Dimensions in mm

ACCESSORIES

SF

S

acc. S

Socket Mu-metal shield type FE1002 type 56127

| the second second | | | |
|-------------------|-----|----|--|
| GEN | JFR | ΔT | |

| Photocathode | | | | |
|---|-------------------|----------------|--------------|----------------|
| Description | semi-transparent, | head-on | , flat | surface |
| Cathode material | | C | Cs-Sb | |
| Minimum useful diameter | | | 32 | mm |
| Spectral response curve 1) | | type A | (S11) | |
| Wavelength at maximum response | | 4200 - | <u>+</u> 300 | 8 |
| Luminous sensitivity ²) | Nk | av. min. | 70 40 | μA/lm μA/lm |
| Radiant sensitivity at 4200 $ m \AA$ | | | 60 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 10 | |
| Dynode material | | Ag-Mg | -0-Cs | sinnin |
| Capacitances | | | | |
| Anode to final dynode | $C_{a/S_{10}}$ | | 3 | pF |
| Anode to all other electrodes | C _a | | 5 | pF |
| TYPICAL CHARACTERISTICS | | | | |
| With voltage divider A | | | | |
| Anode sensitivity at V_b = 1800 V | N _a | av. min. | 700 250 | A/lm A/lm |
| Anode dark current at $N_a = 60 \text{ A/lm}^3$) | I _{ao} | av. (max.(| 0.010 | μΑ μΑ |
| Linearity between anode pulse amplitud and input light pulse | le | up to | 30 | mA |
| | | | | |

1) See spectral response curve in front of this section

- $^2)$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{\rm O}{\rm K}$
- ³) At an ambient temperature of 25 $^{\circ}C$

300 V

80 V

max.

min.

Va/S10

| TYPICAL CHARACTERISTICS (continued) | | | |
|---|-------------------|----------------------|--------|
| With voltage divider B | | | |
| Linearity between anode amplitude and input light pulse | | up to 100 | mA |
| Anode pulse rise time at V _b = 1500 V 1) | | 4.10-9 | s |
| Transit time difference between the centre of the photocathode and the edge at $V_{L} = 1500 \text{ V}$ | | 3,10 ⁻⁹ | S |
| Total transit time at V_b = 1500 V | | 36.10-9 | s |
| LIMITING VALUES (Absolute max. rating sys | stem) | | |
| Supply voltage | v _b | max. 1800 | v |
| Continuous anode current | Ia | max. 1 | mA |
| Voltage between cathode and first dynode | v _{k/S1} | max. 500 min. 120 | v v |
| Voltage between consecutive dynodes | $v_{S_n/S_{n+1}}$ | max. 300 min. 80 | v v |

Voltage between anode and final dynode ²)

RECOMMENDED CIRCUITS



Voltage divider type A

k = cathode $S_n = \text{dynode No.n}$ acc = accelerating electrode a = anode

¹) For an infinitely short light pulse.

²) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 5592

RECOMMENDED CIRCUITS (continued)



Voltage divider type B

| k | = | cathode | Sn | = | dynode No.n |
|-----|---|------------------------|----|---|-------------|
| acc | = | accelerating electrode | а | = | anode |

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be sufficient.

Different kinds of voltage dividers are possible. A circuit of type A results in the highest gain of the tube at a given total voltage; a circuit of type B gives a higher current output with better time characteristics, but the total gain is less at the same total voltage.

When pulses with high amplitudes are taken from the anode, it is useful to decouple the last stages as indicated in the circuit by means of capacitors of a few hundred pF, to avoid a voltage drop between these stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.



Α



10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in applications such as infra-red telecommunication and ranging, and in optical instruments operating in-the far red and near infrared region (astronomical measurements, spectrometry, optical pyrometry, infra-red radiation intensity control instruments).

| QUICK REFERENCE DATA | |
|-------------------------------------|------------|
| Spectral response curve | type C(S1) |
| Useful diameter of the photocathode | 32 mm |
| Anode sensitivity (at 1800 V) | 100 A/lm |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 12-pin (Jedec B12-43)





ACCESSORIES

Socket

Mu-metal shield

acc

7703932

type FE1002 type 56127

| GENERAL | | | | |
|---|-------------------|---------------|-----------|----------------|
| Photocathode | | | | |
| Description | semi-transparent, | head-on | , flat | surface |
| Cathode material | | Ag-O- | Cs | 1.80 |
| Minimum useful diameter | | | 32 | mm |
| Spectral response curve 1) | | type C | C (S1) | |
| Wavelenght at maximum response | | 8000 <u>+</u> | 1000 | 8 |
| Luminous sensitivity 2) | N _k | av. min. | 25 15 | μA/lm μA/lm |
| Infra-red luminous sensitivity ³) | Nk | av. min. | 3 1.4 | μA/lm μA/lm |
| Radiant sensitivity at 8000 Å | | | 2.5 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 10 | |
| Dynode material | | Ag-Mg | -0-Cs | 5 |
| Capacitances | | | | |
| Anode to final dynode | C_a/S_{10} | | 3 | pF |
| Anode to all other electrodes | C _a | | 5 | pF |
| TYPICAL CHARACTERISTICS | | | | |
| With voltage divider A | | | | |
| Anode sensitivity at V_b = 1800 V | Na | av. min. | 100 20 | A/lm A/lm |
| Anode dark current at N _a = 20 A/lm 4) | I _{ao} | max. | 10 | μΑ |
| Linearity between anode pulse amplitud and input light pulse | е | up to | 5 | mA |
| ¹) See spectral response curve in front | of this section | | | |

 $^2)$ Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{\rm O}{\rm K}$

- ³) The infra-red lumen is the flux resulting from one lumen yielded by a tungsten ribbon lamp (colour temperature 2850 ^oK) going through an infra-red filter corning CS94 No.2540, fusion 1613 thickness 2.61
- 4) At an ambient temperature of 25 $^{\mathrm{o}}\mathrm{C}$

min.

max.

min.

80 V

300 V

> 80 V

 V_{S_n}/S_{n+1}

Va/S10

| TYPICAL CHARACTERISTICS (continued) | | | |
|--|-------------|----------------------|--------|
| With voltage divider B | | | |
| Linearity between anode pulse amplitude and input light pulse | | up to 10 | mA |
| Anode pulse rise time at V_b = 1500 V ¹) | | 4.10-9 | s |
| Transit time difference between the centre of the photocathode and the edge at V _b = 1500 V | | 3.10 ⁻⁹ | s |
| Total transit time at V_b = 1500 V | | 36.10 ⁻⁹ | S |
| LIMITING VALUES (Absolute max. rating syste | m) | | |
| Supply voltage | Vb | max. 1800 | v |
| Continuous anode current | Ia | max. 30 | μA |
| Voltage between cathode and first dynode | v_{k/S_1} | max. 500 min. 120 | v v |
| | | max. 300 | v |

Voltage between consecutive dynodes

Voltage between anode and final dynode 2)

RECOMMENDED CIRCUITS



= cathode k $S_n = dynode No.n$ acc = accelerating electrode anode a =

¹) For an infinitely short light pulse.

²) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 8073

RECOMMENDED CIRCUITS (continued)



Voltage divider type B

dynode No.n anode

| k | = | cathode | Sn | = | |
|-----|---|------------------------|----|---|--|
| acc | = | accelerating electrode | а | = | |

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be sufficient.

Different kinds of voltage dividers are possible. A circuit of type A results in the highest gain of the tube at a given total voltage; a circuit of type B gives a higher current output with better time characteristics, but the total gain is less at the same total voltage.

When pulses with high amplitudes are taken from the anode, it is useful to decouple the last stages as indicated in the circuit by means of capacitors of a few hundred pF, to avoid a voltage drop between these stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.



A



10 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for optical spectrometry, ultraviolet photometry and other applications which require a good sensitivity in the ultraviolet region.

| QUICK REFERENCE DATA | . A service la que demo |
|-------------------------------------|-------------------------|
| Spectral response | type U (S13) |
| Useful diameter of the photocathode | 32 mm |
| Anode sensitivity (at 1800 V) | 700 A/lm |

DIMENSIONS AND CONNECTIONS

S10

90

100

7703032

Base: 12-pin (Jedec B 12-43)





Dimensions in mm

ACCESSORIES

S7

S.5

acc.S

Socket

Mu-metal shield

type FE1002 type 56127

| GENERAL | | | | |
|---|--------------------|-------------|------------|----------------|
| Photocathode | | | | |
| Descirption | semi-transparent, | head-or | n, flat | surface |
| Cathode material | | (| Cs-Sb | |
| Minimum useful diameter | | | 32 | mm |
| Spectral response curve 1) | | type | U (S13 | 3) |
| Wavelength at maximum response | | 4000 | ± 300 | R |
| Luminous sensitivity ²) | N _k | av. min. | 70 40 | μA/lm μA/lm |
| Radiant sensitivity at 4000 $ m \AA$ | | | 60 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 10 | |
| Dynode material | | Ag-Mg | g-O-Cs | s and a |
| Capacitances | | | | |
| Anode to final dynode | C _{a/S10} | | 3 | pF |
| Anode to all other electrodes | Ca | | 5 | pF _ |
| TYPICAL CHARACTERISTICS | | | | |
| With voltage divider A | | | | |
| Anode sensitivity at V_b = 1800 V | Na | av. min. | 700 250 | A/lm A/lm |
| Anode dark current at $N_a = 60 \text{ A/lm}^3$) | I _{ao} | av. max. | 0.010 | μΑ μΑ |
| Linearity between anode pulse amplitud and input light pulse | le | up to | 30 | mA |
| | | | | |

¹) See spectral response curve in front of this section

 $^2\ensuremath{)}$ Measured with a tungsten ribbon lamp having a colour temperatue of 2850 $^0\ensuremath{\mathrm{K}}$

³) At an ambient temperature of 25 $^{\rm O}{\rm C}$

| TYPICAL CHARACTERISTICS (continued) | | |
|--|---------|----|
| With voltage divider B | | |
| Linearity between anode amplitude and input light pulse up | to 100 | mA |
| Anode pulse rise time at V_b = 1500 V ¹) | 4.10-9 | s |
| Transit time difference between the centre of the photocathode and the | | |
| edge at V_b = 1500 V | 3.10-9 | s |
| Total transit time at V_b = 1500 V | 36.10-9 | s |

LIMITING VALUES (Absolute max. rating system)

| Supply voltage | Vb | max. | 1800 | V |
|---|-----------------------------------|--------------|------------|--------|
| Continuous anode current | Ia | max. | 1 | mA |
| Voltage between cathode and first dynode | v_{k/S_1} | max. min. | 500 120 | V V |
| Voltage between consecutive dynode | V _{Sn} /S _{n+1} | max. min. | 300 80 | v v |
| Voltage between anode and final dynode ²) | v _{a/S10} | max. min. | 300 80 | V V |

RECOMMENDED CIRCUITS



Voltage divider type A

k = cathode $S_n = \text{dynode No.n}$ acc = accelerating electrode a = anode

¹) For an infinitely short light pulse.

2) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked. 7Z2 8037

RECOMMENDED CIRCUITS (continued)



Voltage divider type B

| k | = | cathode | Sn | = | dynode No.1 |
|-----|---|------------------------|----|---|-------------|
| acc | = | accelerating electrode | a | = | anode |

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be sufficient.

Different kinds of voltage dividers are possible. A circuit of type A results in the highest gain of the tube at a given total voltage; a circuit of type B gives a higher current output with better time characteristics, but the total gain is less at the same total voltage.

When pulses with high amplitudes are taken from the anode, it is useful to decouple the last stages as indicated in the circuit by means of capacitors of a few hundred pF, to avoid a voltage drop between these stages.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.



Α





11 STAGE PHOTOMULTIPLIER TUBE

The tube is intended for use in applications such as gamma-ray spectrometry.

| QUICK REFERENCE DAT | A | |
|--|--------|-------|
| Spectral response | type A | (S11) |
| Useful diameter of the photocathode | 44 | mm |
| Anode sensitivity (at 1800 V) | 1000 | A/lm |
| Energy resolution for 0.661 Mev Cs137 line | 8.5 | % |

DIMENSIONS AND CONNECTIONS

Dimensions in mm

Base: 14-pin (Jedec B14-38)



ACCESSORIES

S10

Sð

S6

S4

SZ

Socket

Mu-metal shield

FE1001 type 56128 type

7Z2 5466

MAINTENANCE TYPE

GENERAL

| Photocathode | | | | |
|---|-------------------|-------------|----------------|----------------|
| Description | semi-transparent, | head-o | on, flat | surface |
| Cathode material | | | Cs-Sb | |
| Minimum useful diameter | | | 44 | mm |
| Spectral response curve 1) | | type A | (S11) | |
| Wavelength at maximum response | | 4200 | 0 <u>+</u> 300 | 8 |
| Luminous sensitivity ²) | N _k | av. min. | 80 70 | μA/lm μA/lm |
| Radiant sensitivity at 4200 Å | n ontongeoting in | | 65 | mA/W |
| Multiplier system | | | | |
| Number of stages | | | 11 | |
| Dynode material | | Ag-Mg | -0-Cs | |
| Capacitances | | | el) air: | |
| Anode to final dynode | $C_{a/S_{11}}$ | | 3 | pF |
| Anode to all other electrodes | Ca | | 5 | pF |
| TYPICAL CHARACTERISTICS | | | | |
| Anode sensitivity at V _b = 1800 V | Na | av. min. | 1000 400 | A/lm A/lm |
| Anode dark current at N _a = 60 A/lm 3) | I _{ao} | av. max. | 0.015 0.050 | μΑ μΑ |
| Linearity between anode pulse amplitud and input light pulse | le | up to | 30 | mA |

Anode pulse rise time at V_b = 1500 V ⁴)

1) See spectral response curve in front of this section

 2) Measured with a tungsten ribbon lamp having a colour temperature of 2850 $^{
m O}$ K

3) At an ambient temperature of 25 °C

4) For an infinitely short light pulse

7Z2 5467

5.10-9

s

2
TYPICAL CHARACTERISTICS (continued)

| Transit time difference between the centre of the photocathode and the | | | |
|--|----------------|---------------------|--------|
| edge at V_b = 1500 V | | 4.10 ⁻⁹ | s |
| Total transit time at V_b = 1500 V | | 45.10 ⁻⁹ | s |
| Energy resolution for 0.661 Mev Cs137 line 1 ; |) | av. 8.5 max. 9.0 | % % |
| LIMITING VALUES (Absolute max. rating sys | stem) | | |
| Supply voltage | v _b | max. 1800 | v |

| Continuous anode current | Ia | max. | 1 | mA |
|---|-----------------------------------|--------------|------------|--------|
| Voltage between cathode and first dynode | v _{k/S1} | max. min. | 500 200 | v v |
| Voltage between consecutive dynodes | v _{Sn} /S _{n+1} | max. min. | 300 80 | v v |
| Voltage between anode and final dynode 2) | $v_{a/S_{11}}$ | max. min. | 300 80 | v v |

RECOMMENDED CIRCUIT



¹) Measured with a 1.5" x 1" Nal crystal

²) When calculating the anode voltage, the voltage drop in the load resistance should not be overlooked 7Z2 7856

OPERATIONAL CONSIDERATIONS

To achieve a stability of about 1% the ratio of the current through the voltagedivider bridge to that through the heaviest loaded stage of the tube should be approx. 100.

For moderate intensities of radiation a bridge current of approx. 0.5 mA will be a practical value.

The best results in γ -ray spectrometry will be achieved with a voltage of 4 times "Vs" between the cathode and the first dynode; however, the limiting values must not be exceeded. At a high tension of about 1200 V the tube will work most favourably.

When the tube has been exposed to full daylight just before mounting, it will probably show an increased dark current, which will be back at its normal value after several hours of operation.

It is advisable to screen the tube with a mu-metal cylinder against the influence of magnetic fields.

153 AVP



A



Scintillators





SAM

ZnS-SCINTILLATORFOR α AND α + β RADIATION DETECTION

SAM scintillators comprise an acrylate disc, covered at one side with a thin aluminized scintillationfoil.

Zinc sulphide activated with silver is used as scintillating material.

The scintillator surface may be touched. Only high pressures or abrasive products can damage the film locally.

The SAF type consists of the same scintillating layer deposited on cellulose acetate-foil instead of acrylate.

CHARACTERISTICS

| Time constant of fluorescence | 10-6 | S |
|---|------|----|
| Wavelength of maximum emission | 4500 | R |
| Maximum ambient temperature | 40 | °C |
| Detection efficiency, minimum | 47.5 | % |
| average | 55 | % |
| (measured with a thin Am^{241} source 5.45 - 5.48 MeV, $p 9$ mm, distance 7 mm from the scintillator) | | |

| Mass per unit area of the ZnS layer | 5 | mg/cm ² |
|---|-----------|--------------------|
| Mass per unit area of the metal-coating | 600 - 800 | $\mu g/cm^2$ |

SCINTILLATORS FOR ALPHA -BÊTA DETECTION

Type SPABM consisting of a metallized film of ZnS deposited on a thin foil of SPF (thickness ≥ 0.2 mm)can be delivered with or without acrylate support.

UNMETALLIZED SCINTILLATORS

Types SA and SPAB (unmetallized SAM and SPABM) can be ordered.

SPECIAL SCINTILLATORS

All types can be made resistant to a salty atmosphere for at least 100 hours on request.

7Z2.7988

SAM

Standard dimensions:

Discs:

| Туре | Diameter (mm) | Thickness (mm) | Matching photomultiplier |
|--------|------------------|-------------------|--------------------------|
| SAM19 | 19 | 3 | XP1110 |
| SAM25 | 25 | 3 | 52AVP |
| SAM40 | 40 | 3 | 150AVP |
| SAM50 | 50 | 3 | 53AVP/XP1000 |
| SAM70 | 70 | 3 | XP1030 |
| SAM125 | 125 | 3 | 54AVP |

Sheet:

| SAM223/127 | length | : | 223 | mm | |
|------------|-----------|---|-----|----|--|
| | width | : | 127 | mm | |
| | thickness | : | 3 | mm | |

Foil:

| SAF4400/70 | length | : 44 | 100 | mm | an a |
|------------|----------|------|------|----|--|
| | width | : | 70 | mm | |
| Spinite | thicknes | s:0 | . 23 | mm | |

SAM



Quality control points with a thick U source and equivalent values for a thin Pu source

A



SIS

Na I (TI) CRYSTAL SCINTILLATOR FOR & AND X-RAYS DETECTION AND SPECTROMETRY

SIS scintillators consist of Thallium activated sodium iodide crystals. The crystals are mounted in aluminium with glass windows.

CHARACTERISTICS

| Time constant of fluorescence | 0.25.10-6 | S |
|----------------------------------|-----------|----------------------------------|
| Time constant of phosphorescence | 2.5.10-3 | S |
| Wavelength of maximum emission | 4100 | A |
| Density | 3.66 | |
| Refractive index | 1.77 | |
| Maximum temperature gradient | 10 | ^o C min ⁻¹ |

SCINTILLATORS FOR GAMMA-SPECTROMETRY

The types with dimensions up till 44 x 50 can be realized with a resolution of $\leq 9\%$ for the peak of a $\rm C_S{}^{137}$ gamma ray source. For bigger dimensions and well-type crystals: < 10%.

The typenumber of this spectrometry quality is followed by SP.

SCINTILLATORS FOR X-RAY DETECTION AND COUNTING

Thin SIS mounts can be ordered (thickness of the crystal \leq 5 mm) with a Be window (thickness 0.20 mm).

SPECIAL SCINTILLATORS

Anticoincidence mounts can be made on request. (SIS crystal with or without mounting in a SPF scintillator). Standard dimensions:

| Туре | Diameter A of the crystal (mm) | Thickness B of the crystal (mm) | Matching photomultiplier |
|--------------------------|--------------------------------------|---------------------------------------|---|
| SIS 12x12 | 12 | 12 | |
| SIS 12x25 | 12 | 25 | } XP 1110 |
| SIS 19x19 | 19 | 19 |) XP 1110 |
| SIS 19x25 | 19 | 25 | } 150 AVP |
| SIS 25x12 | 25 | 12 | |
| SIS 25x25 | 25 | 25 | 150 AVP |
| SIS 25x50 | 25 | 50 | J |
| SIS 32x25 | 32 | 25 | a man i nasimi |
| SIS 32x32 | 32 | 32 | } 150 AVP |
| SIS 44x25 | 44 | 25 |) 52 AVD |
| SIS 44x38 | 44 | 38 | 152 AVP |
| SIS 44x50 | 44 | 50 | J 135 AVP |
| SIS 50x50 | 50 | 50 | nan de marce de la com |
| SIS 63x50 | 63 | 50 | XP 1030 |
| SIS 63x63 | 63 | 63 | XP 1031 |
| SIS 63x75 | 63 | 75 | , |
| SIS 75x50 | 75 | 50 | XP 1030 |
| SIS 75x75 | 75 | 75 | $\begin{array}{c} \begin{array}{c} XP \ 1031 \\ 54 \ AVP \end{array}$ |
| Well-type: SIS 44x50P | 44 | 50 | Dimensions of the well: diameter 17 mm depth 39 mm |

Other dimensions on request.

SIS

Dimensions of the mounted crystal:

| | | dimensio | ons (mm) | |
|-----------|------|----------|----------|-----|
| Туре | Е | С | D | F |
| SIS 12x12 | 16.2 | 20.2 | 16.8 | 5.5 |
| SIS 12x25 | 16.2 | 20.2 | 29.8 | 6.5 |
| SIS 19x19 | 22.2 | 26.2 | 23.8 | 5.5 |
| SIS 19x25 | 22.2 | 26.2 | 29.8 | 6.5 |
| SIS 25x12 | 29.2 | 33.2 | 16.8 | 5.5 |
| SIS 25x25 | 29.2 | 33.2 | 29.8 | 5.5 |
| SIS 25x50 | 29.2 | 33.2 | 54.8 | 6.5 |
| SIS 32x25 | 36.2 | 40.2 | 29.8 | 5.5 |
| SIS 32x32 | 36.2 | 40.2 | 36.8 | 6.5 |
| SIS 44x25 | 48.2 | 52.2 | 29.8 | 6.5 |
| SIS 44x38 | 48.2 | 52.2 | 42.8 | 6.5 |
| SIS 44x50 | 48.2 | 52.2 | 54.8 | 6.5 |
| SIS 50x50 | 54.2 | 58.2 | 54.8 | 6.5 |
| SIS 63x50 | 67.2 | 71.2 | 54.8 | 6.5 |
| SIS 63x63 | 67.2 | 71.2 | 67.8 | 6.5 |
| SIS 67x75 | 67.2 | 71.2 | 79.8 | 6.5 |
| SIS 75x50 | 79.2 | 83.2 | 54.8 | 6.5 |
| SIS 75x75 | 79.2 | 83.2 | 79.8 | 6.5 |



7Z2 7992

SIS



Absorption of γ radiation in the crystal

SPF

FLUORESCENT PLASTIC SCINTILLATOR FOR α , β , γ , FAST NEUTRONS AND COSMIC RAYS DETECTION

SPF scintillators are composed of polystyrene with p-terphenyl and 1 - 1' 4 - 4' tetraphenylbutadiene.

The p-terphenyl is the fluorescent agent, while the TPB corrects its emission spectrum in order to adapt it to the spectral sensitivity of the photo-multiplier.

They are delivered with an adhesive papercover to protect the surface against damage. Before use this paper can be easily removed.

CHARACTERISTICS

| Time constant of fluorescence | 4.10-9 | S |
|--|----------------|----|
| Time constant of phosphorescence | 0 | |
| Wavelength of maximum emission | 4300 | A |
| Density | 1.06 | |
| Refractive index | 1.59 | |
| Softening point | 80 - 85 | 00 |
| Light output % Anthracene | 55 - 65 | % |
| Coëfficient of linear expansion 6.10 |)-5-8.10-5 | |
| Ratio no. of H-atoms to no. of C-atoms | ≈ 1.0 | |

SCINTILLATORS FOR BÊTA DETECTION

Type SPFM (aluminized SPF) The light-tight metalcover has a mass per unit area of $600 - 800 \ \mu g/cm^2$.

SCINTILLATORS FOR ALPHA DETECTION

SPF foil with or without support, made of acrylate or glass.

SPECIAL SCINTILLATORS

- Compositions for increased temperatures (maximum 150 °C)
- To obtain an improved efficiency the scintillators can be ordered with a metal or titanium dioxide reflective coating.

SPECIAL FORMS

All forms can be prepared to customers specifications.

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Standard dimensions:

Discs and cylinders:

| Туре | Diameter (mm) | Standardized thicknesses (x) (mm) | Matching photomultiplier |
|----------|------------------|--|--------------------------------------|
| SPF 25/x | 25 | 1979 - Supplementary and a s | 52AVP |
| SPF 40/x | 40 | oniges, entingent, vg. u | 150 AVP |
| SPF 50/x | 50 | 0.2-0.5-1-1.5-3- 20-80-100-200 | {53AVP/56AVP XP1000/XP1020/XP1021 |
| SPF 70/x | 70 | and the second second second | XP1030 |
| SPF125/x | 125 | 0.2-0.5-1-2-3- 20-80-100-200 | 54AVP/58AVP/XP1040 |
| SPF175/x | 175 | 155 | 57AVP/60AVP |
| SPF260/x | 260 | 260 | 57AVP/60AVP |
| SPF450/x | 450 | 300 | 57AVP/60AVP |

Sheets and blocks:

| Туре | Length (mm) | Width (mm) | Standardized thicknesses (x) (mm) |
|----------------|----------------|---------------|--------------------------------------|
| SPF 350/350/x | 350 | 350 | 1-2-4-5-6-8-10 |
| SPF 500/500/x | 500 | 500 | 8-10-15-20-25 |
| SPF 800/500/x | 800 | 500 | 10-15-20-25-30 |
| SPF1500/1000/x | 1500 | 1000 | 10-15-20-25 |

Foil: thickness between 5 and 100 μ .

Scintillators of one piece can be made up till 100 kg. Bigger blocks (up till 1000 kg) can be manufactured by welding more pieces together.

SPF



Range of particles in dependence of energy

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PLASTIC HORNYAK SCINTILLATOR FOR FAST NEUTRONS MEASUREMENT IN NUCLEAR REACTORS

SPH scintillators are composed of a styrene monomer polymerized with zinc sulphide. The action of neutrons causes the styrene to produce recoil protons which ionize the zinc sulphide, thus producing scintillations.

CHARACTERISTICS

| Time constant of fluorescence | 10-6 | s |
|--|---------|----|
| Wavelength of maximum emission | 4500 | R |
| Softening point | 80 - 85 | °C |
| Response to fast neutrons | 1.5 | % |
| Ratio no. of H-atoms to no. of C-atoms | ≈ 1.0 | |

SENSITIVITY TO GAMMA RAYS AND SLOW NEUTRONS

Because this sensitivity is low the luminous pulses produced by these two types of radiation have a very much smaller amplitude. It is therefore possible to eliminate them almost completely by choosing the threshold of the discriminator which follows the photomultiplier at such a high level that only the pulses from fast neutrons are counted.

Standard dimensions:

Discs:

| | Туре | Diameter (mm) | Thickness (mm) | Matching photomultiplier |
|---|--------|------------------|-------------------|--------------------------|
| 1 | SPH 25 | 25 | 15 | 52AVP |
| | SPH 40 | 40 | 15 | 150AVP |
| | SPH 50 | 50 | 15 | 53AVP/XP1000 |
| | SPH 70 | 70 | 15 | XP1030 |
| | SPH125 | 125 | 15 | 54AVP |

SPH

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EASTIC HORMYNE SCINTILLATOR 8 RASE NEUTRONS MEASUREMEN HN NUCLEAR REACTORS



Response curve with a Ra-Be source

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INDEX OF TYPENUMBERS

| Type No. | Section | Type No. | Section | Type No. | Section |
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| D10-12 | CRT | M28-12W | CRT | XP1003 | PmT |
| D13-15 | CRT | M36-11W | CRT | XP1004 | PmT |
| D13-16 | CRT | M36-13W | CRT | XP1005 | PmT |
| D13-16/01 | CRT | M.13-16 | CRT | XP1010 | PmT |
| D13-17 | CRT | MG/U/Y6-2 | CRT | XP1011 | PmT |
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| D13-23 | CRT | ORP11 | PcD | XP1021 | PmT |
| D13-24 | CRT | ORP30 | PcD | XP1023 | PmT |
| D13-26 | CRT | ORP50 | PcD | XP1030 | PmT |
| D13-26/01 | CRT | ORP60 | PcD | XP1031 | PmT |
| D13-27 | CRT | ORP61 | PcD | XP1032 | PmT |
| D.3-91 | CRT | ORP62 | PcD | XP1033 | PmT |
| D.7-5 D.7-6 D.7-11 D.7-31 D.7-32 | CRT CRT CRT CRT CRT | ORP63 ORP90 RPY13 RPY18 RPY19 | PcD PcD PcD PcD PcD PcD | XP1040 XP1110 XP1111 XP1111B XP1113 | PmT PmT PmT PmT PmT |
| D.7-36 | CRT | RPY20 | PcD | XP1114 | PmT |
| D.7-78 | CRT | RPY27 | PcD | XP1115 | PmT |
| D.10-6 | CRT | RPY41 | PcD | XP1115B | PmT |
| D.10-74 | CRT | RPY43 | PcD | XP1115C | PmT |
| D.10-78 | CRT | SAM | Sc | XP1116 | PmT |
| D.13-2 | CRT | SIS | Sc | XP1117 | PmT |
| D.13-32 | CRT | SPF | Sc | XP1118 | PmT |
| D.13-34 | CRT | SPH | Sc | XP1120 | PmT |
| E10-12 | CRT | XP1000 | PmT | XP1121 | PmT |
| M21-11W | CRT | XP1001 | PmT | XP1122 | PmT |

CRT = Cathode-ray tubes

PcD = Photoconductive Devices

PmT = Photomultiplier Tubes

PT = Photo tubes

CT = Camera tubes

Sc = Scintillators

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| Type No. | Section | Type No. | Section | Type No. | Section |
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| XP1123 XP1130 XP1131 XP1140 XP1141 | PmT PmT PmT PmT PmT | 155UG 55850 55850AM 55851 *55852 | PT CT CT CT CT | ЭСИ | |
| XP1180 53A VP 53U VP 54A VP 54U VP | PmT PmT PmT PmT PmT | 55875 55875R,G,B 55876 | CT CT CT | | 4174 51-92 71,710 71,710 |
| 56A VP 56A VP/03 56A VP/05 56C VP 56TU VP | PmT PmT PmT PmT PmT | | | 1102 -1300 1140 1140 | 91-94-949 91-94-94 01-95-00 101-8-00 |
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CRT = Cathode-ray tubes PcD = Photoconductive Devices PmT = Photomultiplier Tubes PT = Photo tubes CT = Camera tubes Sc = Scintillators

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| Catho | de-ray tubes | |
|--------|--------------------|---|
| Came | ra tubes | |
| Photo | tubes | |
| Photo | conductive devices | S |
| Photo | omultiplier tubes | |
| Scinti | llators | |







